EFFECT OF TEMPERATURE AND CHAIN LENGTH OF THE ALKANE ON H^E of 2-METHOXYETHANOL+ALKANE MIXTURES

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SUMMARY

Esperimental results of the composition dependence of the molar excess enthal- py H^E are reported for binary mixtures of some alkanes with 2-methoxyethanol at 323, 348 and 373 K and pressures up to alkane molecule on HE 25 bar. The effect of size and shape of the and the dependence of $\mathtt{H}^\mathtt{L}$ on temperature are discusse The experimental results can be described with a modified form of the UNIFACmodel combined with an association term taking into account the H-bonding of 2-methoxyethanol. The MUNIQUAC-RAS-model used is explained; its system-specific parameters vary systematically with temperature and with size and shape of the alkanes mixed with 2-methosyethanol.

INTRODUCTION

Fiuid phase equilibria and thermodynamic excess properties of mistures consisting of a selfassociating component and an inert solvent can be described most adequately by theoretical models which account for multiple association due to hydrogen bonding $(ref. 1-4)$. These models, however, so far are not flexible enough to describe different properties with the same set of system-specific model parameters (ref. 5, 61. Therefore good experimental data are required at varying state conditions for many more appropriate mistures in order to test the applicability and to improve theoretical models for predicting the thermodynamic behaviour of fluids and their mixtures. Without reliable predictions proper design of seperation processes is impossible.

In this paper experimental results of H^E are reported for binary mixtures of 2-methosyethanol with the following alkanes: n-herane, n-heptane, n-octane, n-decane and 2,2,4-trimethylpentane. Using the MUNIQUAC-model proposed by Bijl, de Loos and Lichtenthaler (ref. 7) combined with the linear association (RAS) model according to Renon and Prausnitz (ref. 8) the dependence of H^E on composition and temperature can be represented very well. An empirical correlation of the systemspecific model parameters could be developed allowing the calculation of H^{E} at any

state condition within the ranges investigated. 2-methosyethanol is a polar, selfassociating solvent widly used in industry and therefore such calculations are also of interest for practical application.

EXPERIMENTAL

Apparatus

The quasi-isothermal flow calorimeter (Model 7501 from HART SCIENTIFIC, Utah, USA) has been described elsewhere (ref. 6, 9) and therefore only a short summary of the experimental procedure is given here.

Fig.1 shows schematically the set-up of the calorimeter. The two pure components

Fig. 1. Schematic diagram of the flow calorimeter. $P_{1,2}=VARIAN-pumps$, FC=flow cell, OB=thermostatted oil bath H=hood, W=waste box, $\mathcal{V}_1,\! \mathcal{V}_2\! =\! \mathcal{V}$ alves, A=autoclave B=nitrogen bomb.

to be mised are pumped continuously by two precision high pressure syringe pumps $P_{1,2}$ (VARIAN 8500) into a mixing coil sitting in a flow cell FC. FC is immersed in an oil bath OB thermostatted at the temperature the mixing process is taking place. A Peltier cooler removes with constant rate energy from FC and a pulsed control-heater compensates for this energy and for the energy liberated (exothermicl or absorbed (endothermic) by the mixing process. In this way the temperature of the flow cell and consequently that one of the mixture formed are maintained at the constant temperature of OB (quasi-isothermal operation). The mixture leaves OB and flows into an autoclave A, which contains nitrogen kept at that pressure the measurement is performed. The volume of A is so large (\sim 2000 cm³) that during one measurement

the change in pressure due to the decrease in volume by entering liquid mixture (\sim 30 cm³) usually is neglegible. Through valve V₁ the liquid mixture can be removed from A after each measurement.

