# **USE OF SPREADSHEETS IN THERMAL ANALYSIS. PART 6**

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#### ABSTRACT

In a recent report [1], a mathematical expression was developed for the concurrent evaluation of two rate constants in two consecutive first-order reactions. When this expression was implemented using a computer program, the values of the rate constants obtained agreed favorably with theoretically assumed and reported experimental values.

In the present paper, the preceding expression will be implemented utilizing spreadsheet analysis. To this end, the computer program used to implement the above expression has been modified and adapted for spreadsheet use. The resulting macro has then been utilized to analyze both theoretical and experimental data. The calculated values of rate constants obtained have been compared with theoretically assumed and reported experimental values.

#### INTRODUCTION

Recently, an expression was developed for the concurrent estimation of two rate constants for two consecutive first-order reactions [1]. Subsequently, a computer algorithm was developed to implement this expression; BASICA (IBM) was employed for the testing of the experimental data involved. Values of the rate constants obtained agreed favorably with theoretically assumed and reported experimental values.

In the present paper, the preceding reaction type will be used and the preceding algorithm will now be modified and adapted for the spreadsheet analysis of theoretical and experimental data in order to evaluate concurrently the two rate constants. Their calculated values will be compared with theoretically assumed and reported experimental values. It may also be mentioned here that the spreadsheet utilized was Lotus 1-2-3, Release 2.2.

## SOME THEORETICAL ASPECTS

A symbolic representation of two consecutive irreversible first-order reactions follows:

$A \xrightarrow{k_1} B + gas$	(1a)
$B \xrightarrow{k_2} C + gas$	(1b)

In the preceding expressions, A, B and C denote starting material, intermediate product and final product, respectively, while  $k_1$  and  $k_2$  denote the rate constants for the two steps, as shown. The utilization of TG should allow the estimation of the extent of the reactions depicted in eqns. (1a) and (1b), based on the amount of gas liberated.

In order to estimate  $k_1$  and  $k_2$  concurrently, the following mathematical expression was derived:

$$\ln\{\left[\rho - k_2(1-\alpha)\right]_0 / \left[\rho - k_2(1-\alpha)\right]\} = k_1(t-t_0)$$
(2)

where  $\rho = d\alpha/dt$ ,  $\alpha$  is the degree of conversion and the subscript 0 refers to an initial set of data values. It can readily be seen from eqn. (2) that if we make the left-hand side of eqn. (2) equal to Y then

$$Y = A_2 X + A_1 \tag{3}$$

where

 $A_2 = k_1, X = t - t_0 \text{ and } A_1 = 0$ 

By using eqn. (3), we can now employ the concept of a spreadsheet macro based on a computer algorithm previously devised and modified [1-3]. Values of  $k_1$  and  $k_2$  will be determined by means of an iteration procedure wherein a minimum value of  $A_1$  will be obtained for the conditions employed.

## APPLICATIONS OF THE METHOD

The procedure was initially tested using two sets of theoretical data. In the first case, values of  $k_1 = 0.0444$  and  $k_2 = 0.00123$  were assumed in deriving data. In Table 1, values of  $\alpha$ , reaction rate (arbitrary units) and reaction time (arbitrary units) are displayed in the range A5-C11. The initial set of data values used (subscript 0) is shown in columns A1-C1. At the bottom of Table 1 there is a listing of the various range names employed. Furthermore, in Table 2 the cell contents of the worksheet in Table 1 are listed, so that although the macro in Table 1 is not visible in its entirety the complete macro may be gleaned from a perusal of Table 2. It may be noted here that the run time for this and subsequent worksheets mentioned varies between about 15 s and 20 s (with windowsoff and utilizing a 386-20 computer). Initial values of tmp and  $k_2$  were  $1 \times 10^{-5}$  and 0, respectively, for all the runs made. The final results obtained can be viewed in row A29 in Table 1. These calculated values are virtually identical with the assumed values for  $k_1$  and  $k_2$ .

It should also be mentioned here that the algorithm employed, eqns. (2) and (3), did not act as a well-behaved function. Thus, as the values of  $k_2$  were incremented and began to exceed the most likely final value of  $k_2$ , the

# TABLE 1

Worksheet to determine  $k_1$  and  $k_2$  from theoretical data [1]

