# THE DELTATHERM DYNAMIC ADIABATIC CALORIMETER: SOME APPLICATIONS

E. L. Dosch

Technical Equipment Corporation, Denter, Colorado 80204 (U.S.A.)

W. W. WENDLANDT Thermochemistry Laboratory, Department of Chemistry, University of Houston, Houston, Texas 77004, (U.S.A.) (Received October 17th, 1969)

## ABSTRACT

The Deltatherm dynamic adiabatic calorimeter is described. The operation and calibration of the instrument are discussed and its application to the determination of the  $C_p$  of several metals and the  $\Delta H$  of several dehydration reactions. The accuracy and precision of the calorimeter are about  $\pm 1\%$ .

## INTRODUCTION AND THEORY

Although it is a convenient technique to use, quantitative differential thermal analysis (QDTA) has a number of disadvantages when compared to dynamic calorimetry<sup>1,2</sup>. The usual relationship used in QDTA is

# $m\Delta H = KA$

where *m* is the mass of the sample,  $\Delta H$  is the heat of reaction of the system, *A* is the area of the curve peak, and *K* is the calibration constant<sup>3</sup>. The determination of *K* is the main source of error since it varies with the thermal conductivity of the system and hence the temperature. Small errors in the evaluation of *K* introduce much larger errors in the  $\Delta H$  values obtained. In general, heats of fusion, heats of reaction, and other thermochemical measurements, can be determined by QDTA with a precision and accuracy of about  $\pm 5$  to  $\pm 10\%$ .

To obtain a higher order of precision and accuracy, say  $\pm 1\%$ , some type of a dynamic calorimeter must be employed for the measurements. A number of these instruments have been described, perhaps the most sophisticated is the differential scanning calorimeter (DSC) described by Watson *et al.*<sup>4</sup> and O'Neill<sup>5</sup>. Other calorimeters have been discussed by Speros and Woodhouse<sup>6</sup>, Thomasson and Cunningham<sup>7</sup>, Sherwin<sup>8</sup>, Solomons and Cummings<sup>9</sup>, and more recently by Hill and Slessor<sup>10</sup>. The Hill and Slessor calorimeter is a rather interesting one in that heating and temperature control is done by means of focused radiation from projection lamps. There are several excellent reviews on dynamic calorimetry. The general area of microcalorimetry is reviewed by Calvet and Prat<sup>11</sup> while the entire area of calorimetry, including applications and instrumentation, is discussed by Wilhoit<sup>12</sup>.

## The Deltatherm adiabatic calorimeter

The Deltatherm calorimeter has previously been described by Dosch<sup>13</sup>. The calorimeter is a constant heating-rate type in which the sample chamber is heated at a constant rate, any departure from which is detected and applied to it as a correction factor. The temperature difference between the sample chamber and its adiabatic enclosure is detected by a differential thermocouple whose output is used to automatically vary the power applied to the sample, thereby maintaining adiabatic conditions.

The specific heat of a substance,  $C_p$ , is defined as

$$C_p = \frac{q}{m(T_2 - T_1)} \tag{1}$$

where q is the amount of heat required to raise the temperature of mass m from  $T_1$  to  $T_2$ . Substituting the electrical equivalent for heat,

$$q = k_1 P t \tag{2}$$

into Eqn. (1) and rewriting in differential form,

$$C_{p} = \frac{k_{1}P}{m} \left(\frac{\mathrm{d}t}{\mathrm{d}Y}\right) \tag{3}$$

where P is the power, t is the time, and  $k_1$  a constant. Rewriting Eqn. (3) for a constant heating rate, dT/dt, the specific heat becomes

$$C_{p} = \frac{k_{3}P}{\mathbf{i}_{m}} \tag{4}$$

Hence, the specific heat of a substance is directly proportional to the electrical power input to the calorimeter since  $k_3$  and m are constant for a given system. With proper calibration,  $k_3$  can be evaluated so that the  $C_p$  of a substance can be calculated for any temperature. The advantage of the constant heating-rate mode the conventional constant input power type of system is that the power curve gives the variation of  $C_p$ directly with temperature without first computing the reciprocal of the heating rate. Also, the former type of system provides data having a kinetics significance due to the constancy of the heating rate.