The energy supplied by the control-heater before (or after) and during a mixing process keeping the temperature of FC constant is a direct measure of the energy of mixing. Knowing the volumetric flowrates delivered, the molar masses and densities of the pure components the mole fraction of the mixture obtained in the mixing coil can be calculated. Just as well the corresponding molar excess enthalpy can be calculated from these data and the measured change in heating power before and during the continuous mixing process at the temperature and pressure the esperiment is performed. Measurements with various flow rates give different compositions of the mixture formed and therefore the dependence of $\mathtt{H}^\mathbf{E}$ on mole fraction can be determined. The calorimeter described can be used in the temperature range $20-200^{\circ}$ C for pressures up to 150 bar.

Results and Discussion

The substances used in this work were obtained from standard laboratory supply sources and the purity was at least 99.5 Vol%. They were used without further pu rification. However, 2-methoxyethanol was dried with molecular sieve and kept under nitrogen in order to avoid oxidation.

The results of H^E at 323, 348 and 373 K for all mixtures investigated are given in Tables l-3 respectively. The pressure usually is 1 bar except at the higher temperatures where the measurements had to be performed at pressures up to 25 bar for some of the mixtures in order to avoid the formation of a vapour phase. The actual pressure is always given in brackets in the headings in Tables 1-3. Some measurements performed at 150 bar revealed that the effect of pressure on H^E at the temperatures and for the mixtures investigated is rather small. At 15 bar and 25 bar the effect is below 0.5% in the entire mole fraction range and therefore it can be neglected within the estimated inaccuracy of the experiments: \pm 2% in H^E and $+5*10^{-4}$ in the mole fraction.

The H^{E} -values are for all mixtures positive (endothermic mixing). Figs. 2-4 show the composition dependence for some selected mixtures at various temperatures. In all cases it was possible to represent the dependence of H^E on mole fraction with the Redlich-Kister Equation:

$$
H^{E}(x) = x(1-x) \sum_{m=0}^{n} A_m (2x-1)^m
$$
 (1)

264

with x being the mole fraction of 2-methoxyethanol. Up to 7 coefficients A_m were necessary to give such a good description of $\rm H^\Sigma$ as shown in Figs. 2-4. The Redlich Kister constants A_m at the various temperatures together with the standard deviation $\delta(H^E)$ obtained by the method of least squares with all data points weighed equally are given in Table 4.

x	H^E J *mol $^{-1}$	x	H^E $J*_{mol}^{-1}$	
		x 2-methoxyethanol + $(1-x)$ C ₆ H ₁₄ (1 bar)		
0.0761	767	0.5798	1327	
0.1308	992	0.6222	1286	
0.1414	1037	0.6986	1184	
0.2030	1192	0.7671	1050	
0.2478	1253	0.8317	866	
0.3541	1353	0.8917	631	
0.4516	1368	0.9479	341	
0.5405	1344			
		x 2-methoxyethanol + $(1-x)$ C ₇ H ₁₆ (1 bar)		
0.1102	929	0.6501	1375	
0.1445	1040	0.6990	1326	
0.2709	1351	0.7223	1299	
0.3824	1453	0.7879	1126	
0.4816	1466	0.8479	932	
0.5703	1453	0.9028	685	
0.5978	1432	0.9533	380	
		x 2-methoxyethanol + $(1-x)$ 2,2,4-trimethylpentane (1 bar)		
	735		1401	
0.0651 0.1040	963	0.5108 0.5987	1335	
0.1222	1036	0.6762	1274	
0.1596	1155	0.7451	1148	
0.1728	1188	0.8068	1008	
0.2946	1399	0.8624	828	
0.3170	1418	0.9038	643	
0.3852	1457	0.9126	595	
0.4104	1439	0.9583	317	

TABLE 1. Experimental results of the molar excess enthalpy for 2-methoxyethanol + alkane mixtures at 323.15 K

