## **CORRELATION COEFFICIENTS AND MECHANISM USING TG DATA**

**LEO REICH and S.S STIVALA \*** 

*Deparhnent of Chemistry and Chemical Engineering, Stevens Institute of Technology, Hoboken, N.J. 07030 (US A.)* 

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#### **ABSTRACT**

**The use of linear correlation coefficients to ascertain mechanism from TG data was shown to be unsatisfactory This** is **in agreement with results reported by others who also indicated the necessity of using additional Isothermal techniques for determinmg mechanism.** 

**Two methods, Reich-Stivala (R-S) and double-log (D-L), were employed to distinguish one mechanism from among 15 theoretical possibilities for heterogeneous solidstate reactions using theoretical TG data. With a certain degree of accuracy oi TG data and for relatively large** *E/RT* **values (above 18). the R-S method was shown to be superior to the D-L method and a good indicator of a most probable mechanism. In this respect, the utilization of supplemental isothermal techniques may not be necessary when the R-S method is used under certain conditions.** 

#### **INTRODUCTION**

**The linear correlation coefficient (r) has been employed by various workers as an adjunct in the estimatron of kinetic parameters, i.e., activation**  energy  $(E)$  and reaction order  $(n)$  from TG data. In this respect, Fong and **Chen [l] attempted to determine which of 17 possrble expressions for heterogeneous decompositions best fit their TG data for the thermal dehydroxylation of magnesium hydroxide by using r values. These authors found that it was very drfficult to determine the probable mechanism (and hence values of E and n) based on r values since at least half of the expressions tested gave values of r above 0.995. Other workers found similar results. Thus, Heide and co-workers [2,3] found that linear correlation coefficients were not satisfactory for ascertaining the kinetic mechanism from among various theoretically possible mechanisms postulated. Cnado and Morales**  [4,5] and Dharwadkar et al. [6] also reported that high *r* values do not **necessanly lead to the establishment of mechanism using TG data. These workers [4-6] were in agreement that supplemental isothermal runs were also necessary in mechanism studies. Thus, Dharwadkar et al. [S] studied the decomposition of cadmium carbonate in argon by TG techniques. The TG curves obtained were analyzed using a combination of the Coats-Redfem** 

**<sup>\*</sup> To whom correspondence should be addressed.** 

*[7]* and Avrami-Erofeyev [8,9] expressions, 1.e.

$$
\log\left(\frac{g(\alpha)}{T^2}\right) = -\frac{E}{RT} + \log\left(\frac{ARP}{(RH)E}\right) \tag{1}
$$

where,  $P = 1 - 2 X + 6 X^2 - 24 X^3 + 120 X^4 + \cdots$ ;  $X = RT/E$ ;  $g(\alpha) = F \int d\alpha /$ f(a)]; T = temperature (K); A = frequency factor; (RH) = heating rate;  $\alpha$  = fractional conversion;  $R = gas$  constant. In eqn. (1),  $g(\alpha)$  was set equal to  $[-\log (1-\alpha)]^{1/\nu}$ , where N could equal 1, 2 or 3. Dharwadkar et al. [6] found that plots of eqn. (1) (P assumed to be constant) were linear for all three values of N and that the *r* values obtained were almost unity (0.997-0.998). However, addltlonal isothermal runs were carried out and clearly indicated that the value of  $N$  should be 3.

The preceding results with regard to r values may not be surprising when it is considered that the r value 1s only a relative term. The square of *r* is proportional to the ratio, explained data variation to total data variation, when least squares analysis of data is used. Thus, while a high  $r$  value indicates a good fit of data to a least squares line, it does not necessarily mean that an espression which afforded this value is more likely than one which gave a somewhat lower *r* value.

The purpose of this paper is to extend a method previously reported by Reich and Stivala  $(R-S)$  [10,11] to three mechanisms and, based on these cases, ascetiam whether or not it is necessary to supplement TG techniques with isothermal techniques in order to establish a probable mechanism (and consequently values of kinetic parameters) The  $R-S$  method was initially applied to TG data (presumably obtained from heterogeneous decompositions) utilizmg the well-known espression for homogeneous kinetics

$$
\frac{d\alpha}{dT} = \frac{A}{(RH)} \exp\left(-\frac{E}{RT}\right) (1-\alpha)^n
$$
 (2)

Despite its apparent limitations, eqn. (2) has been employed by numerous workers for analyzing TG data (it is theoretically valid for heterogeneous reactions with values of  $n = 0$ , 1/2, 2/3, 1) In this paper, the R-S method and a double-log (D-L) method will be applied to 15 kinetic functions which are mechanistically possible for heterogeneous reactions.

