APPLICATIONS OF THERMOGRAVIMETRY FOR VAPOR PRESSURE DETERMINATION

H. G. WIEDEMANN

Mettler Instrumente, A. G., Greifensee (Switzerland) **(Received August 30th, 1971)**

IKTRODUCTIOX

Nesmeyanov' has reviewed some of the current methods for the determination of vapor pressures together with the pressure ranges over which these methods can be applied (Table I). One of these is the Knudsen effusion method^{7,8}, used for the measurement of low vapor pressures in the range from 10^0 to 10^{-5} torr, and involves measurement of the rate of loss of molecules of the evaporating substance Ieaving **the**

TABLE I

MONOGRAM SHOWING THE SENSITIVITY OF THE VARIOUS METHODS FOR MEASURIXG VAPOR PRESSURE

opening of an effusion cell. A series of recent papers^{10-12,18,19} describes the adaptation of this method to a thermobalance in which the normal TG sample holder is replaced by an effusion cell. This procedure allows measurement of the loss in weight of an evaporating substance due to the exit of its molecules through a calibrated orifice. Measurements are made under isothermal conditions, with weight loss being recorded as a function of time simultaneously with sample temperature, and with

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pressure measured outside the effusion cell. Morawietz and Roeder¹³ used this method for the determination of the vapor-phase of the potassium-mercury melt, and detected formation of intermetaliic compounds of the HgK, type. Similarly, Hoenig $et al.¹⁵$ have studied the evaporation of gadolinium carbide in the temperature range $IB00-IB00°C$.

In the organic field, this same method was used successfully by Cordes et *al.' o* for the vapor pressure measurement of such aromatic complexes as chromium**dibenzene** and chromium-hexacarbonyk The present work demonstrates the extent to which a vacuum thermobalance can be used for routine vapor pressure measurements of organic compounds_

APPARATUS

Measurements were made using the MettIer Thermoanalyzer. This apparatus has been described earlier⁹ and, therefore, only special details relating to these measurements will be presented.

Fig. 1 shows schematically the most important components of the instrumentation. The thermobalance, D, is located in a tank thermostatically controlled at 25° C.

Fis I- Schematic drawing of experimental equipment. A. Knudsen cdl; **B, Cold trap; C, Ionization gauge; D, Balance acd housing; E, Diffusion pumps; F, Thermostatically controlled** reaction chamber.

The vacuum of 10^{-6} torr required for these measurements is obtained by a built-in system of which only the two diffusion pumps (E) are shown. Two different types of furnaces were used for these measurements. The furnace, F. hooked on to the balance, consisted of a double-waIled glass container through which liquids such as ethyiene giycol. water and mistures of glycerin and water could be ciruIated from a thermostat, according to the temperature range desired $(-20²C)$ to $+ 150^oC$). Cold trap, B, was filled with liquid nitrogen or other refrigerant. Molecules leaving the Knudsen cell, A, pass through the cpening into the cold trap where the majority are condensed. thus avoiding any condensation on the rod supporting the Knudsen ceI1.

Fig. 2. Double cold trap for measurements with cooling baths from -20° **to** -90° **C.**

Fig. 2 shows another "furnace" used for measurements below -20° C. The **Dewar fiask housing the Knudsen ceil was** filled with different coolants, such as; carbon tetrachloride-solid carbon dioxide $(-23^{\circ}C)$, ethyl alcohol-solid carbon dioxide $(-78\degree C)$, etc., while the cold trap was filled with liquid nitrogen. These coolant temperatures were reproducible to ± 1 ^cC. Ionization gauge, C, (see Fig. I) controlled and recorded the pressure in the furnace compartment during the measurements.

Knudsen **cell**

Fig. 3 shows a photograph and a schematic cross-section of the Knudsen cell empIoyed. The body. A, of this cell is made of aluminum. The lower part of the ceI1 is fixed to a 4-hole aIumina capillary tube connected to the balance. A coppcrconstantan thermocouple, E, brought into the cell through a vacuum-tight connection, directly measures either the temperature of the sample, F. or the temperature of the vapor phase just above the sample. A second thermocouple, D, $(Pt-Pt/10\% Rh)$ is Iocated outside the cell and serves to control temperature in the furnace compart-

Fig. 3. The effusion cell.

ment. The orifice. B, is made of a 0.01 mm thick Cr-Ni foil into which a hole is punched_ A screw cover pcmits ready exchange of **orifices with various hole diameters (I,2 and 3** mm). A second opening was used for sample introduction and both screw covers sealed on Teflon rings. Sample volumes of ≤ 1.5 cm³ can be studied at working temperatures from -100° to $+200^\circ$ C.