TABLE 2. Experimental results of the molar excess enthalpy for 2-methoxyethanol + alkane mixtures at 348.15 K

x	H _E	x		x	
			x 2-methoxyethanol + $(1-x)$ C ₆ H ₁₄	(25 bar)	
0.0407	555	0.5502	1938	0.7943	1242 859
0.1912 0.3246	1655 1976	0.6234 0.7129	1778 1554	0.8688 0.9371	402
0.4435	2040				
			x 2-methoxyethanol + $(1-x)$ C ₇ H ₁₆	$(15$ bar)	
0.0364 0.1056	529 1248	0.3687 0.4421	2167 2184	0.7350 0.8119	1642 1319
0.1704	1662	0.5521	2084	0.9433	485
0.2605	2001	0.6490	1897		
			x 2-methoxyethanol + $(1-x)$ C ₈ H ₁₈ (1 bar)		
0.0976 0.1859	1233 1827	0.5253 0.5780	2242 2166	0.8274 0.8915	1356 969
0.3394	2253	0.6727	1953	0.9487	516
0.4065	2312	0.7550	1679		
			x 2-methoxyethanol + $(1-x) C_{10}H_{22}$ (1 bar)		
0.1148 0.2149	1422 2049	0.5135 0.6215	2437 2264	0.7870 0.9079	1718 969
0.3030	2346	0.7113	2010	0.9568	507
0.3811	2463				
	x 2-methoxyethanol + (1-x) 2,2,4-trimethylpentane (10 bar)				
0.1603 0.2957	1589 2049	0.5999 0.6773	1980 1801	0.8630 0.9130	1021 689
0.4117	2161	0.7461	1582	0.9585	327
0.5121	2110	0.8076	1309		

TABLE 3. Experimental results of the molar excess enthalpy for Z-methoxyethanol + alkane mixtures at 373.15 K

TABLE 4. Coefficients A_m/J^* mol⁻¹ and standard deviations $\delta(H^{\omega})$ for least-squares representation of H-/J*mol – for 2-metho thanol $+$ alkane by eqn. (1) at 323.15, 348.15 and 373.15 K.

323.15		K

348.15 K

353.15 K

As shown in Fig. 2 at 373 K the endothermic H^{E} -values are increasing with increasing number of C-atoms in the n-alkane, i.e. with increasing chain length. Analogous behaviour is found at 323 K and 348 K.

Fig. 2. Effect of chain length of the n-alkane component on H^E at 373.15 K for x 2-methoxyethanol+(1-x) alkane: Δ n-hexane at 25 bar, \Box n-heptane at 15 bar, $*$ n-octane at 1 bar, O n-decane at 1 bar. Curves calculated with eqn. (1) using coefficients from Table 4.

For the mixture with the branched alkane the H^{E} -values are less endothermic with respect to the values for the mixture with the corresponding n -alkane. This is shown in Fig. 3, where the dependence of H^{E} on mole fraction at 373 K for the mixture with 2,2,4-trimethylpentane is nearly the same as the one for the mixture with

n-heptane. Branching makes an alkane molecule more compact and it is behaving like a shorter n-alkane.

Fig. 3. Effect of branching of the alkane component on H^E at 373.15K for x 2-methoxyethanol+(1-x)alkane: \Box n-heptane at 15 bar, \Diamond 2,2,4-trimethylpentane at 10 bar, $*$ n-octane at 1 bar. Curves calculated with eqn. (1) using coefficients from Table 4.

A similar effect of branching has been observed for the upper critical solution temperature (UCST) of the liquid-liquid-equilibria which 2-methosyethanol+alkane mixtures show at lower temperatures (ref. 7). The shorter and the more branched an alkane molecule is the lower is UCST. The mixtures of 2-methoxyethanol with n -heptane and 2,2,4-trimethylpentane respectively nearly have the same UCST at 1 bar.

In Fig. 4 the strong effect of temperature on H^E is shown, as an example, for the mixture 2-methoxyethanol+n-hexane. Changing the temperature from 323 K to 373 K changes the maximum of H^E from about 1370 J*mol⁻¹ to about 2040 J*mol⁻¹. This behaviour is typical for mixtures of an associating and an inert component and it is due to the change in the difference of the number of the H-bonds the associating component forms in its pure state and in the mixture (ref. 10, 111. Analogous behaviour is observed for all the other mixtures investigated,

Fig. 4. Effect of temperature on H^E for x 2-methoxyethanol+(1-x) n-hexane: -..--- 323.15 K, 1 bar; ---348.15 K, 15 bar; .U.s..373.15 K, 25 bar. Curves calculated with eqn. (I) using coefficients from Table 4.

