

Copper Metal Matrix Composite Cu-TiO₂ Electrodeposited in Aqueous Suspensions of the Nanometric Size Particles of Anatase and Rutile*

by V. Medelienė^{1**}, R. Juškėnas¹, M. Kurtinaitienė¹ and M. Jaskula²

¹*Institute of Chemistry, A. Goštauto 9, 01108 Vilnius, Lithuania*

²*Jagiellonian University, Faculty of Chemistry, Ingardena 3, 30-060 Kraków, Poland*

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The electrolytic codeposition of nanometric size TiO₂ particles with copper from an aqueous electrolyte has been investigated. Two crystalline modifications of TiO₂ – anatase and rutile were used to prepare a nanodispersed suspension. Qualitative dispersion-hardened Cu-TiO₂ composite coatings were obtained with the reproducible results only from a freshly prepared concentrated electrolyte-suspension. It has been revealed that nanodispersed materials can be obtained electrochemically with an anatase sort of titania. Rutile powder is not as suitable as anatase for this purpose.

Key words: copper composite, nanometer-dispersed aqueous suspension of TiO₂

The primary attention of researchers in obtaining the composite coatings was devoted to the inert ceramic particles of micrometer size by electrodeposition with metals and alloys. The materials, obtained from the structured micrometer-dispersed suspensions, possess high strength due to the connection-contacts of coagulation type, which are formed as a result of cohering of the particles through the layer of the liquid medium of electrolyte with a force of 10^{-8} – 10^{-12} N. The coatings formed have a dispersion-hardened metallic matrix with an evenly distributed solid phase of particles. For example, nickel composite coatings containing micrometric size particles such as SiC, Al₂O₃ are widely used in the automotive industry and in the aeronautics as wear, corrosion and oxidation resistance coatings [1–8].

Relatively little information is available on the formation of metal matrix composite coatings in aqueous electrolyte-suspensions with particles of submicrometric size [9–12]. The development of composite plating with submicrometric size particles is, however, hampered by the following problems. In aqueous plating electrolytes, particles easily agglomerate due to the compression of the diffusive double layer surrounding the particles with the high ionic strength. As a consequence, the codeposition of agglomerated particles takes place and the anticipated mechanical, chemical and/or physical properties of the composite coatings are not reached. Sec-

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** Author for correspondence. E-mail: viktorija.m@centras.lt

ondly, the codeposition of particles from aqueous electrolytes increases due to decrease in the hydrophilicity of particles by using surfactants with the hydrophobic effect [4–6]. In an attempt to overcome the problems of agglomeration of sub-micrometric/or nanometric size particles and their low degree of codeposition linked to the surface hydrophilic-hydrophobic balance, the other way is the electrolytic codeposition of particles from a non-aqueous, for example, aluminium electrolyte [13].

The interest in metallic coatings containing particles has also led to research in the structuring of thin films with the help of nano-sized powders. Nanophase ceramics have generated considerable scientific interest recently because of the improvements in a variety of properties that are expected to result from grain-size reduction to the nanometer scale. These materials have several technical applications like catalysts lowering the sintering temperature, increasing the sintering rate, controlling the microstructure in high performance ceramic materials, and electronic and magnetic applications, micro-electromechanical components. The desirability of small and uniform particle size for obtaining quality ceramics has been documented in general [14] and for TiO_2 specifically [15,16].

Titania powders, widely used in industrial application as pigments, opacifiers, photocatalysts, and fillers, have been obtained either directly from titanium-bearing minerals or by precipitation from solutions of titanium salts. Titania particles have also been made by reaction in aerosols. The most common procedure for the preparation of TiO_2 particles reported in literature is based on the hydrolysis of acidic solutions of Ti (IV) salts and hydrolysis reactions of titanium alkoxides have been employed to generate finely divided, high purity TiO_2 powders [17–24].

Titanium(IV) oxide (TiO_2) is nontoxic, opaque and brilliant white. It is commonly known that these properties make it suitable as a pigment in white paint. Titania exists in two tetragonal forms, a metastable phase, anatase, and a stable form, rutile and a orthorhombic form as brookite. Brookite is non stable and not used in practice. The volume free energy of the rutile phase is always lower than that of anatase. Therefore, on heat treatment, the anatase phase transforms into the stable rutile form. The transformation is a nonreversible metastable-to-stable transformation; the transition temperature reported in literature ranges from 450 to 1200°C. The majority of chemical methods of preparation yield the metastable anatase phase, which on further heat treatment gives the rutile phase. Rutile phase, for example, in pigments has a smaller photochemical activity than that of anatase form, and, consequently, higher atmospheric stability [22,25].

Attempts to obtain the composite coatings on the basis of copper with the particles of titania were undertaken [4,26]. The absence of experience in this field and look on the problem as on conventional electrodeposition process did not lead researchers to the desirable results.

The goal of this work was to investigate the aqueous suspension preparation with nanometric size TiO₂ powder, or more precisely, with its crystalline modifications as anatase and rutile in a nanopowder form in order to obtain new materials by electrodeposition with copper.

