# **HIGH-TEMPERATURE THERMODYNAMICS OF CHEMICAL TRANSPORT REACTIONS IN THE TbiGSTEN-BROMINE SYSTEM OF HALOGEN-INCANDESCEhi LAMPS AND ITS INFLUENCE BY HYDROGEN, OXYGEN .4ND CARBON**

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## ABSTRACT

The simultaneous reaction equihbria in the heterogeneous system tungstenbromine and its influence by hydrogen, oxygen and carbon can be evaluated on the basis of chemical thermodynamics. **By** an analysis of the temperature dependence of the mass-balance of tungsten the chemical transport reactions in these systems and the burning behaviour of halogen-incandescent lamps may be predicted\_

Using thermodynamic data as given in the JAKAF Tables or evaluated by comparison with related systems computer-calculations have been made for temperatures 500-4000 K for the various reaction equilibria in the tungsten-bromine system including the infiuence of the additional constituents. Results for the chemical transport reactions are compared to lamp experiments. From the results of the thermodynamic analysis a scheme of the mechanism of the tungsten-bromine cycle in halogen-incandescent lamps is revealed.

## **INTRODUCTION**

In the field of the halogen-incandescent lamps the developments of the last ten **years** have yielded a iot of papers dealing with the chemistry and chemical transport reactions in halogen-incandescent lamps and with the interpretation of these complicated processes. However, only in the very last years extended work, which was based on thermodynamicai fundamentaIs of the reaction equilibria, has succeeded in cIarifying the mechanism of the tungsten-halogen cycle and the influence of further reaction components such as hydrogen, oxygen and carbon on this complex process<sup>1</sup>.

The tungsten-halogen cycle is a complex transport process with many variables, such as: temperature, temperature distribution, gas composition, pressure, gas velocity distribution, system-geometry, etc. and which can be anaiyzed in terms of thermodynamics, gas phase transport, or rate processes.

The main purpose of the present paper is to describe thermodynamic considerations and calcuiations as well as some practical experiments of the high temperature reaction equilibria in the tungsten-bromine system and its influence by hydrogen, oxygen and carbon.

Before going into details a brief explanation of the basic effect of the tungstenhalogen cycIe wiil be given, so that the main action of the halogen in the transport process can be appreciated. During the life of a conventional gas-filled incandescent lamp the filament will lose tungsten by net evaporation into the vapour phase. The tungsten atons leaving the surface of the filament may either diffuse to neighbouring turns of the coil or may be transferred by gas-convection to the bulb wall where they are deposited\_ This tungsten deposition on the wall will absorb light thus decreasing the Iight output of the lamp and setting a lower limit on the envelope size for any power rating. However, the blackening of the bulb wall can be prevented by addition of a small amount of haIogen to tire filling-gas of the lamp. The basic action of the halogen is that tungsten atoms evaporating from the filament and normally depositing at the bulb wall will now *react* in the vapour phase with the halogen forming a volatile tungsten halide. If the temperature of the bulb is sufficiently high no condensation of these compounds occurs and the molecules may diffuse into regions of higher temperatures in the vicinity of the coil where they begin dissociating. Thus, tungsten is returned in the vicinity of the filament and halogen is released for further regenerative reaction cycles.

In order to improve the concepts of this mechanism of the tungsten-halogen cycle on the basis of a quantitative knowledge of the various reaction systems, the chemical equilibrium composition of the relevant systems has been calculated by Neumann and coworkers' using computer programs which have been evaluated by Gottschalk and Neumann<sup>2</sup>. In doing so it has always been assumed that the reaction system was heterogeneous with respect to solid tungsten. In the present paper we will discuss how far these results can be applied to interpret the transport processes in halogen-incandescent lamps, which work on the basis of the tungsten-bromine system