Fig. 5. Comparison between calculated and experimental H^{E} -values for x 2-methoxyethanol+(1-x) n-hexane at various temperatures: --- MUNIQUAC-RAS model

 $-$ Redlich-Kister fit, Δ experiment.

The temperature dependence of $\Delta U_{12} = \Delta U_{AB}$ and $\Delta U_{21} = \Delta U_{BA}$ is shown in Fig. 6 for the mixtures with n-alkanes. Both parameters vary systematically when going from n-hexane to n-decane. Whereas ΔU_{12} increases with increasing number n of C-atoms of the n-alkane ΔU_{21} decreases in the entire temperature range covered. At a particular temperature this dependence on n can be very well represented by the following equations:

Just so as H-bonding of the 2-methoxyethanol molecules determines the dependence of H^E on temperature it is also responsible for the relatively large endothermic H $^{\rm E}-$ values obtained. At a given temperature, however, the dependence of H $^{\rm E}$ on the chain length and the degree of branching can be explained by the existence of some kind of short range order (CMO) in liquids with chain-like molecules (ref. $12-14$). The CMO (Correlation of Molecular Order) can be interpreted as a packing effect between groups of segments of different n-alkane molecules, being the more pronounced the longer the chain-like molecule is. Upon mising with a compact molecule like 2-methoxyethanol the CM0 is destroyed gradually, depending on the composition of the mixture. The energy associated leads to an endothermic contribution to H^E , which increases with increasing CMO. That is the reason why, as shown in Fig. 2, H^{E} increases stronger with increasing chain length than expected from the changes in the intermolecular interactions when going from n-hesane to n-decane. In n-hexane CM0 is less pronounced as in n-decane and therefore the corresponding endothermic H $^{\rm E}$ -contribution is smaller for the mixture with n-hexane than for the mixture with n-decane. Due to steric hinderance pure branched alkanes show only little or no CMO. Therefore for mixtures of branched isomeric alkanes smaller H^{E} -values are observed than for the mixture with the corresponding n-alkane. The CMO-contribution becomes smaller the more branched an alkane molecule is and for that reason, as shown in Fig. 3, H^E for the mixture with 2,2,4-trimethylpentane is smaller than H^E for the mixture with n-octane.

CALCULATIONS

The MCNIQUAC-RAS model

Models for calculating thermodynamic excess properties of mixtures containing associating components usually express these properties as the sum of a physical and a chemical contribution. The physical contribution depends on the dispersion forces between the various molecules whereas the chemical contribution results from the association by H-bonding (ref. 1, 2, 11). This aproach is also used in this work for H^E :

$$
H^{E} = H^{E}_{phys} + H^{E}_{chem}
$$
 (2)

For $H^E_{\ \ \ \text{phys}}$ a <u>m</u>odification of the <u>UNIQUAC</u>-model is chosen. This socalled MUNIQUAC-model was developed by Bijl, de Loos and Lichtenthaler especially for correlating liquid-liquid-equilibria of binary mixtures of 2-methoxyethanol with various alkanes (ref. 7). As these are the same mixtures as investigated in this work it therefore was obvious to combine this model with a proper expression for H_{chem}^E . For H_{chem}^E the real-associated-solution (RAS)-model proposed by Renon and Prausnitz (ref. 8) is chosen, which successfully has been used by various authors

in combined models (ref. 1, 2). In the MUNIQUAC-model for binary mixtures of components 1 and 2 the following relations between local $(\theta_{12},\theta_{21})$ and overal surface fractions (θ_1,θ_2) are used:

$$
\frac{\theta_{21}}{\theta_{11}} = \frac{\theta_2}{\theta_1} \exp\left(-\frac{\theta_2}{\theta_1}\frac{\Delta U_{21}}{RT}\right)
$$
\n(3)
\n
$$
\frac{\theta_{12}}{\theta_{22}} = \frac{\theta_1}{\theta_2} \exp\left(-\frac{\theta_1}{\theta_2}\frac{\Delta U_{12}}{RT}\right)
$$
\n(4)

where ΔU_{21} and ΔU_{12} are system-specific model parameters, R is the universal gas constant and T the temperature. These relations are different from the ones originally proposed by Abrams and Prausnitz (ref. 15) by the ratios θ_2/θ_1 and θ_1/θ_2 within the exp-terms in eqns. (3) and (4) respectively. With eqns. (3) and (4) the local and overall surface fractions are approaching each other asymptotically, if in a mixture θ_2/θ_1 or θ_1/θ_2 are going to zero. In other words the exponents in the expterms are approaching zero, if a mixture is becoming very diluted, i.e. the ideal behaviour at infinite dilution of any real misture is approached asymptotically. Following Maurer and Prausnitz (ref. 16) but using eqns. (3) and (4) the residual part of the excess Gibbs energy G_{res}^E for the MUNIQUAC-model is obtained as:

$$
\frac{d^E_{res}}{RT} = -x_1 q_1 - \ln [\theta_1 + \theta_2 \exp(-\frac{\theta_2 \Delta U_{21}}{\theta_1 RT})]
$$

$$
-x_2q_2 \frac{\theta_2}{\theta_1} \ln [\theta_2 + \theta_1 \exp (-\frac{\theta_1 \Delta U_{12}}{\theta_2 \text{ RT}})] \tag{5}
$$

where q_1 and q_2 are pure-component molecular-structure constants depending on molecular size and surface area. x_1 and x_2 are the mole fraction of component 1 and 2 respectively. Surface fractions θ_1 and θ_2 are given by:

$$
\theta_1 = \frac{q_1 x_1}{q_1 x_1 + q_2 x_2} = 1 - \theta_2
$$
\n(6)

274

Therefore the only parameters which have to be fitted are ΔU_{12} and ΔU_{21} . Assuming these parameters to be independent of temperature the thermodynamic rela tion

$$
\frac{\delta(G^E_{res}/T)}{\delta T} = -\frac{H^E_{phys}}{T^2}
$$
 (7)

yields the following expression for $H_{\text{phys}}^{\text{E}}$:

$$
x_{1}q_{1}\theta_{2}\Delta U_{21} \exp\left(-\frac{\theta_{2}}{\theta_{1}}\frac{\Delta U_{21}}{RT}\right)
$$

\n
$$
\theta_{1} + \theta_{2} \exp\left(-\frac{\theta_{2}}{\theta_{1}}\frac{\Delta U_{21}}{RT}\right)
$$

\n
$$
\frac{\theta_{1} + \theta_{2} \exp\left(-\frac{\theta_{1}}{RT}\right)}{\theta_{1} RT}
$$

\n
$$
\frac{\theta_{1} \Delta U_{12}}{\theta_{2} RT}
$$

\n
$$
\theta_{2} + \theta_{1} \exp\left(-\frac{\theta_{1}}{\theta_{2}}\frac{\Delta U_{12}}{RT}\right)
$$

\n(8)

With this equation ΔH_{phys}^{E} can be calculated using only pure component data as soon as ΔU_{21} and ΔU_{12} are determined.

The RAS-model (ref. 8) gives the following expression for H_{chem}^E :

$$
H^{E}_{chem} = x_1 K_1 \Delta h_1^*(\varphi_{1,mon} - \varphi_{1,mon}^0)
$$
 (9)

where index 1 refers to the associating component. Assuming linear consecutive association the association constant is defined as:

$$
K_1 = \frac{c_i}{c_{i-1} * c_1} \frac{1}{V_1}
$$
 (10)

