

A new method to estimate kinetic parameters from a single non-isothermal DSC curve

Yang Zhengquan, Hu Rongzu¹ and Xie Yi

Xian Modern Chemistry Research Institute, Xian 710061 (China)

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According to our previous paper [1], the reaction rate equation used to determine non-isothermal kinetic parameters by a single non-isothermal DSC curve (see Fig. 1) is

$$\frac{d\alpha}{dt} = Af(\alpha) \left[1 + \frac{E}{RT} \left(1 - \frac{T_0}{T} \right) \right] \exp\left(-\frac{E}{RT} \right) \quad (1)$$

where α , T , $f(\alpha)$, T_0 , t , R , A and E have the usual meanings [1,2].

Differentiation of eqn. (1) with respect to T gives

$$\begin{aligned} \frac{d\left(\frac{d\alpha}{dt}\right)}{dT} = Af(\alpha) e^{-\frac{E}{RT}} \left\{ \frac{E}{RT^2} \left[\frac{2T_0}{T} + \frac{E}{RT} \left(1 - \frac{T_0}{T} \right) \right] \right. \\ \left. + \frac{A}{\phi} \left[1 + \frac{E}{RT} \left(1 - \frac{T_0}{T} \right) \right]^2 f'(\alpha) e^{-\frac{E}{RT}} \right\} \quad (2) \end{aligned}$$

where ϕ is the constant heating rate.

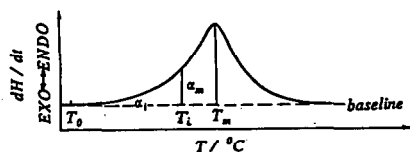


Fig. 1. Schematic diagram of typical DSC curve.

¹ Author to whom correspondence should be addressed.

TABLE 1
Several kinetic functions used for the present analysis

Function		Function form	
No.	Integral form	Differential form	
	$G(\alpha)$	$f(\alpha)$	$f''(\alpha)$
1	α^2	$\frac{1}{2}\alpha^{-1}$	α^{-3}
2	$\alpha + (1 - \alpha)\ln(1 - \alpha)$	$-\ln(1 - \alpha)$	$-[2 + \ln(1 - \alpha)](1 - \alpha)^{-2}$
3	$(1 - \frac{2}{3}\alpha) - (1 - \alpha)^{2/3}$	$\frac{2}{3}[(1 - \alpha)^{-1/3} - 1]^{-1}$	$-\frac{1}{3}(1 - \alpha)^{-7/3}[(1 - \alpha)^{-1/3} - 1]^{-2}$ $\{2 - (1 - \alpha)^{-1/3}[(1 - \alpha)^{-1/3} - 1]^{-1}\}$
4, 5	$[1 - (1 - \alpha)^{1/3}]^n$	$\frac{3}{n}(1 - \alpha)^{2/3}[1 - (1 - \alpha)^{1/3}]^{-(n-1)}$	$-\frac{2}{3n}(1 - \alpha)^{-4/3}$ $[1 - (1 - \alpha)^{1/3}]^{-(n-1)} + \frac{2n-1}{3n}(1 - \alpha)^{-1} [1 - (1 - \alpha)^{1/3}]^{-n}$ $+ \frac{n-1}{3}(1 - \alpha)^{-2/3} [1 - (1 - \alpha)^{1/3}]^{-(n+1)}$
6	$[1 - (1 - \alpha)^{1/2}]^{1/2}$	$4(1 - \alpha)^{1/2} [1 - (1 - \alpha)^{1/2}]^{1/2}$ $+ [1 - (1 - \alpha)^{1/2}]^{-1/2}$	$-(1 - \alpha)^{-3/2} [1 - (1 - \alpha)^{1/2}]^{1/2}$ $-\frac{1}{2}(1 - \alpha)^{-1} [1 - (1 - \alpha)^{1/2}]^{-1/2}$ $-\frac{1}{4}(1 - \alpha)^{-1/2} [1 - (1 - \alpha)^{1/2}]^{-3/2}$
7	$[(1 + \alpha)^{1/3} - 1]^2$	$\frac{2}{3}(1 + \alpha)^{2/3} [(1 + \alpha)^{1/3} - 1]^{-1}$ $-\frac{1}{2} [(1 + \alpha)^{1/3} - 1]^{-2}$	$-\frac{1}{3}(1 + \alpha)^{-4/3} [(1 + \alpha)^{1/3} - 1]^{-1}$ $-\frac{1}{3}(1 + \alpha)^{-1} [(1 + \alpha)^{1/3} - 1]^{-2}$ $+ \frac{1}{3}(1 + \alpha)^{-2/3} [(1 + \alpha)^{1/3} - 1]^{-3}$