## PRINCIPLES OF CALCULATION

Thermodynamic principles follow those normally **obeyed. The** basic **assump tions are (i) that the** chemical reactions are reversible, (ii) that thermodynamic equilibrium is achieved at the gas-solid interface, and (iii) that the reactions are not controlled by reaction kinetics. Then the composition of the gas-phase can be calculated making appropriate use of the relationships of the law of mass action

$$
\prod_{i=1}^{k} P_i^{r_{ij}} = K_{p_j}(T) \qquad \qquad i = 1, 2, ... k \n j = 1, 2, ... n
$$

**from Dalton's law of constant total pressure** 

$$
P_{\text{tot}} = P_{\text{inert}} + \sum_{i=1}^{k} P_i
$$

**and from the constancy of the mass-balance of the gaseous constituents of the systems** 

$$
{}^{\circ}P_{\mathbf{a}} = \sum_{i=1}^{\kappa} \gamma_{\mathbf{a}} P_i
$$

where  $P_i$  = partial pressure of the i-th component (atm),  $v_{ij}$  = reaction coefficient of the i-th component for the j-th equilibrium reaction,  $K_{p_j}$  = temperature dependent **reaction constant for the j-th equilibrium relation,** *"P, =* **input pressure of constituent a, and**  $y_2$  **= constitution coefficient of constituent a in the i-th component. In the** following calculations the pressure of the inert gas  $P_{\text{inert}}$ , has always be assumed to be more than 90% of the total pressure  $P_{tot}$  of the system. While the mass-balances of **the gaseous constituents are always constant, the mass-balance of the heterogeneous constituent may vary with temperature.** 

**Thermodynamic equilibrium data have been taken from the JANAF- Thermo**chemical Tables<sup>3</sup> or have been estimated using empirical relations for the reaction **enthalpies and entropies by comparison with the tungsten-chlorine or the tungsten**fluorine system<sup>4,5</sup>. For the tungsten-bromine compounds the data used are tabulated in Table 1 for temperatures from 1000-4000 K.

**TABLE 1** 

Compound	$log K_{\rm p}$				Reference
	1000 K	2000 K	3000 K	4000 K	
<b>WBr</b>	$-23.87$	$-9.20$	$-4.42$	$-2.15$	3
WBr <sub>2</sub>	$-2.35$	0.47	1.36	1.71	8
WBr.	6.51	1.05	$-0.76$	$-1.74$	4
WBr <sub>s</sub>	5.12	$-1.78$	$-4.02$	$-5.19$	
<b>WBr</b>	3.09	$-5.19$	$-7.85$	$-9.22$	
WOB <sub>L</sub>	13.82	2.87	$-0.78$	$-2.47$	5
$WO_2Br_2$	23.68	9.24	4.41	2.08	5

**REACTION CONSTANT OF TUNGSTEN BROMIDES AND TUNGSTENOXIDE BROMIDES** 

**Calculations have been performed on a Siemens 4OO4/45 computer for temperatures between 500 and 4OOO K at 100 K intervais for bromine concentrations**  from  $10^{-1}$  to  $10^{-6}$  atm, bromine to hydrogen ratios from 4:1 to 1:3 and bromine to oxygen ratios from 10:1 to 1:4. The presence of carbon was considered for the case of **methylenebromide CH,Br, and for the addition of abon dioxide or carbon monoxide.** 

## **THEORETICAL RESULTS AND LAMP EXPERIMENTS**

**The thermodynamic equilibrium calculations generally yield more or less steep gradients in partiai pressures of the reaction components with temperature, which will give rise to diffusion processes. As long as the mass-balance of the heterogeneous** 

constituent is constant, these material fluxes produce and annihilate themselves by dissociation or recombination. But if there exists a gradient in the material balance, transport of matter arises in **the** direction down the actual gradient. The possibiIity of a chemical transport reaction can therefore be predicted from the temperature dependence of the mass-balance of the heterogeneous constituent. The direction of transport being given by the gradient of the mass-balance: i.e., positive gradient, tungsten transport from hot to cold; negative gradient, tungsten transport from cold