EXPERIMENTAL

Materials: The coatings studied were electrodeposited on the copper substrate (1 cm²) for morphology, elemental composition by XPS, crystalline state investigations and for microhardness measurements, on titanium (for morphology studies) in an acidic 0.5 M copper electrolyte and in electrolyte-suspensions with TiO₂ particles (with its crystalline modifications form as rutile or anatase) at a cathodic current density (i_c) of 2 A/dm² and at 18 ± 1 °C. A magnetic stirrer was used to agitate electrolyte-suspension. Electrolytic copper was used as an anode.

The preparation of suspension: To prepare the suspension the average size of TiO₂ particles was (nm): in the case of anatase – 100 ÷ 1000 and rutile – 100 ÷ 2000. The concentration of TiO₂ particles in electrolyte-suspensions was 100 and 200 g · dm⁻³. 100 ml volume electrolyte-suspensions were freshly prepared to obtain stable hydrosols of TiO₂. The hydrosols of TiO₂ were stabilized in aqueous suspension with the same constant 0.5 M concentration of ions of H⁺; SO₄²⁻; Cu²⁺/Cu⁺ at pH = 0.8 for two types and concentrations of suspensions. Analytical grade chemicals and bidistilled water were used to prepare solutions.

X-ray microprobe spectral analysis of titanium: The titanium (Ti) distribution in copper coatings was studied using a JXA-50A electron scanning microscope (Japan) by X-ray microprobe spectral analysis. The X-ray attack was applied to the whole surface using 25 to 100 discharges in different surface places of the materials under investigation. The duration of electron beam attack was 10–20 sec. The average X-ray intensity values on electron emission of Ti were obtained after computer data treatment. The amount of TiO₂ was calculated multiplying the quantity of the distributed Ti in copper composite coating on the ratio between the atomic mass of TiO₂ and Ti – 79.88 and 47.88, respectively.

X-ray photoelectron spectroscopy (XPS) analysis: The elemental composition of Cu-TiO₂ coatings deposited from freshly prepared electrolyte-suspension was investigated by XPS. The spectra were recorded with an ESCALAB MK-11 spectrometer (VG Scientific, UK) using characteristic MgK_α radiation (the energy of 1253.6 eV, pass energy of 20 eV). The spectrometer had a base pressure of 5 × 10⁻⁵ Torr in a spectrometer chamber where Ar⁺ ion bombardment was performed. The argon gas pressure in preparation chamber was maintained at 6 × 10⁻⁵ Torr and the ion gun was operated at 2 kV and 20 mA at normal incidence. Under these conditions the titanium phase can be etched at a rate of 2–3 nm · min⁻¹. The XPS spectrum lines were recorded at the surface and at the various depths of coating. When investigating the reference samples by XPS, the spectra of the following elements were recorded: Cu 2p_{3/2}; Ti 2p_{3/2}; O 1s; C 1s. The empirical sensitivity factors of the elements were taken. The measured binding energies (E_b) of elements were calibrated with respect to the C 1s electron peak at 284.6 eV due to residual pump-oil on the sample surface [27,28]. The maximum accuracy of the method was 0.1 at. %.

X-ray diffraction method: The crystalline state of TiO₂ particles both in copper coatings and in the powder form used were identified by the X-ray diffraction method using an X-ray diffractometer D8 (Bruker AXS) and applying CuK_α radiation at λ_{Cu} = 1.5418 Å. X-ray diffraction peaks of Cu and TiO₂ were recorded with a constant rate of 0.5° · min⁻¹ of detector [29].

The morphology study: The morphology of matrix surface of Cu-TiO₂ coatings was investigated by using a transmission electron microscope PEM-100 (Ukraine) and shadowed with Pd used carbon replicas. A replicating C-Pd film (with adhered particles) was torn off from the surface with gelatin which was dissolved after that in hot water. The morphology of Cu and Cu-TiO₂ and that of particles incorporated in the copper matrix was studied and micrographed with a JXA-50A field-emission (SEI) type scanning electron microscope at an acceleration voltage of 25 kV and an electron current (ec) of 5 · 10⁻¹² A.

The measurement of microhardness: Vickers microhardness (HV_{50} in $\text{kgf} \cdot \text{mm}^{-2}$) was measured using an indenter PMT-3 on a $50 \mu\text{m}$ thick surface by a 50 g indentation of load and was calculated by the formula:

$$HV_{50} = \frac{1857.4 \cdot P}{d^2} \quad (1)$$

where P is the load, g, and d is a diagonal of diamond prism, mm. The microhardness was measured under normal conditions for coatings from freshly prepared electrolyte-suspensions and after their ageing for 45 days.