	A	8	C	D	E	F	6	н	1
1	0.5065	1.544E-03	70			0.0009369			
2	222222	********	=====	(22222233)	****		*********		********
3	Alpha	Rate	Time	k2	X		¥	XXX	Y¥Y
						*********	*********	*******	**********
		8.137E-04		0.0012301					1.775014
_		6.062E-04			60	6.52E-05			7.103606
		5.372E-04			90	1.71E-05			16.02583
_		5.054E-04			120				28.51152
		4.038E-04			150				
		4,320E-04				3.19E-08			
		4.164E-04				4.38E-09		72900	150.6344
12			*****	*********					
	Totals				960				355.4318
• •									
15	X¥Y	Tep	ki	Macro				,	Intepti
16									
	39.968	15~10	0.04	{let into			<==\a		0.001872
	159.91				-	t xk2,+xk2		kib	k2b
	360.29			-		{branch \(	-		
	640.75		1000	-	-	k2~{let xk2			0.001230
	1011.9					ntcpt)=1}{			
	2469.3					cpt){€abs(+		}{let 1	ntcpt1,int
	3313.7					}{branch lo			
- ·		3			-	t tep,+tep,			
	7996.0			•		}{branch de	onel}		
26 27				{branch \	-	71MIN	10 00001	A	
- 28			uune.	1190103718	ar .(1	beep 3}RUN	TO UNEN:	iwali (	ENGN+ET1BE
	ting .	alver ki i		0.0444		0.00123			
27	LTUBE /	alues ki i	e x4;	0.0499		0.00123			

#### Range Name Table

DONE1	D27	SYY	113
FINAL	A29	THP	917
INTEPT	H17	X	E5.,E11
INTOPTI	I17	161	C17
K1	C17	XK2	05
K1B	H20	XX	H5H11
K2B	120	XY	A17A23
LOOP	D20	Ŷ	65611
LOOP2	024	YY	15111
SX	E13	\۵	D17
SXX	H13	۱D	D18
SXY	A25		
SY	513		

cells for the intercept and  $k_1$  displayed an "ERR" message. The macro statements D20 and D21 were therefore used. Upon encountering the error message, there occurs a branching to "loop" whereby the value of  $k_2$  is decreased until the "ERR" message disappears (at this point the now positive value of  $k_2$  should be very close to the most probable value). Furthermore, there may now occur an exchange of values between intcpt Cell contents of worksheet in Table 1

A1: [N7] 0.5065 B1: (S3) [N10] 0.001544 C1: [N5] 70 F1: [W10] +B1-\$XK2\$(1-A1) A2: [₩7] \= B2: (F7) [W10] \= CZ: [W5] \= D2: [₩10] \= E2: [#4] \= F2: [W10] \= 62: [N9] \= H2; [₩7] \≠ 1Z: \= A3: [W7] ^Alpha B3: [#10] ^Rate C3: [#5] "Time D3: [W10] ^kZ E3: [₩4] ^X 63: [₩9] ^Y H3: [N7] ^XEX 13: Y#Y A4: [W7] \= B4: [W10] \= C4: [W5] \= D4: [W10] \= E4: [N4] \= F4: [W10] \= 64: [N9] \= H4; [W7] \= 14: \= A5: 1871 0.5395 B5: (S3) [W10] 0.0008137 C5: [W5] 100 D5: [W10] 0.00123012 E5: [N4] +C5-\$C\$1 F5: (S2) [W10] +B5-\$XK2\$(1-A5) 65: (F5) [W9] @LN(\$F\$1/F5) H5: [W7] +E5#E5 15: +65165 A6: [W7] 0.5602 B6: (S3) [W10] 0.0006062 C6: [W5] 130 E6: [W4] +C6-\$C\$1 F6: (S2) [W10] +B6-\$XK2\$(1-A6) 66: (F5) [W7] @LN(\$F\$1/F6) H6: [W71 +E6\$E6 16: +66466 A7: [W7] 0.5772 B7: (S3) [#10] 0.0005372 C7: FN51 160 E7: [N4] +C7-\$C\$1 F7: (S2) [W10] +B7-\$XK2\$(1-A7) 67: (F5) [W9] @LN(\$F\$1/F7) H7: [W7] +E7#E7 17: +67#67 AB: [W7] 0.5928