Fig. 1 (left). Schematic diagram of the temperature dependence of the mass-balance of tungsten in a **tungsten-halogen s\_ystem\_** 

**Fig. 2** (right). **Schematic diagram of thermodynamic conditions for blackening and no-blackening of the buIb-waII of haiogcn-incandescent lamps.** 



**Fig\_ 3. Temperature dcpendencc of gas-phase composition in the tungsten-bromine system;**   $^{9}P_{\text{Br2}} = 10^{-3}$  atm.

to hot. Thus, the mass-balance may be obviously looked upon as solubility of tungsten in the vapour phase.

A schematic diagram of the temperature dependence of the mass-balance of tungsten in the halogen systems is given in Fig. 1 showing the direction of transport and the corresponding areas of ablation or deposition of material. These considerations lead to the following conclusion for the performance of a tungsten-halogen lamp: As tungsten transport is always proceeding in a direction from a high to a low value of the mass-balance of tungsten there will be blackening of the bulb-wall if at the temperature of the filament this value is higher than at the temperature of the wall and vice versa. A schematic diagram of this condition for blackening and noblackening of the wall of an incandescent lamp is given in Fig. 2.

The temperature dependence of the distribution of partial pressures in the tungsten-bromine system is shown in Fig. 3 for a bromine input pressure of  $10^{-3}$  atm. Main component of the vapour phase is tungsten tetrabromide at low temperatures and atomic bromine at high temperatures. MoIecular bromine and tungsten dibromide are only of minor importance at medium temperatures. A plot of the tungsten mass-balance in the tungsten-bromine system against temperature, normalized with respect to the bromine input pressure, is given in Fig. 4. As can be seen from the



Fig. 4. Temperature dependence of the mass-balance of tungsten in the tungsten-bromine system, **normalized to the bromine input pressure.** 

Fig. 5. Temperature dependence of the gas-phase composition in the tungsten-bromine-hydrogen system;  $Br_2:H_2 = 1:1$ ;  ${}^oP_{Br_2} = 10^{-3}$  atm.

**diam transport of tungsten is** possibIe in this **system** in a wide area of temperatures\_ At high temperatures tungsten transport proceeds from hot to cold, due to the net **evaporation of tungsten; at iow temperatures tungsten transport proceeds from cold to hot, due to the** dissociation **of the** tungsten bromides with increasing temperature-As may be inferred from these mass-balances blackening of the bulb-wall of incandescent Iamps can be prevented using bromine as regenerative getter, provided the halogen concentration exceeds  $10^{-5}$  atm. Furthermore, the well-known attack of the filament and of the supports at low temperatures is well explained by the high solubility **of** tungsten at these temperatures with **a vaIue of the mass-balance of 0.5, which corresponds to the formation of tungsten tetrabromide WBr,.** 

The problem of corrosion at the cold ends of the filaments can be improved using hydrogen bromide instead of elementary bromine, as has been proposed by **van Tijen6 and T'Jampens and van de Weijer '. The introduction of hydrogen into the reaction system, however,** is only partially successful. There is a strong interference of hydrogen with the tungsten-bromine system, as can be seen from a plot of the composition of the gas phase, Fig. 5, or a plot of the mass-balances in the tungstenbromine-hydrogen system for a constant ratio of' **l:I, Fig. 6, or for various ratios of bromine to hydrogen, Fig. 7.** :

![](_page_5_Figure_2.jpeg)

*Fig. d* **Temperature** *dependence of* **the mass-balance of tungsten in** *the* **tungsten-bromine-hydrogen**  system, normalized to the bromine input pressure;  $Br_2:H_2 = 1:1$ .

**Fig. 7. Temperature dependence of the mass-baiance of tungsten in the tungsten-bromine-hydrogen system. normaliz& to the bromine input pressure, for wrious ratios of bromine to hydrogen;**   $^{\circ}P_{\text{err}} = 10^{-3}$  atm.