RESULTS AND DISCUSSION

Both in the anatase and rutile case the amount of TiO_2 particles in Cu- TiO_2 coatings codeposited with copper in acidic copper electrolyte-suspension depends on the concentration of particles in electrolyte-suspension and on the suspension preparation time (Table 1). Qualitative dispersion-hardened Cu- TiO_2 composite coatings are obtained with the reproducible results only from freshly prepared concentrated electrolyte-suspensions (Table 2). One can see from the data on the microhardness of composite coatings obtained by prolonged electrolysis of electrolyte-suspension and presented in Table 2 that the hardening effect on copper matrix decreased in this case. A longer exposure time and ageing of electrolyte-suspension also had a negative effect on the microhardness of coatings (Table 2, column 5). The HV value of Cu-anatase coating decreased from 244 ± 25 to $179 \pm 19 \text{ kgf} \cdot \text{mm}^{-2}$ at a concentration of TiO_2 equal to 100 and $200 \text{ g} \cdot \text{dm}^{-3}$, respectively.

Table 1. The amount of titanium (Ti) in Cu- TiO_2 composite coating *versus* on concentration (c) of nanometric TiO_2 particles-hydrosols in electrolyte-suspension. The thickness of coating in Tabs. 1, 2 – $50 \mu\text{m}$.

| Coatings from freshly prepared suspension | Concentration of suspension/ $\text{g} \cdot \text{dm}^{-3}$ | Amount of Ti in coating/mass% | Calculated amount of TiO_2 /mass% |
|---|--|-------------------------------|--|
| 1. Cu- TiO_2 (Anatase) | 100 | 3.935 | 6.53 |
| 2. Cu- TiO_2 (Anatase) | 200 | 6.275 | 10.46 |
| 3. Cu- TiO_2 (Rutile) | 100 | 3.804 | 6.338 |
| 4. Cu- TiO_2 (Rutile)* | 100 | 3.0 | 4.99 |
| 5. Cu- TiO_2 (Rutile) | 200 | 6.174 | 10.298 |

*from 64 days-aged suspension.

On the coating surface anatase particles have major advantages in adhesion to the electrode surface – this clearly was seen on the optical image of surface after the samples were carefully washed and centrifuged. It is worthy to note that the carbon replic method enables to observe stronger adhesion of anatase (Fig. 1 a, b). The study of elemental composition of coatings at depth has shown greater quantities (at. %) of titanium and oxygen in the anatase case as well (Table 3). Stronger adhesion in this case predominated and the amount of anatase particles on the surface was greater than that

of rutile and due to this more incorporated into the Cu-TiO₂ coating (Table 3). The behaviour of rutile when electrodeposited with copper may be explained by weak adhesion of lesser quantity of particles in suspension – 100 g·dm⁻³. The increase in concentration of rutile particles up to 200 g·dm⁻³ in suspension the dispersion hardenning effect of Cu-TiO₂ coatings is possible (Table 2). Strong adhesion with growing metal layer is essential for the incorporation of particles into the matrix.

Table 2. Microhardness (HV₅₀) ± its dispersion of Cu-TiO₂ coatings at 20 ± 1°C *versus* on concentration of TiO₂ in electrolyte-suspension (c) and on electrical charge quantity passed through the used suspensions (Q).

| Coatings | c/g·dm ⁻³ | HV ₅₀ /kgf·mm ⁻² (Q _{1,2} = 206 C) | HV ₅₀ /kgf·mm ⁻² (Q ₃ = 340 C) | HV ₅₀ /kgf·mm ⁻² (After 45 days + Q ₄ = 880 C) |
|----------------------------------|----------------------|--|--|--|
| 1 | 2 | 3 | 4 | 5 |
| 1. Cu | 0 | 168 ± 14 | 169 ± 17 | – |
| 2. Cu-TiO ₂ (Anatase) | 100 | 244 ± 25 | 229 ± 33 | 179 ± 19 |
| 3. Cu-TiO ₂ (Anatase) | 200 | 262 ± 19 | 266 ± 26 | 187 ± 17 |
| 4. Cu-TiO ₂ (Rutile) | 100 | 190 ± 25 | 190 ± 12 | 219 ± 12 |
| 5. Cu-TiO ₂ (Rutile) | 200 | 254 ± 18 | 208 ± 14 | 190 ± 16 |

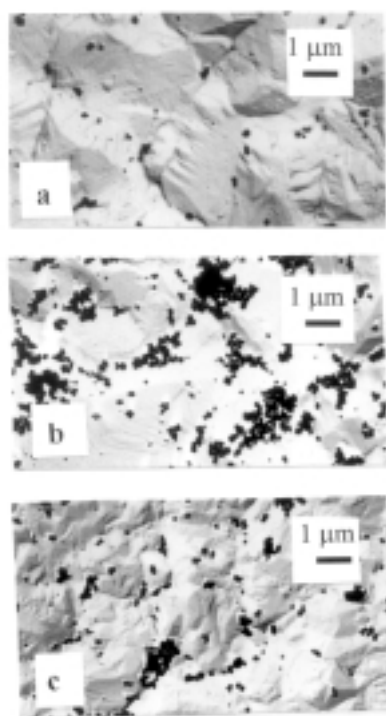


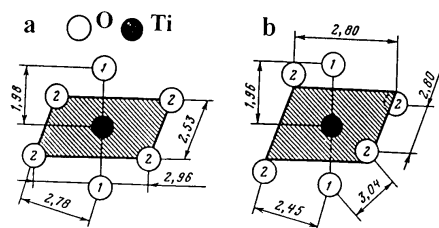
Figure 1. Morphology of Cu-TiO₂ coating surface with rutile (a) and anatase (b, c) particles codeposited in a freshly prepared (a, b) and 64 days-aged suspension (c). The concentration of suspension – 100 g·dm⁻³. The thickness of coatings – 50 μm.