## **SOME THEORETICAL BACKGROUND**

From eqn.  $(1)$ , the following eqn.  $(3)$  can readily be obtained. In this equation, P terms are not included. At relatively high *E/RT* values, P is approximately constant; further, P ratios are close to unity. However, at relatively low  $E/RT$  values this is no longer true, so that eqn. (3) becomes less accurate and/or invahd, depending upon the *E/RT* value. General!y, the  $E/RT$  value should be greater than 18.

$$
\log \left[ \frac{g(\alpha_1)}{g(\alpha_2)} T(1) \right] U(1) = \frac{E}{R}
$$
\nwhere,  $T(1) = (T_2/T_1)^2$ ;  $U(1) = T_1 T_2 / (T_2 - T_2)$ . From eqn. (3), the double-

log expression can be derived

$$
\frac{\log[K_{R}G(\alpha_{1})]}{\log[K_{R}G(\alpha_{2})]} (TR) = Z_{1}
$$
\n(4)

where,  $K_{\rm R} = T_{\rm R}^{2}/g(\alpha_{\rm R}); T_{\rm R}$  and  $\alpha_{\rm R}$  denote an arbitrary reference temperature and its corresponding conversion, respectively;  $G(\alpha_1) = g(\alpha_1)/T_1^2$ ,  $G(\alpha_2) =$  $g(\alpha_2)/T_2^2$ ;  $TR = T_1 (T_R - T_2)/T_2(T_R - T_1)$ . In eqn. (4),  $Z_1$  should theoretically be equal to unity.

Equations  $(3 \text{ and } 4)$  will be applied to the following 15 possible kinetic functions. As previously indicated in the R-S method  $[10,11]$ , the most probable function will be that whose  $E/R$  and/or  $Z_1$  values have the lowest mean deviations (MD).

# **TESTING THE R-S AND D-L METHODS**

Fifteen theoretically possible kinetic functions for describing solid-state processes were tested. In the folIowing are listed, in order, the function number and corresponding expression for  $g(\alpha)$ 

1, 
$$
\alpha
$$
; 2,  $\alpha^2$ ; 3,  $\alpha^{1/2}$ ; 4,  $\alpha^{1/3}$ ; 5,  $\alpha^{1/4}$ ; 6,  $1 - (1 - \alpha)^{1/2}$ ; 7,  $1 - (1 - \alpha)^{1/3}$ ;  
\n8,  $-\log(1 - \alpha)$ ; 9,  $[-\log(1 - \alpha)]^{2/3}$ , 10,  $[-\log(1 - \alpha)]^{1/2}$ ;  
\n11,  $[-\log(1 - \alpha)]^{1/3}$ ; 12,  $[-\log(1 - \alpha)]^{1/4}$ : 13,  $\alpha + (1 - \alpha) \log(1 - \alpha)$ ;  
\n14,  $1 - 2\alpha/3 - (1 - \alpha)^{2/3}$ : 15,  $[1 - (1 - \alpha)^{1/3}]^2$ .

In the preceding, Nos. 1,  $3\rightarrow 5$  denote a power law mechanism, 6 and 7, a contracting geometry mechanism;  $8-12$ , Avrami-Erofeyev expressions (nucleation):  $2, 13$  and  $14$ , one-dimensional diffusion, two-dimensional (cyhndncal symmetry) diffusion and three-dimensional (sphencaI symmetry) diffusion (Ginstling-Brounshtein equation), respectively; 15, three-dimensional (spherical symmetry) diffusion (Jander equation).

The 15 expressions were tested with three sets of theoretical  $\alpha - T(K)$ data generated by means of eqn. (1) and various kinetic parameters (this derived data as well as that which follows was obtained by means of a computer; see ref. 12 for a description of a computer program involving the  $R-S$ method). Derived  $\alpha - T$  data was obtained using function Nos. 7, 10, and 15 along with various parameters and eqn.  $(1)$ . In this equation, P was calculated to the 24th power, and  $E/RT$  values were greater than 18. When  $E/RT$  values are less than ca. 18, the utilization of eqn. (3) (and eqn. (1)) becomes moot.