## EXPERIMENTAL

## The calorimeter

A block diagram of the calorimeter is shown in Fig. 1. The temperature difference between the sample and the adiabatic enclosure is detected by the differential thermocouple TCI. The voltage output of TCI is amplified by a chopper stabilized d. c. amplifier whose output controls a solid-state power driver which supplies up to 4 watts of power to the heater, H1. The differential temperature is also recorded on one channel of the multi-channel recorder to indicate the extent with which adiabatic



AUTOMATIC ADIABATIC CALORIMETER SYSTEM Fig. 1. Block diagram of the Deltatherm calorimeter system.

conditions are being maintained in the adiabatic enclosure. In general, adiabatic conditions are maintained to within  $\pm 0.05^{\circ}$  after dynamic conditions are established in the calorimeter (above 50-75°C). The power input to the sample chamber is measured by a Hall effect multiplier watt-meter and is continuously recorded on another channel of the recorder. The main furnace heater, H2, is controlled by the electronic constant rate programmer; heating rates from 2 to 20°C per min are available. The temperature of the calorimeter is detected by thermocouple TC2 and is recorded on the chart 50°C intervals.

A cross-section of the calorimeter assembly is shown in greater detail in Fig. 2. The calorimeter is mounted upon a cast ceramic pillar which can be inserted into the standard Deltatherm furnace. The adiabatic enclosure consists of a massive copper block (A) enclosed by the copper covers (B), (C), and (D). Surface temperature uniformity in the inner chamber is about 0.1 °C at a heating rate of 10°/min and proportionately less at slower heating rates. The sample chamber (F) and its cover (F) are made of silver and are thermally isolated from the block by the ceramic pillar (K). The sample container heater (G) consists of an Inconel sheathed Nichrome wire resistance element wound in the form of a helix on the inside of the sample chamber. The temperature of the sample container and block are detected by Iconel sheathed Chromel-Alumel thermocouples (J) and (L), respectively. These two thermocouples are connected together in a differential mode for temperature detection. The sample (H) consists of either a machined ingot of a solid substance, a packed powder, or a container for powdered or liquid samples.

## Sample preparation

The sample may consist of a solid, powdered or liquid material. For machinable



Fig. 2. Cross-section of calorimeter. (A) Copper block; (B), (C), and (D), copper covers; (E) sample chamber cover; (F) sample chamber; (G) heater; (H) sample; (J) thermocouple; (K) ceramic support; (L) thermocouple.

solids, a cylinder having the maximum dimensions of 0.35 in (in diameter) by 0.55 in (in length), may be employed. Non-corrosive and non-fusible (in the temperature range to be investigated) powdered substances may be placed directly into the sample chamber. For corrosive or fusible solids and/or liquids, a stainless steel sample capsule may be used. The inside dimensions of the stainless steel capsules are 0.285 in (in diameter) by 0.520 in (in length) and have a volume of 0.6 ml. The sample is weighed out into the capsule and enclosed by means of a press-fit cover.

#### Calibration of calorimeter

The  $C_p$  calibration procedure consists of the determination of the ordinate of the chart paper in terms of calories per inch. The calibration constant,  $k_3$  [Eqn. (4)] is thus

$$k_3 = \frac{\Delta P}{mC_p} \tag{5}$$

The procedure consists of first obtaining a "power curve", at the operating conditions to be employed for the  $C_p$  determinations, of the calorimeter and empty sample capsule. The standard  $C_p$  reference substance is usually a machined ingot of metai.

#### DELTATHERM DYNAMIC ADIABATIC CALORIMETER

From the difference between the power curves for the standard substance and the empty calorimeter, the  $\Delta P$  may be obtained and hence,  $k_3$ . Using  $\alpha$ -nickel, the calibration constants, at different power settings, are given in Table I. The agreement between the individual  $k_3$  values was  $\pm 2\%$  of each other.