Table 3. Elemental composition (in at.%) of composite Cu-TiO₂ coatings on the surface and in the depth of matrix analysed by XPS method. Thickness of coating in Tables 3, 4 – 25 μm.

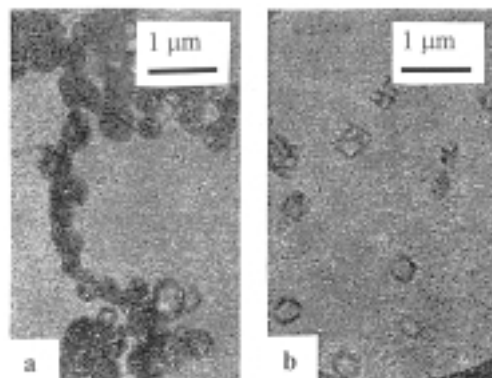
| Etching depth/nm | Elements | TiO ₂ amount g·dm ⁻³ | | | |
|--------------------|-------------|--|----------------|---------------|---------------|
| | | Anatase | | Rutile | |
| | | 100 | 200 | 100 | 200 |
| 0 (on the surface) | Cu | 10.71 | 14.63 | 16.89 | 16.09 |
| | O | 85.61 | 79.68 | 78.39 | 79.82 |
| | Ti | 3.68 | 5.69 | 4.72 | 4.1 |
| | Ti:O | 1:23.28 | 1:14.01 | 1:16.6 | 1:16.4 |
| 1.5 | Cu | 75.72 | 65.25 | 81.99996 | 75.82 |
| | O | 19.62 | 27.42 | 14.43 | 19.32 |
| | Ti | 4.66 | 7.33 | 3.61 | 4.86 |
| | Ti:O | 1:4.20 | 1:3.74 | 1:3.99 | 1:3.97 |
| 6.0 | Cu | 82.39 | 73.15 | 86.08 | 78.82 |
| | O | 14.86 | 22.43 | 11.26 | 16.82 |
| | Ti | 2.76 | 4.42 | 2.66 | 4.35 |
| | Ti:O | 1:5.38 | 1:5.07 | 1:4.23 | 1:3.87 |
| 66 | Cu | 84.00 | 70.37 | 86.53 | 77.59 |
| | O | 14.03 | 27.66 | 11.45 | 20.31 |
| | Ti | 1.97 | 1.97 | 2.02 | 2.10 |
| | Ti:O | 1:7.12 | 1:14.07 | 1:5.68 | 1:9.67 |
| 126 | Cu | 81.52 | 66.16 | 85.04 | 75.45 |
| | O | 15.32 | 28.24 | 11.85 | 20.30 |
| | Ti | 3.16 | 5.60 | 3.11 | 4.25 |
| | Ti:O | 1:4.84 | 1:5.04 | 1:3.8 | 1:4.78 |

It should be emphasized that the oxide TiO₂ due to its special features and extraordinary casual state in solutions has been an object of studies for decades [30–33]. According to [30–32], the chemical-physical transformations in aqueous suspension with the further colloidal stage affected the suspension state of superhydrophilic TiO₂ powder of anatase and rutile.

The structurization of suspension with the superhydrophilic TiO₂ particles due to chemical transformations, the first of them, hydrolysis of hydrated oxides TiO₂·nH₂O to complex ions [Ti(OH)₆]²⁻ in an aqueous solutions occurs. In addition, fourvalent transition-metal titanium due its oxophilic properties exhibited in its strong binding to hydroxide to form simple octahedral complex. In accordance with [30–33], the subsequent polymerization of the existing aquacomplex as [Ti(OH)₂(OH)₄]²⁺ takes place. The experimental data in Table 3 testify that the stechiometric elemental proportion of titanium to oxygen is greater than that in the formula of TiO₂. In Scheme 1 the coordination number (6) of titanium atom is related to the octahedral structure with oxygen atoms (or hydroxyl ions in aqua solutions) both in the anatase and rutile case.

**Scheme 1.** Interatomic spacings in crystalline structure of anatase (a) and of rutile (b).

According to [17,30], during a complicated multi-step structurization process in suspension the further colloidal stage that is formation of micelles and granules after the equilibrium processes of coagulation and peptization of the hydrosols of TiO₂ in strongly acidic solutions occurs. The formed in freshly prepared suspension hydrosols of TiO₂ are stabilized with the ions of H⁺; OH⁻; SO₄²⁻; Cu²⁺/Cu⁺ present in solutions at pH = 0.8. Amorphous hydrosols are formed from a freshly prepared aqueous suspension of TiO₂. Nanocrystalline (≥ 100 nm) TiO₂ are formed after 1–2 h of suspension preparation with titania (Scheme 2) [30].