B8: (\$3) [W10] 0.0005054 C8: [W5] 190 E8: [#4] +C8-\$C\$1 F8: (52) [W10] +88-\$XK2\$(1-A8) 68: (F5) [N9] @LN(\$F\$1/F8) H8: [W7] +E8#E8 18: +68#68 A9: [N7] 0.6076 87: (53) [W10] 0.0004838 C9: [W5] 220 E7: [W4] +C9-\$C\$1 F9: (S2) [#10] +B9-\$XK2\$(1-A9) 69: (F5) [W9] @LN(\$F\$1/F9) H9: [W7] +E9#E9 17: +67\$67 A10; [W7] 0.6488 B10: (53) [W10] 0.00043205 C10: [W5] 310 E10; [#4] +C10-\$C\$1 F10: (S2) [W10] +B10-\$XK2\$(1-A10) 610: (F5) [W9] @LN(\$F\$1/F10) H10: [W7] +E10#E10 I10: +610#610 A11: [W7] 0.6615 B11: (S3) [W10] 0.0004164 C11: FW51 340 E11: [W4] +C11-\$C\$L F11: (S2) [W10] +B11-\$XK2\*(1-A11) 611: (F5) [W9] @LN(\$F\$1/F11) B11: [W7] +E11#E11 I11: +6111611 A12: [W7] \= 812; [₩10] \= C12: [₩5] \= D12: [W10] \= E12: [₩4] \= F12: [W10] \= 612: [W9] \= H12: [#7] \= I12: \= A13: [W7] 'Totals----> E13: [W4] @SUM(X) 613: [N7] @SUM(Y) H13: [W7] @SUM(XX) 113: @SUM(YY) A14: [₩7] \= B14: [W10] \= C14: [N5] \= D14: [N10] \= E14: [W4] \= F14: [W10] \= G14: [W7] \= H14: [W7] \= 114: \= A15: [W7] \*X#Y 815: [W10] \*Tep

Cell contents of worksheet in Table 1

C15: [W5] ^k1 015: [W10] ^Nacro H15: [#7] 'Intopt 115: 'Intepti A16: [¥7] \= B16: [W10] \= C16: [W5] \= D16: [W10] \= E16: [#4] \= F16: [W10] \= 616: [W9] \= H16: [¥7] \= 116: \= A17: [W7] +E5#65 B17: (S0) [W10] 1.0000000E-10 C17: [W5] (@ROWS(X)#SXY-SX#SY)/(@ROWS(X)#SXX-(SX)^2) D17: [W10] '{let intcpt1,100} 617; [#9] ^(==\a H17: [W7] (SY/@ROWS(X))-\$K1\$(SX/@ROWS(X)) 117: 0.0018725353 A18: [W7] +E6\$66 D18: [W10] '{goto}xk2"{let xk2,+xk2+tmp}" 618: [W9] ^<==\d H18: [W7] ^k16 I18: ^k2b A19: [W7] +E7#67 D19: [W10] '{if +intcpt>0}{branch \d} H19: [W7] \= 119: \= A20: [W7] +E8#68 C20: [W5] 'loop D20: [W10] '{home}{goto}xk2^{let xk2,+xk2-tmp}" H20: [W7] 0.044412747 120: 0.00123012 A21: [#7] +E9169 D21: [W10] '{if @iserr(+intcpt)=1}{branch loop} A22: [N7] +E10#610 D22: [W10] '{if @abs(+intcpt)(@abs(+intcpt1)){let intcpt1,intcpt){let k2b,+xk2}{let k1b,+xk1} A23: [W7] +E11#611 D23: [W10] '{if +intcpt<0}{branch loop} A24: [N7] \= D24: [W10] '{goto}tmp"{let tmp;+tmp/10} A25: [W7] @SUM(XY) D25: [W10] '{if +tmp(IE-9){branch done1} D26: [W10] '{branch \d} C27: [#5] 'done1 D27: [W10] '{goto}final"(beep 3)RUN IS OVER! {wait @now+@time(0,0,5)){escape} A29: [W7] 'Final values k1 & k2; D29: (F4) [W10] +K1B F29: (F5) [W10] +K2B

and intept1,  $k_{2b}$  and  $xk_2$  and  $k_{1b}$  and  $xk_1$  (cf. Table 2, D22). Tmp is then decreased in value by a factor of 10 and the iteration is either restarted or final values are displayed, depending on the value of tmp (the run is concluded when the value of tmp is less than  $1 \times 10^{-9}$ ).