Temperature (°C)	∆P (in)	Cp (Ni) (cal/g/°C)	Heat absorbed (cal)	k₃ (cal/in)	
				and the second sec	
Power = 25%					
100	2.24	0.114	0.815	0.364	
200	2.46	0.125	0.894	0.363	
300	2.76	0.138	0.987	0.360	
400	2.51	0.123ª	0.880	0.350	
500	2.47	0.126*	0.901	0.365	
			$k_3$ (average) = 0.360 cal/i		
Power = 50%					
100	4.76	0.114	0.815	0.171	
200	4.97	0.125	0.894	0.180	
300	5.26	0.138	0.987	0.188	
400	4.69	0.123	0.880	0.188	
500	4.61	0.126 <sup>®</sup>	0.901	0.195	
			$k_3$ (average) = 0.184 cal		

#### TABLE I

CALIBRATION OF CALORIMETER WITH  $\alpha$ -NICKEL<sup>6</sup>

m = 7.151 g; Ni(a),  $Cp = 4.06 + 7.04 \times 10^{-3} Y$  and Ni( $\beta$ ),  $Cp = 6.00 + 1.80 \times 10^{-3} T^{14}$ ;  $\Delta T = 2.5X$ ; heating rate, 5°/min. <sup>b</sup> $\beta$ -Nickel.

The calorimeter was also calibrated for  $\Delta H$  measurements by use of a substance having a known heat of fusion,  $\Delta H_f$ . The standard substance used was pure tin with a  $\Delta H_f$  of 1720 cal/g atom or 14.5 cal/g<sup>14</sup>. The procedure consisted of first obtaining the power curve for the calorimeter plus empty capsule, at the operating conditions to be employed for the various investigations. A known amount of tin is then sealed into the capsule and a power curve obtained as above. The fusion peak in the second curve is integrated by means of a planimeter and its area determined. The calibration constant,  $K_{\rm H}$ , is calculated from

$$K_{\rm H} = \frac{m\Delta H_{\rm f}}{A} = {\rm cal/in^2} \tag{6}$$

where *m* is the mass of the sample, in g;  $\Delta H_f$  is the heat of fusion of the sample, in cal/g; and *A* is the peak area in in<sup>2</sup>. The results of this calibration procedure are given in Table II while the power curve is given in Fig. 3.

# Heats of fusion and reaction studies

The procedure was identical to that used for the calibration studies. Compounds studied included lead,  $CuSO_4 \cdot 5H_2O$ , and  $BaCl_2 \cdot 2H_2O$ . Samples of pure copper and aluminum were used for the  $C_p$  determinations.

Thermochim. Acta, 1 (1970) 181-189



Fig. 3. Calorimeter power curve for tin; heating rate, 5°/min.

#### TABLE II

 $K_{\rm H}$  calibration data using tin as the standard

Heating rate (°/min)	Area (in²)	Heat absorbed (cal)	K <sub>H</sub> (cal/in <sup>1</sup> )
10	3 949	23.46	9 241
10	2.800	23.47	8.382
10	2.912	23.47	8.060
10	2.688	23.47	8.731
5	2.752	23.47	8.760
5	2.752	23.47	9.051
5	2.864	23.47	8.700
2.5	2.688	23.47	8.917

**RESULTS AND DISCUSSION** 

## C<sub>p</sub> Determinations

A typical calorimeter  $C_p$  power curve is shown in Fig. 4. Three curves are shown in the figure: (a) the power curve for the empty calorimeter plus sample container; (b) the power curve for the calorimeter containing the sample; and (c) the  $\Delta T$  curve. The  $\Delta P$  in Eqn. (5) is obtained by measuring the distance between the two power curves.



Fig. 4. A typical calorimeter  $C_p$  power curve.