8	$[(1-\alpha)^{-1/3}-1]^2$	$\frac{2}{3}(1-\alpha)^{4/3}[(1-\alpha)^{-1/3}-1]^{-1}$	$-2(1-\alpha)^{1/3}[(1-\alpha)^{-1/3}-1]^{-1}$ $-\frac{1}{2}[(1-\alpha)^{-1/3}-1]^{-2}$	$\frac{2}{3}(1-\alpha)^{-2/3}[(1-\alpha)^{-1/3}-1]^{-1}$ $+\frac{2}{3}(1-\alpha)^{-1}[(1-\alpha)^{-1/3}-1]^{-2}$ $+\frac{1}{3}(1-\alpha)^{-4/3}[(1-\alpha)^{-1/3}-1]^{-3}$
9	$-\ln(1-\alpha)$	$1-\alpha$	-1	0
10-16	$[-\ln(1-\alpha)]^n$ $(n=\frac{2}{3}, \frac{1}{2}, \frac{1}{3},$ $4, \frac{1}{4}, 2, 3)$	$\frac{1}{n}(1-\alpha)[-\ln(1-\alpha)]^{-(n-1)}$	$-\frac{1}{n}[-\ln(1-\alpha)]^{-(n-1)}$ $-\frac{n-1}{n}[-\ln(1-\alpha)]^{-n}$	$\frac{n-1}{n}(1-\alpha)^{-1}[-\ln(1-\alpha)]^{-n}$ $+(n-1)(1-\alpha)^{-1}[-\ln(1-\alpha)]^{-(n+1)}$
17-22	$1-(1-\alpha)^n$ $(n=\frac{1}{2}, 3, 2,$ $4, \frac{1}{3}, \frac{1}{4})$	$\frac{1}{n}(1-\alpha)^{-(n-1)}$	$\frac{n-1}{n}(1-\alpha)^{-n}$	$(n-1)(1-\alpha)^{-(n+1)}$
23-27	α^n ($n=1, \frac{3}{2},$ $\frac{1}{2}, \frac{1}{3}, \frac{1}{4}$)	$\frac{1}{n}\alpha^{-(n-1)}$	$-\frac{n-1}{n}\alpha^{-n}$	$(n-1)\alpha^{-(n+1)}$
28	$(1-\alpha)^{-1}$	$(1-\alpha)^2$	$-2(1-\alpha)$	2
29	$(1-\alpha)^{-1}-1$	$(1-\alpha)^2$	$-2(1-\alpha)$	2
30	$(1-\alpha)^{-1/2}$	$2(1-\alpha)^{3/2}$	$-3(1-\alpha)^{1/2}$	$\frac{3}{2}(1-\alpha)^{-1/2}$

At the point of maximum transformation rate one can obtain from the well-known condition

$$\left[\frac{d\left(\frac{d\alpha}{dt}\right)}{dT} \right]_{\substack{T=T_m \\ \alpha=\alpha_m}} = 0$$

$$\frac{E}{RT_m^2} \left[\frac{2T_0}{T_m} + \frac{E}{RT_m} \left(1 - \frac{T_0}{T_m} \right) \right] + \frac{A}{\phi} \left[1 + \frac{E}{RT_m} \left(1 - \frac{T_0}{T_m} \right) \right]^2 f'(\alpha_m) e^{\frac{-E}{RT_m}} = 0 \quad (3)$$

Differentiation of eqn. (2) with respect to T gives

$$\frac{d^2\left(\frac{d\alpha}{dt}\right)}{dT^2} = Af(\alpha) e^{\frac{-E}{RT}} \left\{ \frac{E}{RT^4} \left(-6T_0 - \frac{3E}{R} + \frac{6ET_0}{RT} + \frac{E^2}{R^2T} - \frac{E^2T_0}{R^2T^2} \right) \right.$$

$$+ \frac{A}{\phi} \frac{3E}{RT^3} \left(2T_0 + \frac{E}{R} - \frac{ET_0}{RT} \right) \left[1 + \frac{E}{RT} \left(1 - \frac{T_0}{T} \right) \right] f'(\alpha) e^{\frac{-E}{RT}}$$

$$\left. + \left(\frac{A}{\phi} \right)^2 \left[1 + \frac{E}{RT} \left(1 - \frac{T_0}{T} \right) \right]^3 \left[(f'(\alpha))^2 + f(\alpha)f''(\alpha) \right] e^{\frac{-2E}{RT}} \right\} \quad (4)$$