eviated	wo	rksheet	to d	letermin	$e k_1$ ar	nd $k_2$	from th	neoretical data [1]
3.60 <b>0E</b> -03	60			0.0018596				
			X	**********	¥2224¥223	XXX	Y I Y	
2.70E-03 1.55E-03 1.24E-03 1.00E-03 7.20E-04 5.80E-04 4.75E-04	90 150 180 240 300 390 450	0.0026529	30 90 120 180 240 330 390	1.22E-03 4.04E-04 2.11E-04 1.48E-04 3.71E-08 2.02E-05 1.25E-07	0.42183 1.52691 2.17790 2.52819 6.21757 4.52092 9.60622	8100 14400 32400 57600 108900 152100	2.331447 4.743253 6.391729 38.65815 20.43875 92.27954	
			<b>222</b>			0.00265		
	5.600E-03 Rate 2.70E-03 1.55E-03 1.24E-03 1.00E-03 7.20E-04 5.60E-04 4.75E-04 4.0BE-04	5.600E-03         60           Rate         Time           2.70E-03         90           1.55E-03         150           1.24E-03         180           1.00E-03         240           7.20E-04         300           5.80E-04         370           4.75E-04         450           4.08E-04         510	S.600E-03         60           Rate         Time         k2           2.70E-03         90         0.0026529           1.55E-03         150           1.24E-03         180           1.00E-03         240           7.20E-04         300           5.80E-04         370           4.75E-04         450	Rate         Time         k2         X           2.70E-03         90         0.0026529         30           1.55E-03         150         90         1.24E-03         180         120           1.00E-03         240         180         120         50         7.20E-04         300         240           5.80E-04         370         330         4.75E-04         450         390           4.08E-04         510         450         450         390         450	S.600E-03         60         0.0018596           Rate         Time         k2         X           2.70E-03         90         0.0026529         30         1.22E-03           1.55E-03         150         90         4.04E-04           1.00E-03         240         180         1.48E-04           1.00E-03         240         180         2.02E-05           5.80E-04         370         330         2.02E-05           4.75E-04         450         370         1.25E-07	S.600E-03         60         0.0018596           Rate         Time         k2         X         Y           2.70E-03         90         0.0026529         30         1.22E-03         0.42183           1.55E-03         150         90         4.04E-04         1.52691           1.24E-03         180         120         2.11E-04         2.1770           1.00E-03         240         180         1.48E-04         2.52819           7.20E-04         300         240         3.71E-06         6.21757           5.80E-04         370         330         2.02E-05         4.52092           4.75E-04         450         390         1.25E-07         9.60622           4.08E-04         510         450         2.10E-06         6.78555	S.600E-03         60         0.0018596           Rate         Time         k2         X         Y         X4X           2.70E-03         90         0.0026529         30         1.22E-03         0.42183         900           1.55E-03         150         90         4.04E-04         1.52691         8100           1.22E-03         180         120         2.11E-04         2.17790         14400           1.00E-03         240         180         1.48E-04         2.52819         32400           7.20E-04         300         240         3.71E-06         6.21757         57600           5.80E-04         350         2.02E-05         4.52092         108900           4.75E-04         450         370         1.25E-07         9.60622         152100           4.08E-04         510         450         2.10E-06         6.78555         202500	Rate         Time         k2         X         Y         X&X         Y ¥Y           2.70E-03         90         0.0026527         30         1.22E-03         0.42183         900         0.17793B           1.55E-03         150         90         4.04E-04         1.52691         B100         2.331447           1.24E-03         180         120         2.11E-04         2.17790         14400         4.743253           1.00E-03         240         180         1.48E-04         2.52819         32400         6.391729           7.20E-04         300         240         3.71E-06         6.21757         57600         38.65815           5.80E-04         370         330         2.02E-05         4.52092         108900         20.43875           4.75E-04         450         390         1.25E-07         9.60622         152100         92.27954           4.08E-04         510         450         2.10E-06         6.78555         202500         46.04371

In the second case, where theoretical values were again used to test the spreadsheet macro, values of  $k_1 = 0.0167$  and  $k_2 = 0.00265$  were assumed. Contrary to the first case a plot of  $\alpha$  vs. t was now constructed using the

#### TABLE 4

Abbreviated worksheet to determine  $k_1$  and  $k_2$  from experimental data [4]

0.432	3.390E-03	90							
Alpha	Rate	Time	k2	X		Y	XXX	Y & Y	
0.621 0.672 0.738	1.32E-03 9.00E-04 6.88E-04	180 240 300		90 150 210	1.31E-04 3.39E-05	1.66311 2.71130 4.06376	8100 22500 44100	16.51577	
19.003 149.67 406.69 Final values k1 & k2=====> 1.134 0.150 853.43 ======= 1423.8									

TABLE 3

theoretically derived values, in order to determine values of the slope ( $\rho$ ) at various times (rather than use theoretical values). The values obtained are displayed in the worksheet in Table 3 (abbreviated to avoid repetition of the macro already described) under and above the heading "Rate". The nine data triads used afforded values of  $k_1 = 0.0185$  and  $k_2 = 0.00265$  (a computer program used with this data [1] gave values for  $k_1$  and  $k_2$  of 0.0174 and 0.00265, respectively). It may also be noted here that many values of  $\alpha$  and t are necessary in order to obtain the required accurate slopes. The experimental data to be utilized next had relatively few such values.

The spreadsheet macro was finally tested using experimental data previously reported [4]. The data obtained in this report were for the hydrolysis of 2,7-dicyanonaphthalene. From a smooth plot of these experimental data, values were obtained as depicted in the worksheet in Table 4 (abbreviated to avoid repetition of the macro already described). Units are in terms of minutes. Final values, in terms of hours, were  $k_1 = 1.13$  and  $k_2 = 0.150$ . When the same data were analyzed using a computer program [1], these k-values were 1.12 and 0.150, respectively.

#### REFERENCES

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