#### DELTATHERM DYNAMIC ADIABATIC CALORIMETER

The specific heats of copper and aluminum, at various temperatures, are given in Table III. The  $C_p$  values for copper are in good agreement with the calculated values<sup>14</sup>, especially at the higher temperatures. The values found for aluminum were 4 to 16% lower than the calculated values with the errors becoming smaller at the higher temperatures. The reason for this large difference is not known.

#### TABLE III

Temperature	C <sub>p</sub> , copper (cal/g/°C)		C <sub>p</sub> , aluminum (cal/g/°C)		
(°C)	found	calc."	found	calc.»	
100	0.104°	0.094	0.188	0.224	
200	0.107	0.095	0.253	0.235	
300	0.106	0.099	0.261	0.246	
400	0.102	0.101	0.265	0.257	
500	0.102	0.103	0.278	0.268	

C.	DETERMINATIONS	HEATING	RATE	OF	5°	/win)	5
~		(BEATING)	NAIE	OF.	~ .	/	,

"Calc. from  $C_p = 5.41 + 1.50 \times 10^{-3}$  Y. Calc. from  $C_p = 4.94 + 2.96 \times 10^{-3}$  Y. C<sub>p</sub> data in cal/g/°C.

## **∆H** Determinations

The  $\Delta H$  for the dehydration of CuSO<sub>4</sub>·5H<sub>2</sub>O was obtained by use of Eqn. (6). The calorimeter power curve for the dehydration reaction is shown in Fig. 5.

Copper sulfate 5-hydrate dehydrates by the following reactions:

- (a)  $CuSO_4 \cdot 5H_2O(c) \rightarrow CuSO_4 \cdot 3H_2O(c) + 2H_2O(l)$
- (b)  $2H_2O(l) \rightarrow 2H_2O(g)$
- (c)  $CuSO_4 \cdot 3H_2O(c) \rightarrow CuSO_4 \cdot H_2O(c) + 2H_2O(g)$
- (d)  $CuSO_4 \cdot H_2O(c) \rightarrow CuSO_4(c) + H_2O(c)$



Fig. 5. Calorimeter power curve for the dehydration of  $CuSO_4$ ·5H<sub>2</sub>O.

The curves in Fig. 5 were due to the above reactions. The first two peaks were due to reactions(a)-(c), while the last peak was caused by reaction (d). This is a well known system and has been studied by a number of investigators<sup>15-17</sup>. Only recently,

Thermochim. Acta, 1 (1970) 181-189

Wendlandt<sup>18</sup> has detected the presence of liquid water in this system [reaction (a) above] by means of electrical conductivity measurements.

The  $\Delta H$  values obtained for the dehydration reaction are given in Table IV. These values are given in kcal/mole of water and in kcal/mole of compound. The agreement between the values found here and the literature values is quite good.

The calorimeter was also used to obtain the  $\Delta H$  of dehydration of BaCl<sub>2</sub>·2H<sub>2</sub>O. This compound dehydrates according to the reactions<sup>15</sup>:

(a)  $BaCl_2 \cdot 2H_2O(c) \rightarrow BaCl_2 \cdot H_2O(c) + H_2O(l)$ 

(b) 
$$H_2O(l) \rightarrow H_2O(g)$$

(c)  $BaCl_2 \cdot H_2O(c) \rightarrow BaCl_2(c) + H_2O(g)$ 

The first peak in the power curve was due to reactions (a) and (b) and the second, by reaction (c). The  $\Delta H$  values are given in Table IV. The  $\Delta H$  values obtained were in good agreement with the literature values.