At the point of inflection of the DSC curve in Fig. 1, one can obtain from the condition

$$\left[\frac{d^2\left(\frac{d\alpha}{dt}\right)}{dT^2} \right]_{\substack{T=T_i \\ \alpha=\alpha_i}} = 0$$

$$\frac{E}{RT_i^3} \left\{ \frac{3T_0}{T_i} + \left(\frac{E}{RT_i} - 3 \right) \left[\frac{3T_0}{T_i} + \frac{E}{RT_i} \left(1 - \frac{T_0}{T_i} \right) \right] \right\}$$

$$+ \frac{A}{\phi} \frac{3E}{RT_i^2} \left[\frac{2T_0}{T_i} + \frac{E}{RT_i} \left(1 - \frac{T_0}{T_i} \right) \right]$$

$$\times \left[1 + \frac{E}{RT_i} \left(1 - \frac{T_0}{T_i} \right) \right] f'(\alpha_i) e^{\frac{-E}{RT_i}} + \left(\frac{A}{\phi} \right)^2 \left[1 + \frac{E}{RT_i} \left(1 - \frac{T_0}{T_i} \right) \right]^3$$

$$\times \left[(f'(\alpha_i))^2 + f(\alpha_i)f''(\alpha_i) \right] e^{\frac{-2E}{RT_i}} = 0 \quad (5)$$

TABLE 2
 Calculated values of kinetic parameters for the dehydration process for compounds I-III

Compd.	Ozawa and Kissinger methods											log A	G(α)			
	ϕ	T_m	E_o	E_k	$\log A_k$	r_o	r_k	ϕ	T_0	T_i	T_m			α_i	α_m	E
I	5	126.0	182.0	184.6	22.2	0.99	0.99	5	104.8	120.5	126.0	0.31	0.66	187.8	22.1	$-\ln(1-\alpha)$
	10	130.6														
	15	133.7														
II	20	135.8														
	5	151.6	156.7	157.6	17.4	0.99	0.99	5	128.0	145.5	151.6	0.25	0.55	165.0	17.6	$1-(1-\alpha)^{1/2}$
	10	157.4														
III	15	160.3														
	20	164.9														
	5	125.8	101.2	99.7	10.8	0.96	0.95	5	82.5	118.7	125.8	0.34	0.66	102.2	10.8	$[1-(1-\alpha)^{1/2}]^{1/2}$
	10	138.4														
	15	140.3														
	20	142.2														

Notation: ϕ , heating rate ($^{\circ}\text{C min}^{-1}$); T , temperature ($^{\circ}\text{C}$); E , apparent activation energy (kJ mol^{-1}); A , pre-exponential constant (s^{-1}); r , linear correlation coefficient; subscript O, data obtained by Ozawa's method; subscript K, data obtained by Kissinger's method; T_0 , the initial point of the deviation from the baseline of the DSC curve ($^{\circ}\text{C}$); subscript i, the point of inflection of the DSC curve; subscript m, the point of maximum transformation rate of the DSC curve; α , the fraction of the material reacted; $G(\alpha)$, integral mechanism function.

By substituting all the forms of $f(\alpha)$ listed in Table 1 and the corresponding forms of $f'(\alpha)$ and $f''(\alpha)$ and the values of T_0 , T_i , T_m , ϕ , α_i and α_m into eqns. (3) and (5), the corresponding values of E and A may be determined by computer. Equations (3) and (5) are suitable for computer programming for fast computations. For example, by substituting the original data of the dehydration process of the ammonium salt monohydrate (I), potassium salt monohydrate (II) and copper salt tetrahydrate (III) of 3-nitro-1,2,4-triazol-5-one, listed in Table 2, and all the forms of $f(\alpha)$, $f'(\alpha)$ and $f''(\alpha)$ into the eqns. (3) and (5), the corresponding values of E and A and the probable mechanism functions (see Table 2) are obtained by the method of logical choices [1]. These values of E and A are in agreement with the calculated values obtained by the methods of Ozawa [3] and Kissinger [4]. This fact shows that eqns. (3) and (5) are suitable for computing the values of E and A .

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