Scheme 2. SEM of TiO₂ hydrosols: a – amorphous particles formed from freshly prepared suspension; b – nanometric sized crystalline (≥ 100 nm) particles of TiO₂ formed after 1–2 h of suspension preparation.

One can see in the SEM pictures of the surface morphology of Cu-TiO₂ coatings codeposited from an aged suspension (Figs. 2–4), that the shape of incorporated particles is perfect when compared to that from a freshly prepared suspension – most of observable codeposited into matrix particles had an amorphous shape (Scheme 2 and Figs. 2, 3). The formation of structurized suspension in co-deposition of sub/or nanocomposites is based on the crystalline or amorphous TiO₂ hydrosols formation in a freshly prepared suspension. In aged suspension their peptization occurred and particles were round and identical (Fig. 4). In this case the optimal structurization of suspension in order to obtain heterogenic dispersion-hardened coatings did not occur. The aged during peptization TiO₂ particles were incorporated into the matrix, probably, in a mechanical way and had not any hardening effect on it (Table 2, column 5).

On the other hand, it is known, that non-metallic inclusions in the metal can change its thin structure and break up the crystal lattice, resulting in changes in the physical and mechanical properties of the electrodeposits. The inclusions of inert particles affect fine structure parameters: the concentration of packing defects of both deformation and twinning types can increase, as well as the dislocations density and their movement [7,8,29,34].

The crystalline structure can be evaluated on the basis of the XRD peak broadening β , which is calculated from the formula:

$$\beta = B_{FWHM}^{Sp} - B_{FWHM}^{St} \quad (2)$$

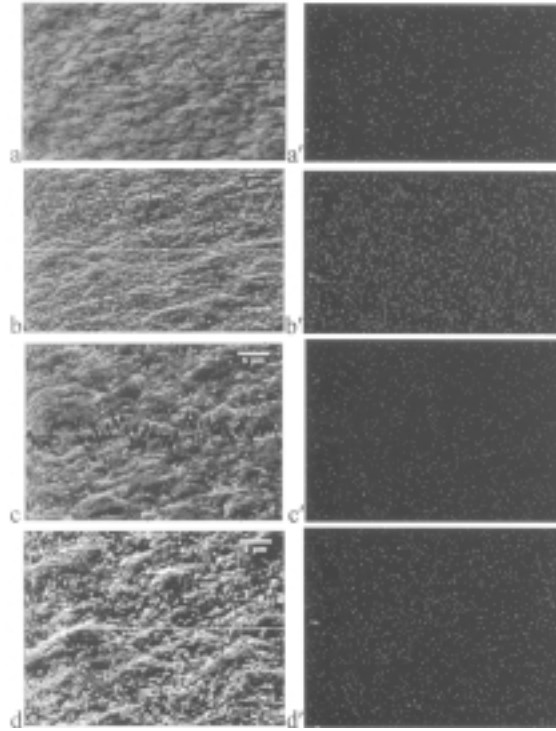


Figure 2. Secondary electron image of Cu-TiO₂ composite at a depth of coating of 5 μm as a function of concentration of nanometric size particles of anatase (a, b) and rutile (c, d). The distribution of Ti in Cu-TiO₂ coating: a', b' – with anatase and c', d' – with rutile. The concentration of TiO₂ particles in suspension (g · dm⁻³): (a, a', c, c') – 100 and (b, b', d, d') – 200.

Superscript *Sp* means the XRD peak's full width at the half maximum for specimen and superscript *St* that for the standard. The parameters of crystalline structure are crystallite size (*D*) and crystallite microdeformation (*ε*). The crystallite size (*D*) can be calculated from the Scherrer formula [29]:

$$D = \frac{0.9\lambda}{\beta \cos \Theta} \quad (3)$$

where λ is a wavelength of X-ray radiation used. Crystallite microdeformation level can be evaluated from the formula:

$$\varepsilon = \frac{\beta}{4 \tan \Theta} \quad (4)$$

The dependence of $\tan \Theta$, $\sec \Theta$ and β of Cu-TiO₂ coatings on the X-ray diffraction angle θ shows that β is closer to $\tan \Theta$ dependence and this indicates that broadening of diffraction peak is determined by microdeformation but not by crystallites (blocks) size (Fig. 5). The studies of crystalline structure of copper coatings have shown that the penetration of TiO₂ particles into the matrix has insignificant influence on the fine