For some measurements a Pyrex glass cell having a sphere diameter of approximateIy I5 mm was used. In this case the substance was introduced through the orifice and the copper-constantan thermocouple inserted through a vacuum-tight inlet at the bottom in order to measure the sample temperature.

CALCULATIONS

The Knudsen vapor pressure of four different organic compounds was studied: p -chlorophenyl- $N'.N'.$ dimethyl urea (Monuron, a herbicide), p-phenacetin, anthracene and benzoic acid. Sublimation was studied in the temperature range of 250- 400 ⁻K, *i.e.* well below their respective melting points.

Equilibrium vapor pressures were calculated according to the ideal Knudsen Eqn- (1)

$$
p = \frac{\Delta m}{\Delta t} \times \frac{1}{q} \sqrt{\frac{2\pi RT}{M}}
$$
 (1)

where $p =$ vapor pressure in dyne cm⁻² (1 dyne cm⁻² = 0.750062 torr), $R = 8.314 \times$ 10^7 erg $^{\circ}$ C⁻¹ mole⁻¹, q = orifice area in cm², $\Delta m/\Delta t$ = rate of weight loss in g sec⁻¹, *T* = temperature in K , and *M* = molecular weight of the specimen in g.

For each of three sets of data (anthracene, phenacetin, monuron) three separate curves were fitted:

$$
\ln p = B + \frac{A_1}{T} \tag{2}
$$

$$
\ln p = B + \frac{A_1}{T} + A_2 \ln T \tag{3}
$$

$$
\ln p = B + \frac{A_1}{T} + A_2 \ln T + A_3 \, T \tag{4}
$$

It was found in each case that Eqn. (2) gave a satisfactory fit to the data³. The standard errors of the estimated values of A and B were also calculated. The correlation coefficient, $r (r^2)$ = the proportion of the variance of In p accounted for by the fitted regression) was as follows for Eqn (2): for anthracene $r = 0.9988$, for phenacetin $r = 0.9995$, and for monuron $r = 0.9976$. When extra terms were included, no significant improvement in r was found so that Eqn. (2) was accepted as an appropriate fit to the data given in Tabie II and shown in Fig. 4.

Vapor pressure curves for small temperature ranges can thus be approximated using Eqn. (2); however for larger temperature ranges Eqn. (4) is used. The vaiue of the product 4.574A corresponds directly to the heat of sublimation (.1H_s) for measurements below the melting point, and to the heat of vaporization (AH_x) for measurements which have been made at temperatures above the melting point. If me isurements are made over a narrow temperature range on both **sides of the melting point,** then since the temperature dependence of $.H_s$ and AH_s can be neglected over small temperature ranges, $(.1H_s - .1H_s)$ corresponds to the heat of fusion, $.1H_f$. Fig. 5 shows this method of obtaining $\mathcal{A}H_f$ using the experimental values of vapor pressure, for the case of benzoic acid.

ESPERI%fENTAL

The mean value of the orifice diameter **in the Knudsen cell was determined by use of a microscope with ocular micrometer and the corresponding area was calulated prior to making the effusion measurements_**

The Knudsen cell made from aluminum was unsuitable for use with the halogenated organic compounds studied, since these appeared to decompose during the

Fig. 4. Knudsen vapor pressure of different compounds at 250²-400^cK. Monuron, p-phenacetin, an**thracene. benzoic acid.**

test. Therefore a Pyres cell having the same features as the aIuminum ceI1 was used. Since, for mechanical stability, the glass cell could not be made with a wall thickness **of 0.01 mm. the orifice area was determined by calibration against the known vapor** pressure of benzoic acid^{21.22}. From the rate of vaporization of benzoic acid at different temperatures the orifice area could be determined using Eqn. (5)

$$
q = -\sqrt{\frac{2\pi RT}{M}} \times \frac{g}{p} = -K\sqrt{\frac{Tg}{p}}
$$
 (5)

where $q =$ orifice area in cm², $p =$ vapor pressure in torr, $q =$ rate of weight loss in g sec^{-1}, and R, T and M have the usual meanings. This Eqn. can be simplified by combining several vaIues into a constant, *K.* The mean vaIue of the orifice area of the glass cell (Fig. 6) was found to be 1.93×10^{-2} cm² (Table III).