At low and moderate temperatures hydrogen has a strondy reducing effect on the tungsten-bromine compounds, by which the chemical transport reactions are drastically influenced. Up to temperatures near 2000 K bromine is bound by hydrogen in the form of hydrogen bromide, thus decreasing the concentration of free bromine and tungsten bromides, the latter never reaching a value of 1% of the reaction components. By the presence of hydrogen in the tungsten-bromine system the regions of tungsten transport from hot to cold are severely reduced, while at lower temperatures the direction of transport may be completely reversed.

As to the transport processes in halogen-incandescent Iamps the presence of hydrogen, therefore, yields a strong deterioration or even complete suppression of the transport of tungsten from the wall back to the coil At the same time transport of material from hot to cold is, due to the reversed direction of transport, significantly enhanced. In lamp systems containing stoichiometric amounts of hydrogen needle-like or dendritic growth of tungsten crystals is much enlarged at medium temperatures where the curvature of the mass-balance exhibits a more or less pronounced minimum. At higher concentrations of hydrogen even blackening of the bulb may occur.

At those concentrations normally used in halogen-incandescent lamps the value of the mass-balance of tungsten at wall temperatures does not differ very much from the value at the temperature of the fiiament, especially for lamps with a high lumenper-watt output. Thus, there is always a dangerous tendency of wall-blackening to be

![](_page_6_Figure_3.jpeg)

**Fig. 8. Temperature dependence of gas-phase composition in the tungsten-bromine-oxygen system;**   $Br_2:O_2 = 1:1$ ;  $^{\circ}P_{Br_2} = 10^{-3}$  atm.

*expected.* **But due to the permanent presence of traces of oxygen in these lamps the**  value of the mass-balance at wall temperatures is raised by the formation of tungstenoxide bromide WO<sub>2</sub>Br<sub>4</sub> instead of tungsten tetrabromide WBr<sub>4</sub> such that this problem **is overcome in most cases.** 

**The temperature dependence of the gas-phase composition in the tungstenbromine-oxygen system is shown in Fig. 8 for a bromine input pressure of 10<sup>-3</sup> atm** and a bromine to oxygen ratio of 1:1. Most remarkable feature of the influence of **oxygen on the tungsten-bromine system is the formation of** *a* **mixed tungsten**oxygen-bromide compound, tungstenoxide bromide WO<sub>2</sub>Br<sub>2</sub>, at lower temperatures **and the formation of various tungstic oxides at higher temperatures\_ Characteristic is**  in oxygen containing systems, furthermore, the precipitation of solid tungstic oxide at **temperatures below 1500 K-**

**In general oxygen has an activating influence on the halogen cycle in incandescent lamps. By formation of a great variety of oxygen compounds the massbalance of tungsten is markedly increased at low and at moderate temperatures, thus**  increasing the solubility of tungsten in these temperature regions and enhancing the **transport processes. As can be seen from the plots of the mass-balances, Figs. 9 and 10, the direction of tungsten transport from cold to hot is not altered in these temperature regions as long as the oxygen concentration is not exceeding the concentration of bromine\_ If the oxygen concentration is higher there will be a decrease in the solubility of tungsten in the vapour phase at low temperatures due to the precipitation of solid tungstic oxide-**

**A further reaction constituent in the reaction systems of haiogen-incandescent lamps finally may be carbon. The presence of carbon, however, shows only inter**ferences in systems which contain oxygen. In oxygen-free systems there is practically

![](_page_7_Figure_4.jpeg)

**Fig. 9. Temperature dependence of the mass-balance of tungsten in the tungsten-bromine-oxygen**  system, normalized to the bromine and oxygen input pressure;  $Br_2:O_2 = 1:1$ .