 K_1 is regarded to be independent of i with c_i being the molar concentration of imers consisting of i associated molecules and V_1 being the molar volume of component 1. According to this definition K₁ is a dimensionless quantity. Δh_1^* is the

change in energy associated with the formation of one mole H-bonds. x_1 is the overall mole fraction and $\varphi_{1,\text{mon}}^0$ and $\varphi_{1,\text{mon}}^0$ are the volume fractions of monomers (non-associated molecules) in the mixture and the pure liquid respectively. $\varphi_{1,\text{mon}}$ and $\frac{90}{1,\text{mon}}$ can be calculated with the following equation

$$
\varphi_{1,\text{mon}} = \frac{1 + 2K_1\Phi_1 - \sqrt{(1 + 4K_1\Phi_1)}}{2K_1^2\Phi_1} \tag{11}
$$

(with $\varphi_{1,\text{mon}} = \varphi_{1,\text{mon}}^0$ for $\Phi_1 = 1$)

In this equation Φ_1 is the overall volume fraction given by:

$$
\Phi_1 = \frac{x_1 V_1}{x_1 V_1 + x_2 V_2} \tag{12}
$$

with V_2 being the molar volume of component 2.

The temperature dependence of K_1 can be written as:

$$
K_1 = K_1^0 \exp(-\frac{\Delta h_1^*}{RT} \frac{1}{T} - \frac{1}{T^0})
$$
\n(13)

with K_1^0 being the numerical value at temperature T^0 .

With these equations ΔH^E_{chem} can be calculated using only pure component data as soon as K_1^0 and Δh_1^* are determined. Except for pure component constants the MUNIQUAC-RAS model obtained by using eqn. (8) and eqn. (9) with eqn. (2) gives an expression for H^E with the four system-specific parameters ΔU_{21} , ΔU_{12} , K_1^0 and Δh_1^* .

Determination of model parameters

The system-spezific parameters of the model used can be obtained by fitting the theoretical expression for H^E to experimental data. In order to determine K_1^O and Δh_1^* only the H^E-data at 348 K were used. At this temperature all four parameters K_1^0 , Δh_1^* , ΔU_{12} and ΔU_{21} were fitted simultaneously to the data with pure component constants q_1 and q_2 taken from literature (ref. 17). It was found that for all mixtures the same values of K_1^0 and Δh_1^* can be used:

$$
K_1^0 (T^0 = 348.15 \text{ K}) = 29.1
$$

$$
\Delta h_1^* = -29.3 \text{ kJ*mol}^{-1}
$$

These values also have been used for the other temperatures, i.e. at 323 K and 373 K only the two parameters ΔU_{12} and ΔU_{21} remain to be determined by a best fit to the esperimental data. The parameters obtained at various temperatures clearly showed their dependence on temperature. This dependence can be described by the following relations:

$$
\Delta U_{12} = a_1 + b_1(1/T) \tag{14}
$$

$$
\Delta U_{21} = a_2 + b_2(1/T) \tag{15}
$$

The constants a_1 , b_1 , a_2 and b_2 are different for each mixture and are all given in Table 5.

TABLE 5. Temperature independent constants to describe the temperature dependence of the MUNIQUAC-RAS interaction parameters given by eqns. (14) and (15)

System	a_1	\mathbf{p}_1	a_2	b_{2}
2-methoxyethanol+n-hexane	-2579.9	599.2	2219.6	35.8
2-methoxyethanol+n-heptane	-2684.1	609.8	3198.5	-239.0
2-methoxyethanol+n-octane	-2835.0	650.0	3490.0	-300.0
2-methoxyethanol+n-decane	-3050.0	700.0	4560.0	-600.0
2-methoxyethanol+	-3281.6	770.7	5039.8	-821.9
2,2,4-trimethylpentane				

As an example in Fig. 5 it is shown for mixtures with n-hesane how well the MUNIQUAC-RAS model describes the mole fraction dependence of H^E at various temperatures. The deviation between calculated and experimental $H^{E_{\rightarrow}}$ values is in the entire mole fraction range within the esperimental inaccuracy. For all other mixtures the agreement is just as good.

$$
\Delta U_{12} = c_1 + d_1 n \tag{16}
$$

$$
\Delta U_{21} = c_2 + d_1 n \tag{17}
$$

The constants c_1 , d_1 , c_2 and d_2 consequently are depending on temperature and are given in Table 6.