The wall thickness of the Pyres ceI1 and the form factor are automatically taken into account by determining the orifice area this way. Ciausing has described investigations of this nature^{16, 17}on a wide variety of materials. It is necessary that the

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TABLE II

VAPOR PRESSURES OF THE MEASURED COMPOUNDS

"Orifice diameter 3 mm. For other measurements, orifice diameter 1 mm.

Fig. 5. Determination of heat of sublimation, $AH₂$, heat of vaporization, $AH₂$, and the heat of fusion, ΔH_f , from the vapor pressure curve of benzoic acid.

mean free path of the molecules is larger than the orifice diameter in order to employ the Knudsen formula. Thus, the highest measurable pressure is between 10° and 10^{-1} torr for an orifice diameter of 0.1 mm, depending upon molecular weight.

The lowest vapor pressure to be determined by this method depends on several

Mean value of $q = 1.93 \times 10^{-2}$ cm².

Fig. 6. Pyrex effusion cell. Thermochim. Acta, 3 (1972) 355-366

factors incIuding orifice diameter_ Since effusion rate is very small at Iow pressures, a !arger orifice diameter is required_ Orifice diameters of 3-5 mm are needed for vapor pressures of 10^{-4} - 10^{-6} torr, since the mean free path is about 1m under **these conditions_ Thus, the range over which measurements can be made using this** method depends on the sensitivity and reproducibility of the balance, *i.e.* for an effusion rate of 10^{-9} g sec⁻¹, corresponding to a pressure of 10^{-6} torr, and for a test lasting 10-20 h, the maximum drift of the balance should not be more than $\div 5 \mu$ g ($\sim 5\%$). Furthermore, the vacuum outside the effusion cell is important. In general, this pressure should be about an order of magnitude below the vapor pressure **to be determined in order to ensure effusion of the molecules. This external pressure** is monitored and recorded continuously. The cold trap near the orifice of the Knudsen cell serves to condense the vaporized compound and assists in stabilizing the external **cell serves to condense the vaporized compound and assists in stabiIizing the external pressure_ Maintainin, m the temperature of the sampIe and effusion ceil constant is the most important requirement for such measurements. Since the change of a few tenths 'C wiI1 alter the vaporization rate and Iead to erroneous measurements, the sample temperature thermocoupie was pIaced close to the sampIe under investigation**

Fig. 7. Original diagram of a vapor pressure measurement weight loss produced by effusion of benzoic acid vapor leaving the cell through a calibrated orifice $(7.147 \times 10^{-3} \text{ cm}^2)$ under isotherm **benzoic acid vapor tearing the cell throu_eh a calibrated orifice** (7.147 x JOs3 **cm') under isotherm conditions** (.17.15'0. **recorded as a function of time simultaneously with sample temperature and pressure outside the cell.**

and the temperature was maintained constant by use of a thermostatically controiied Iiquid bath.

A sample weight of about 500 mg was used in the Knudsen cell for each test, and materials were sublimed several times, and degassed on the balance under high vacuum, before effusion measurements.

Fig. 7 shows an original diagram of a run with benzoic acid at 17.28 \degree C, after establishing equilibrium conditions. One small division corresponds to 0.5° C, showing that the temperature was kept constant to ± 0.1 °C over the test time of 6 h. Similarly, the pressure was nearly constant at 1.5×10^{-5} torr. The two weight traces, recorded at different sensitivities, show a constant rate of weight loss. The total measured effusion of benzoic acid was 2.25 mg after 6 h, corresponding to an effusion rate of 10^{-7} g sec⁻¹.

If the effusion rate appears to be non-linear, this may be due to; (i) equilibrium conditions have not yet been reached, (ii) the substance is not pure or has started to decompose, (*iii*) the sample is completely vaporized.

RESULTS ASD DISCUSS104

Fig. 4 and Table 11 show that this measurement technique is applicable over the pressure range 10^0 -10⁻⁶ torr, with the available instrumentation. Comparison with established values is relatively difficult, since very little data for the vapor pressure of organic compounds have been published for this pressure ran_ge. Values for benzoic acid, known to about 10^{-2} torr, are in good agreement with present measurements; however the new data deviate from the available information for monuron^{4} and anthracene¹⁹.

The vapor pressure curve of benzoic acid shows a deviation from linearity in the pressure range 10^{-4} - 10^{-5} torr, possibly due to association or dimerization of the benzoic acid molecules. An attempt to verify this suggestion will be made using simultaneous mass spectrometric measurements.

CONCLUSION

Results of these measurements demonstrate this method for vapor pressure measurements in the range 10^0 - 10^{-6} torr will produce useful results in a comparatively short time. Further tests are underway in different temperature ranges.

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