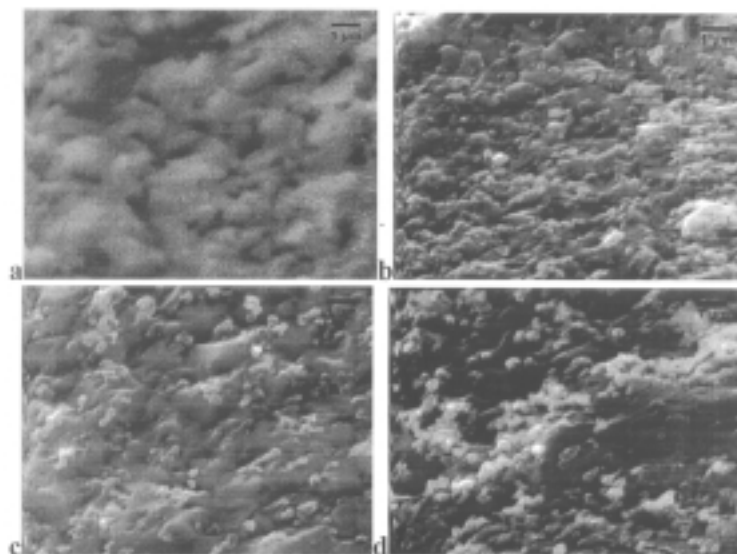


Figure 3. The morphology of Cu-TiO₂ coatings and particles themselves of anatase (a, b) and rutile (c, d). The concentration of particles in electrolyte-suspension ($\text{g} \cdot \text{dm}^{-3}$): a, c – 100, b, d – 200.

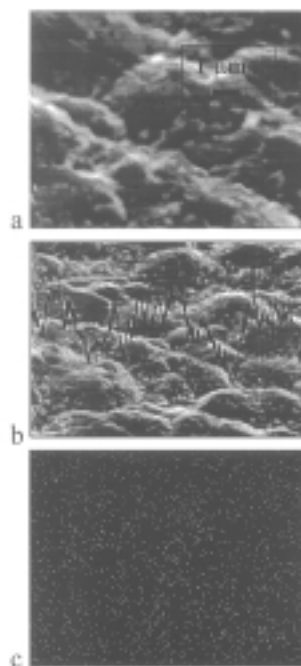


Figure 4. The morphology image of Cu-rutile coating and TiO₂ particles themselves from ageing suspension with concentration of nanometric size particles of rutile – $100 \text{ g} \cdot \text{dm}^{-3}$ (a). Secondary electron image of Cu-rutile composite at a depth of coating of $5 \mu\text{m}$ (b). The distribution of Ti in Cu-rutile coating (c).

crystalline structure of copper (Fig. 6; Compare B_{FWHM} values for copper standard with that for copper in composite coatings in Table 4).

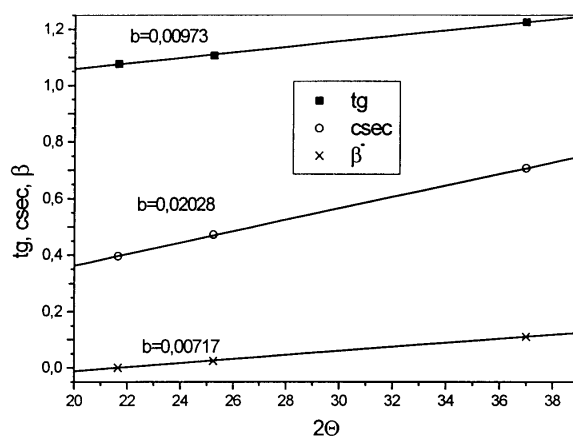


Figure 5. Dependence of tg, csec and β versus X-ray diffraction angle of obtained from aged suspension Cu-anatase coating (analogous to Nr 2 position in Table 4).

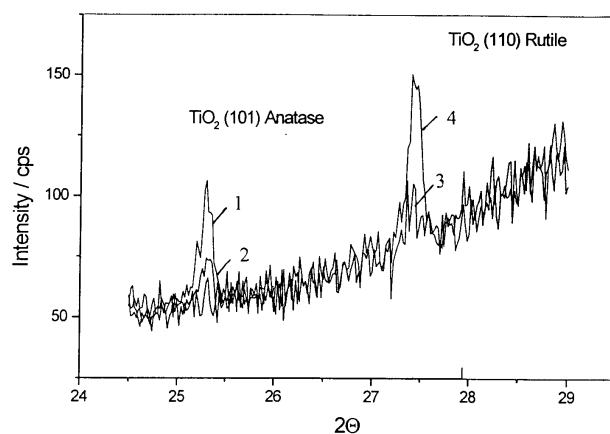


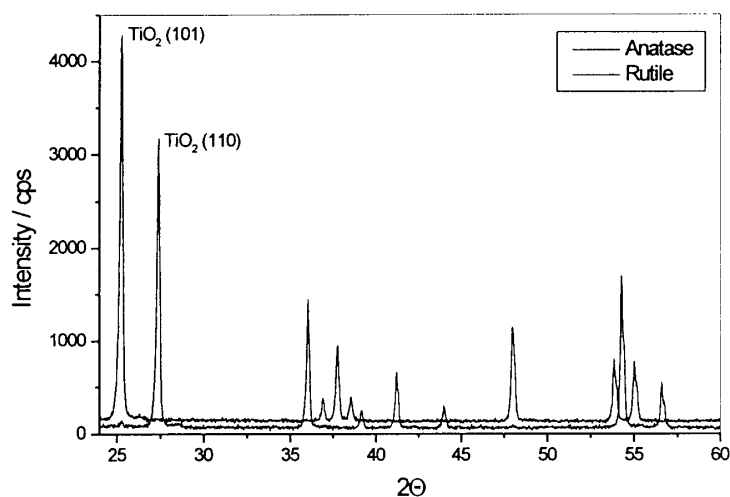
Figure 6. Diffractogram of Cu-TiO₂ coating with incorporated crystalline nanometric size particles of anatase and rutile. The coatings obtained from freshly prepared (curves 1, 3) and from aged suspensions (curves 2, 4). The thickness of coating in Figs. 5–7 – 25 μm .