Fig. 6. Dependence of $\Delta U_{12} \equiv \Delta U_{AB}$ and $\Delta U_{21} \equiv \Delta U_{BA}$ on temperature for 2-methoxy ethanol+n-alkane mixtures.

TABLE 6. Parameters for the correlation of the MUNIQUAC-RAS-parameters with the number of C-atoms of the n-alkanes according to eqns. (16) and (17).

Temperature (K)	c_{1}	d,	c_{2}	d.,
322	-515.2	-37.2	1807.8	90.8
345	-602.5	-42.5	1631.7	120.7
370	-689.8	-47.8	1455.5	150.5

Fig. 7 shows how well the linear relation between $\Delta U_{12} = \Delta U_{AB}$ and $\Delta U_{21} = \Delta U_B$ and n as given by eqns. (16) and (17) is realized.

Fig. 7. Correlation of the MUNIQUAC-RAS-parameters and the number of the C-atom of the n-alkanes according to eqns. (16) and (17).

As K_1^0 and Δh_1^* have always the same values the correlations with temperature and chain length of the n-alkane developed allow the determination of ΔU_{12} and ΔU_{21} by interpolation and to some estend by extrapolation to other 2-methoxyethanoln-alkane mixtures and other temperatures than covered in this work. In other word the model can be used within some border lines to precalculate H^E . The degree o branching could not be included as a correlation parameter because only one misturt containing a branched alkane has been investigated so far.

The calculations with the NUNIQUAC-RAS model clearly show that the physica contribution given by eqn. (8) is much smaller than the chemical one given by eqn (9). As an example in Fig. 8 H_{phys}^E and H_{chem}^E are compared with H^E for 2-methosyethanol+n-hexane at 373 K and 25 bar. Only for large mole fractions of 2-methosyethanol the physical contribution is about as large as the chemical one. H-bonding accounts for the main contribution to H^E as to be expected for the type of mixtures investigated and as already discussed elsewhere (ref. 10).

Fig. 8. Comparison of H^E_{phys} and H^E_{chem} with $H^E = H^E_{\text{phys}} + H^E_{\text{chem}}$ for x 2-methoxyethanol+(l-x1 n-hesane at 373.15 K and 25 bar.

The temperature dependence of H^E also is dominated by the corresponding dependence of $\text{H}^{\text{E}}_{\text{chem}}$. In Fig. 9 the effect of temperature on $\text{H}^{\text{E}}_{\text{phuc}}$ and $\text{H}^{\text{E}}_{\text{chem}}$ is shown again for the mixture with n-hexane. Whereas the anyhow small $\texttt{H}^{\texttt{D}}_{\texttt{phys}}$ decreases with increasing temperature the dominating $\text{H}_{\text{chem}}^{\text{E}}$ increases and deter mines the overall dependence on temperature. Similar behaviour is to be found for all the other mistures investigated and confirms the dominating influence of H-bonding of H^E for mixtures containing at least one associating component.

Fig. 9, Effect of temperature on n-hesane as calculated with eqns. correlation developed. for x 2-methoxyethanol+(l parameters obtained from the

CONCLUSION

The experimental results of H^E for 2-methoxyethanol+alkane mixtures show at a given temperature significant dependence on the size and shape of the alkane molecule whereas the dependence on temperature is dominated by H-bonding of 2-methoxyethanol. The concept of combining the MUNIQUAC-model for the physical contribution to H^E with the RAS-model for the chemical one leads to an expression for H^{E} containing four system-specific parameters. The dependence of H^{E} on temperature and composition can be represented very well with this model-equation. The system-specific parameters could be correlated with respect to their dependence on temperature and chain length of the n-alkane mixed with 2-methoxyethanol. Within the state conditions the correlation covers it is possible to precalculate H^E at any desired temperature and for related mixtures.

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