In the first set of data (DS-1),  $E/R = 23500$  cal mole<sup>-1</sup>, log  $AR/(RH)$   $E =$ 10,  $g(a) = 1 - (1-a)^{1/3}$ , to yield the following values of  $\alpha$  and  $T(K)$ , respec**tively:** 0.0606723, 860; 0.0842361, 870; 0.115733, 880; 0.157228, 890; 0\_2l(i~70, 900; 0.279156, 910; 0.363471, 920; 0.464322, 930; 0.579673, 940; 0.703513, 950; 0.824309, 960; 0.924655, 970. For **the second set of**  data (DS-2),  $E/R = 15000$  cal mole<sup>-1</sup>, log  $AR/(RH)$   $E = 11$ ,  $g(\alpha) = [-\log$  $(1 - \alpha)$ ]<sup>1/2</sup>, to yield the following values of  $\alpha - T(K)$ , respectively.

**0.00454777, 570; 0.01200787, 580; 0.0305348, 590; 0.0743169, 600; 0.170412, 610; 0.355785, 620; 0.635114, 630; 0.895963, 640; 0.992717, 650; 0.999973, 660. For the third, and final, set (DS-3) of theoretical**   $\alpha - T(K)$  data generated,  $E/R = 15000$ , log  $AR/(RH)$   $E = 4$ ,  $g(\alpha) = [1 (1 - \alpha)^{1/3}$ <sup>2</sup>, to vield: 0.0719718, 620; 0.106950, 640; 0.154388, 660; **0.216610, 680; 0.295332, 700; 0.390990, 720; 0.501860, 740; 0.623082, 760; 0.745873, 780; 0.857461, 800; 0.942786, 820. Typical results obtained are listed in Table 1 for DS-1.** 

**From Table 1, it is evident that the most probable mechanism involves**  function No. 7 and  $E/R = 23439 \pm 3$ , as anticipated. The only other possible **mechanism that came reasonably close involved the Jander diffusion expres**sion (No. 15). These results are based on an accuracy of  $\alpha$  to six significant figures (s.f.). When this accuracy was reduced to  $4$  s.f., MD ( $7$ ) = 13 and MD  $(15) = 44$  for the R-S method. However, at this accuracy of  $\alpha$ , the D-L method failed, i.e. for the D-L method, MD (7) =  $1.24 \times 10^{-4}$  and MD (15) = **1.17**  $\times$  10<sup>-4</sup>. When  $\alpha$  was reduced to 3 s.f., for the R-S method, MD (7) = **126 and MD (15) = 261. Thus, whereas the R-S method could distinguish**  mechanism No. 7 from 14 other mechanisms down to an accuracy of  $\alpha$  to 3 s.f., the D-L method could not distinguish between Nos. 7 and 15 at  $\alpha$  to 4 **s-f. It may also be noted here that least squares plots were carried out using**  eqn. (1), DS-1, and the  $g(\alpha)$ 's for Nos. 7, 14, and 15. The following values of  $E/R$ ,  $\log AR/(RH)E$ , and r were obtained, respectively: 23428, 9.85,  $-0.9998$ ; **45606, 31.3, 0.9993; 48683, 35.3, -0 9998. From the preceding, it is vir-**

Function No.	Method			
	$R-S$		$D-L^a$	
	$E/R$ (cal mole <sup>-1</sup> )	MD	$Z_{1}$	MD
	19534	2713	1.081	0.0476
2	40889	5379	1075	0.0429
3	8857	1381	1.098	0.0606
4	5 298	936	1 1 2 4	0.0841
$\overline{5}$	3519	714	1.174	0.135
6	22374	775	1.017	0.00859
7	23439	3	1 000	0.00000184
8	25752	1740	0972	0.0129
9	16561	1144	0.972	0.0133
10	11966	846	0.971	0.0137
11	7371	548	0.969	0.0145
12	5073	400	0.967	0.0155
13	44 371	3116	1 0 3 8	00219
14	45 797	2082	1.023	00128
15	48 697	44	1.000	0.00000339

**TAB1.E 1** 

**Values of average** *E/R* **and MD and Z1 and MD for DS-1 by R-S and D-L methods** 

 $T_R = 970$ ,  $\alpha_R = 0.924655$ .