#### TABLE IV

heats of reaction and/or fusion as determined by the Deltatherm calorimeter (heating rate of  $5^{\circ}$ /min)

Sample	Sample mass (g)	Area (in²)	Heat absorbed (cal)	∆H (cal/g)		
				Found	Lit.	
CuSO4•5H2O	0.777	18.18	161.4	12.98		
•		0.05	53.5	17.2° 69°	71¢	
CuSO <sub>4</sub> •5H <sub>2</sub> O	0.760	1 <b>7.60</b> ª	156.3	12.8°		
		5.92	52.6	17.3 <sup>5</sup> 70 <sup>c</sup>		
CuSO <sub>4</sub> •5H <sub>2</sub> O	0.710	16.29°	144.7	12.7		
		5.60	49.7	17.5 <sup>ቇ</sup> 70 <sup>c</sup>		
BaCl <sub>2</sub> ·2H <sub>2</sub> O	1.057	12.26	108.9	25.2°	26.83°	
BaCl <sub>2</sub> ·2H <sub>2</sub> O	0.835	10.43	92.6	27.1°		
Lead	1.503	0.944	8.38	5.6	5.5	
Lead	1.503	0.944	8.38	5.6		

"First two peaks. "Kcal/mole of water. "Kcal/mole of compound

For a  $\Delta H_f$  determination, the fusion of lead was investigated. The results obtained are shown in Table IV. As can be seen, the results obtained agreed very well with the reported values.

## CONCLUSIONS

As can be seen from the results reported here, the Deltatherm dynamic adiabatic calorimeter is a versatile and useful instrument. It is capable of operation in the temperature range of 50-800 °C. A high temperature version of the instrument,

#### DELTATHERM DYNAMIC ADIABATIC CALORIMETER

capable of operation to a maximum temperature of 1200 °C, is currently being developed. The calorimeter is stated to have an accuracy and precision for  $C_p$  and/or heat of reaction studies of  $\pm 1\%$ . It is anticipated that the calorimeter will be widely used for the investigation of various chemical systems, especially in the higher temperature ranges.

## ACKNOWLEDGMENT

The financial support of part of this work by the U. S. Air Force, Air Force Office of Scientific Research, through Grant No. AF-AFOSR 69-1620 is gratefully acknowledged.

#### REFERENCES

- 1 R. L. BOHON, in H. G. MCADIE (Ed.), Proceedings of the First Toronto Symposium on Thermal Analysis.
- 2 W. W. WENDLANDT, Thermal Methods of Analysis, Wiley, New York, 1964.
- 3 T. OZAWA, Bull. Chem. Soc. Japan, 39 (1966) 2071.
- 4 E. S. WATSON, M. J. O'NEILL, J. JUSTIN, AND N. BRENNER, Anal. Chem., 36 (1964) 1233.
- 5 M. J. O'NEILL, Anal. Chem., 36 (1964) 1238
- 6 D. M. SPEROS AND R. L. WOODHOUSE, J. Phys. Chem., 67 (1963) 2164.
- 7 C. V. THOMASSON AND D. A. CUNNINGHAM, J. Sci. Instr., 41 (1964) 308.
- 8 K. A. SHERWIN, J. Sci. Instr., 41 (1964) 7.
- 9 C. SOLOMONS AND J. P. CUMMINGS, Rev. Sci. Instr., (1964) 35.
- 10 R. A. W. HILL AND R. P. SLESSOR, Trans. Faraday Soc., 65 (1969) 340.
- 11 E. CALVET AND H. PRAT, Recent Progress in Microcalorimetry, Macmillan, New York, 1963.
- 12 R. C. WILHOIT, J. Chem. Educ., 44 (1967) A571, A629, A685, A853.
- 13 E. L. DOSCH, ISA Conference Paper, October 12-15, 1964, New York.
- 14 K. K. KELLEY, High Temperature Heat-Content, Heat Capacity, and Entropy Data for the Elements and Inorganic Compounds, Bureau of Mines Bulletin, 584 (1960).
- 15 H. J. BORCHARDT AND F. DANIELS, J. Amer. Chem. Soc., 79 (1957) 41.
- 16 A. REISMAN AND J. KARLAK, J. Amer. Chem. Soc., 80 (1958) 6500.
- 17 L. BEN-DOR AND R. MARGALITH, Inorg. Chim. Acta, 1 (1967) 49.
- 18 W. W. WENDLANDT, Thermochim. Acta, 1 (1970) 11.

Thermochim. Acta, 1 (1970) 181-189