An X-ray phase analysis of dry powders shows that the rutile powder used has $\sim 2.0\%$ of anatase phase (Fig. 7). Anatase powder has the same amount of unidentified crystalline phase. According to the Scherrer's formula the average size of TiO₂ crystallites in Cu-TiO₂ coatings may be as large as ≥ 250 nm.

At the same time it seems that the anatase suspension has higher stability. As can be seen from the appearance of the TiO₂ peaks on the XRD patterns and from the data in Table 4, columns 4 and 6, the crystalline state of anatase particles incorporated into matrix does not depend on suspension preparation time and on electrical charge quantity passed through the used suspensions ($Q = 67.2$ C) (Fig. 6, curves 1 and 2). Only after longer electrolysis ($Q = 134$ C) rutile particles has been detected in coating. The suspension with rutile powder structurized more complicated than that with anatase.

Table 4. Dependence of parameters of X-ray diffraction peaks on XRD patterns of Cu-TiO₂ coatings on suspension preparation time. Column 1: numbers 1, 3a–3c – coatings electrodeposited in freshly prepared suspension; 2,4 – in ageing suspension.

| Sample | XRD peak | d/nm | B _{FWHM} /deg | I _{max} /cps | I _{int} /(I/I _{max})×100 |
|--------------------------|---------------|---------|------------------------|-----------------------|---|
| 1 | 2 | 3 | 4 | 5 | 6 |
| 1. Cu-TiO ₂ | Cu (111) | 0.20877 | 0.190 | 12252 | 2327.8/100 |
| | Cu (200) | 0.18080 | 0.232 | 2875 | 669.9/28.8 |
| | Cu (220) | 0.12783 | 0.237 | 3610 | 973.6/41.8 |
| | Anatase (101) | 0.3518 | 0.153 | 47.4 | 7.56 |
| 2. Cu-TiO ₂ | Cu (111) | 0.20878 | 0.188 | 39173 | 7235.0/100 |
| | Cu (200) | 0.18079 | 0.240 | 2345 | 590.6/8.2 |
| | Cu (220) | 0.12782 | 0.341 | 1732 | 552.2/7.6 |
| | Anatase (101) | 0.3514 | 0.143 | 18.6 | 2.66 |
| 3 a. Cu-TiO ₂ | Cu (111) | 0.20877 | 0.193 | 15248 | 2951.8/100 |
| | Cu (200) | 0.18080 | 0.239 | 3042 | 757.7/25.7 |
| | Cu (220) | 0.12783 | 0.240 | 2944 | 826.0/28.0 |
| | Rutile (110) | – | – | – | – |
| 3 b. Cu-TiO ₂ | Cu (111) | 0.20876 | 0.192 | 7531 | 1453.6 |
| | Cu (200) | 0.18080 | 0.232 | 2980 | 695.2 |
| | Cu (220) | 0.12784 | 0.232 | 4144 | 1054.0 |
| | Rutile (110) | – | – | – | – |
| 3 c. Cu-TiO ₂ | Cu (111) | 0.20876 | 0.190 | 9078 | 1732.4/100 |
| | Cu (200) | 0.18079 | 0.235 | 3148 | 747.3/43.2 |
| | Cu (220) | 0.12783 | 0.240 | 2986 | 810.3/46.8 |
| | Rutile (110) | – | – | – | – |
| 4. Cu-TiO ₂ | Cu (111) | 0.20876 | 0.191 | 21003 | 4050.6/100 |
| | Cu (200) | 0.18075 | 0.247 | 2506 | 662.3/16.4 |
| | Cu (220) | 0.12782 | 0.345 | 1807 | 594.4/14.7 |
| | Rutile (110) | 0.32484 | 0.153 | 68.5 | 12.1 |
| 5. Cu standard | Cu (111) | 0.20881 | 0.191 | 8219 | 1526.9/100 |
| | Cu (200) | 0.18085 | 0.216 | 4069 | 839.9/55.0 |
| | Cu (220) | 0.12784 | 0.221 | 2353 | 488.4/32.0 |

**Figure 7.** Diffractograms of dry powder of anatase and rutile used to obtain copper composite coatings.

Thus, submicro/ or nanodispersed materials can be obtained electrochemically with an anatase phase of titania (Tables 1–4). Rutile is not as suitable as anatase under the same conditions.

CONCLUSIONS

Qualitative dispersion-hardened Cu-TiO₂ composite coatings can be obtained with the reproducible results only in a freshly prepared concentrated electrolyte-suspension. Submicro/ or nanodispersed materials can be obtained electrochemically with an anatase sort of titania. Rutile powder is not as suitable for this purpose as anatase. The average size of TiO₂ phase in Cu-TiO₂ coating may be as great as ≥ 250 nm.