**tually impossible to predict the most probable mechanism based on r values, as previously contended.** 

**From the DS-2 data, values obtamed from function Nos. S-12 were of a**   $s$ imilar order of magnitude. Thus, for  $\alpha$  to 6 s.f., the R-S method yielded the following values for  $E/R$  and MD:  $E/R$  (8) = 31134 ± 35,  $E/R$  (9) =  $20349 \pm 10$ ,  $E/R$   $(10) = 14957 \pm 3$ ,  $E/R$   $(11) = 9565 \pm 15$ ,  $E/R$   $(12) =$  $6869 \pm 21$ . However, at this level of accuracy of  $\alpha$ , the D-L method failed, **e.g., MD** (8) =  $2.12 \times 10^{-4}$ , MD (10) =  $2.27 \times 10^{-4}$ . When  $\alpha$  was reduced to 4 s.f., mechanism No. 10 still prevailed in the R-S method. However, at  $\alpha$  to 3 **s.f., the R-S method failed, e.g., MD (10 = 48 and MD (12) = 25 (It may be noted here that although function No. 12 appears to be the most probable mechanism** by the R-S method, at an  $\alpha$  of 3 s.f., the lowest  $E/RT$  value **would be less than 10, making this mechanism suspect).** 

**Finally, from the DS-3 data, values obtained for function No. 15 were reasonably close only to values obtamed for the similar function No. 7.**  Thus, at  $\alpha$  of 6 s.f., the R-S method yielded  $E/R$  (15) = 14943  $\pm$  7 and  $E/R$  $(7) = 6761 \pm 48$ ; for the D-L method, MD  $(15) = 2.93 \times 10^{-6}$  and MD  $(7) =$  $6.33 \times 10^{-5}$ . When  $\alpha$  was reduced to 4 s f., for the R-S method, MD (15) = **9 and MD (7) = 48, while for the D-L method, MD (15) = 9.96**  $\times$  **10<sup>-5</sup> and** MD (7) =  $1.04 \times 10^{-4}$ . Thus, for  $\alpha$  to 4 s.f., both methods afforded the mechanism anticipated. However, at an  $\alpha$  of 3 s.f., for the R-S method, MD  $(15) = 84$  and MD  $(7) = 63$ . The R-S method now fails (the  $E/RT$  value for **mechanism No. 7 is less than 9, which should make this mechanism suspect).**  However, the D-L method still applies, i.e., MD  $(15) = 1.80 \times 10^{-3}$  and MD  $(7) = 2.01 \times 10^{-3}$ .

From the preceding, it can be stated, generally, that the R-S method is more reliable than the D-L method. Thus, for an  $\alpha$  of 4 s.f., the R-S method **IS valid for all the cases tested, whereas the D-L method IS not. Below 4 s-f., the R-S method may not be reliable and additional techniques (e.g. isothermal) may be necessary in order to distinguish a mechanism. As previously noted, when the R-S method 1s employed, the function indicated should possess a minimum value of** *E/RT* **greater than 18, and the mmlmum MD obtamed should not be of relatively large magmtude; otherwxe, the function should be considered suspect, and other techniques (e.g., isothermal) should be utilized. Also, the functions listed are not all-inclusive, e.g., the Prout-Tompkins function was omitted. Conclusions regarding a correct mechanism**  should be confirmed, if possible, by means of X-ray diffraction and/or **microscopy. Lastly, in the previous treatment, temperatures have been tacitly assumed to be accurate** 

**Some other methods proposed for ascertaining a mechanism using dynamic thermogravimetry will be mentioned. Thus, Criado [13] proposed a method whereby a series of master curves were devised m order to readily determine the mechanism m the thermal decomposition of solids from differential thermogravimetry (DTG) data. However, this method requires accurate measurements of steep slopes and can only distinguish 6 of the 15 functions previously listed (the remammg functions yielding duplicate or identical reduced rate functions of conversion). Also, Criado et al. [14] esplored the possibility of distinguishing theoretical mechanisms, using TG**  data, from the fraction of solid reacted at maximum reaction rate  $(\alpha_M)$ . **These workers concluded that determinatron of order of thermal decomposi**tion of solids by means of  $\alpha_M$  values would lead to misinterpretation of **results. Thus, they could find no important differences among corresponding**  theoretical values of  $\alpha_M$  arrived at using various mechanisms, e.g., Jander dif**fusion mechanism and 2/3-order reactions (cf. function Nos. 7 and 15 previously listed). Gallagher and Johnson [15] also attempted to distinguish theo**retical kinetic rate laws. They used, as a criterion for the most acceptable **rate law, a mirumum standard deviation obtained from the least squares fit of the best straight line. Others [16,17] used an approach similar to that of Gallagher and Johnson and found they could distinguish individual model equations, with statistical slgmficance, from among 11 theoretically possible**  expressions, using theoretical  $\alpha - T$  data. Satava and Skvara [18] proposed **master curves to ascertain mechanism and kinetic parameters from TG data. Thus, when a particular plot coincided with a certain master curve, the most probable mechanism and E could be determined. Further manipulations of the graphs allowed for the estimation of A.** 

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