Fig. 10. Temperature dependence of the mass-balance of tungsten in the tungsten-bromine-oxygen **system, normalized to the bromine and oxygen input pressure, for various ratios of bromine to**   $oxygen; °P_{Br_2} = 10^{-3}$  atm.

no interference of carbon in the distribution of partial pressures of the reaction components. At moderate temperatures compounds and radicals such as  $C_2H_2$ , CH,  $CH_2$ , ... may be found, but their concentrations are so low that there is no influence on transport characteristics.

In systems, however, containing oxygen as secondary constituent the presence of carbon exhibits a strong interference. At low temperatures formation of carbon dioxide and at high temperatures formation of carbon monoxide is found. The stability of carbon monoxide is such that up to stoichiometric compositions of carbon monoxide all oxygen is extracted from the reaction systems. Thus, carbon is an excellent getter for oxygen in halogen-incandescent lamps. In the tungsten-bromine system the stability of the tungstenoxide bromide  $WO_2Br_2$  is dominant at very low temperatures in the stabihty region of carbon dioxide only. At higher temperatures tungstenoxide bromide and tungstic oxides are only found if the ratio of oxygen to carbon in these systems is higher than the stoichiometry in carbon monoxide. The temperature dependence of the gas-phase composition is shown in Fig. 11 and Fig. 12

![](_page_8_Figure_2.jpeg)

Fig. 11. Temperature dependence of gas-phase composition in the tungsten-bromine-carbon dioxide system;  ${}^{\circ}P_{Br_2} = 10^{-3}$  atm.

Fig. 12. Temperature dependence of gas-phase composition in the tungsten-bromine-carbon monoxide system;  ${}^{\circ}P_{Br_2} = 10^{-3}$  atm.

for the presence of carbon dioxide and carban monoxide in the tungsten-bromine system. The mass-balances in these reaction systems, Fig. 13 and Fig. 14, therefore, show the characteristics of the oxygen-free systems unless the stoichiometric composition of carbon monoxide is exceeded. Thus, as could be experimentally shown<sup>8</sup>, it is far more advantageous for a good performance of any incandescent lamp to use carbon monoxide as oxygen-additive than to use oxygen in elementary form. In the Iatter case an excess of oxygen would enhance the transport of material in the high temperature region and would Iead to shortening of lamp life, whereas in the former case an excess **of carbon monoxide would result in no alteration of transport**  behaviour.

![](_page_9_Figure_1.jpeg)

Fig. 13. Temperature dependence of the mass-balance of tungsten in the tungsten-bromine-carbon dioxide system, normalized to the bromine and oxygen input pressure.

Fig. 14. Temperature dependence of the mass-balance of tungsten in the tungsten-bromine-carbo monoxide system, normalized to the bromine and oxygen input pressure.

## **MECHAXISM OF THE HALOGEX CYCLE**

The interference of the secondary constituents in the reaction systems of halosen-incandescent lamps can be described **in a somewhat simplifying manner as foIIows:** 

**i)** Oxygen acts like an activator in the tungsten-bromine cycle. Transport of tungsten from coId to hot is shifted towards higher temperatures.

ii)  $Hydrogen$  acts as inhibitor in the tungsten-halogen cycle. Due to the formation of hydrogen bromide the mass-balance of tungsten **is** degrading towards lower temperatures reversing the direction of tungsten transport.

iii) *Carbon* **exhibits** no interference in oxygen-free systems. In systems containing oxygen as further secondary constituent carbon acts as excellent getter for oxygen, forming carbon monoxide at moderate and high temperatures\_ In systems containing water, oxygen is gettered by carbon and, therefore, the transport characteristics of hydrogen interference are found.

The thermodynamic calcuiations cannot absolutely predict what will happen in an actual reaction system, as many reactions which are thermodynamically possible are hindered by kinetic factors or by gas convection. The thermodynamic equilibrium calcuiations, however, generally give the limits of the reactions which might be reached,

**thus forming a reliabIe basis for the understanding of transport processes in halogenincandescent lamps.** 

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