The main condition of formation of the nanodispersed system is the structuring of freshly prepared concentrated suspension with the superhydrophilic particles of TiO₂ due to formation of equilibrium hydrosols of TiO₂. Avoiding their ageing and prolonged electrolysis is the guarantee of obtaining the composite coatings in aqueous suspension by the electro-codeposition of TiO₂ particles with copper.

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REFERENCES

1. Safranek W.H., *The Properties of Electrodeposited Metals and Alloys*. Orlando, Florida, (1980).
2. Hovestadt A.L. and Janssen I.J., *J. Appl. Electrochem.*, **25**, 519 (1995).
3. Steinhäuser S., *Die Technik*, **32**, 222 (1977).
4. Saifullin R.S., *Composite Coatings and Materials (in Russian)*, Moscow: Khimiya, (1977).
5. Medeliene V., *Surf. Coat. Technol.*, **154**, 104 (2002).
6. Socha R.P., Laajalehto K. and Nowak P., *Colloids and Surfaces. A: Physicochemical and Engineering Aspects*, **208**, 267 (2002).
7. Borodin I.N., *The Composite Coatings to a Machine Part Hardening (in Russian)*, Moscow: Mashinostroyeniye, (1982).
8. Medeliene V., Leinartas K. and Matulionis E., *Electrochemical Approach to Selected Corrosion and Corrosion Control Studies. (First Joint EFC/ISE Symposium 1999)*. Eds. P.L. Bonora, F. Deflorian. Publication No 28 in European Federation of Corrosion Series. London, Institute of Materials, 193 (2000).
9. Greco V.P. and Baldauf W., *Plating*, **55**, 250 (1968).
10. Nwoko V.O. and Shreier L.L., *J. Appl. Electrochem.*, **3**, 137 (1973).
11. Shibano T. and Otsubo H., *J. Metal Finish. Soc. Japan*, **22**, 513 (1972).
12. Steinhäuser S., *Galvanotechnik*, **92**, 940 (2001).
13. Fransae J.-P., Leunis E., Hirato T. and Celis J., *J. Appl. Electrochem.*, **32**, 123 (2002).
14. Boven H.K., *Mater. Sci Eng.*, **44**, 1 (1980).
15. Barringer E.A. and Boven H.K., *J. Am. Ceram. Soc.*, **65**, C-1999 (1982).
16. Fegley B. Jr., Barringer E.A. and Bowen H.K., *J. Am. Ceram. Soc.*, **67**, C-113 (1984).
17. Pavlova-Veriovkina O.B., Politova E.D. and Nazarov V.V., *Russian J. Colloids*, **61**, 389 (1999).
18. Fu X. and Qutubuddin S., *Colloids Surfaces*, **179**, 65 (2001).

19. Akiyama T., Miyazaki A., Sutoh M., Ichinose I., Kunitake T. and Yamada S., *Colloids Surfaces*, **169**, 137 (2000).
20. Ichinose I., Kawakami T. and Kunitake T., *Adv. Mater.*, **7**, 535 (1998).
21. Harada T., Matsuoka H., Ikeda T. and Yamaoka H., *Colloids Surfaces*, **174**, 79 (2000).
22. Chhabra V., Pillai V., Moshra B.K., Morrone A. and Shah D.O., *Langmuir*, **11**, 3307 (1995).
23. Rattanakawin C. and Hogg R., *Colloids Surfaces*, **177**, 87 (2001).
24. Jean J. H. and Ring T.A., *Colloids Surfaces*, **29**, 273 (1988).
25. Short Chemical Encyclopaedia, Moscow: Soviet. Encyclopaedia. **V** 187 (1967).
26. Jaskuła M., 50th Annual ISE Meeting Abstracts. Pavia (Italy), vol. 2, 277 (1999).
27. Briggs D. and Sich M.P. (Eds), *Practical Surface Analysis by Auger and X-Ray Photoelectron Spectroscopy*, Chichester: Wiley, (1983).
28. Wagner C.D., Rigss W.M., Davies L.E., Moulder J.F. and Muilenberg G.E., *Handbook of X-Ray Photoelectron Spectroscopy*, Minnesota: Perkin-Elmer Corp., (1979).
29. Barret C.S. and Massalski T.B., *Structure of Metals. Crystallographic Methods. Principles and Data*. Oxford, New York: Pergamon Press, (1980).
30. Voyutskiy S.S., *Course of colloidal chemistry (in Russian)*. Moscow: Khimiya, 229 (1975).
31. *Hydrated oxides of IV and V Groups of Elements*. Ed. by Y.V. Yegorov, Moscow: Nauka, **I**, 5 (1986).
32. Medeliene V., Jasulaitiene V., Bikulčius G., Matulionis E. and Jaskuła M., *Book of Abstracts of the 5-th International Summer School-Conference: Advanced Materials and Technologies*, Palanga, Lithuania, 25-29 August 2003. Kaunas: Technologija 21 (2003).
33. *Chemistry*, R. Chang, A book, New York: McGraw-Hill, Inc., (1991).
34. West A.R., *Solid State Chemistry and its Application*, A Book, University of Aberden, Wiley, (1984).