# THERMAL DECOMPOSITION STUDIES ON ETHYLXANTHATO COMPLEXES OF IRON AND NICKEL

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### ABSTRACT

Thermal decompositional studies on bis-ethylxanthato-nickel(II) and tris-ethylxanthato-iron(III) were carried out leading to stoichiometric, dirty green-coloured, NiO and  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> When a mixture of the xanthato complexes containing a Ni Fe atom ratio of 1 2 was decomposed, a mixed metal oxide nickel ferrite, NiFe<sub>2</sub>O<sub>4</sub>, could be obtained at about 700°C Kinetic parameters such as the activation energy,  $E_a$ , and the order of the reaction, n, were calculated using the methods of Freeman and Carroll, Arrhenius, and Borchardt and Daniels The composition,  $E_a$ , and composition-decomposition temperature diagrams were found to be clearly indicative of the formation of a definite reaction product at a certain composition Mechanistic and non-mechanistic approaches have been compared and it was found that most of the processes were explained by the Mampel relation The characterization of the decomposition products was made using X-ray and Mössbauer studies.

# INTRODUCTION

The thermal analysis of metal complexes containing sulphur ligands are rather less extensively studied. For example, tris-ethylxanthato-iron(III), Fe(xan)<sub>3</sub>, has been overlooked [1] for thermal studies, may be because of its impure nature even after repeated recrystallisations. The thermal decomposition of metal xanthates yields corresponding metal sulphides and volatile organic matter, containing CS<sub>2</sub>, COS etc. The study of volatile organic matter has been done [2] by gas chromatography and mass spectrometry. To explain the formation of gaseous products it has been proposed that the first step involves the rupture of C–S bonds producing metal sulphides and a mixture of gases. But there are few reports about the characterization of the residues containing the metal. A number of reports [3–6] may be found on the thermal decomposition of Mi(xan)<sub>2</sub>. The xanthates appear to be suitable for studying the formation of metal sulphides and/or oxides because of their low decomposition temperatures compared with other complexes.

The present study hopes to elucidate more of the kinetic and mechanistic aspects of the thermal decompositions of the pure metal xanthates of nickel(II) and iron(III) and their mixtures. The data on activation energies,  $E_a$ , have been interpreted on the basis of different methods of calculations.

#### EXPERIMENTAL

The complexes,  $Fe(xan)_3$  [7,8] and  $N_1(xan)_2$  [3] were prepared by the procedures reported.  $Fe(xan)_3$  was recrystallised twice from diethyl ether and was used immediately for subsequent studies. The elemental analyses of the starting compounds and of the major decomposition products were performed using standard methods [9].

The TG/DTA studies were performed on the thermobalance set up in the author's laboratory [10]. The characterization of the residues were based on Mossbauer and X-ray powder studies on typical samples.

# **RESULTS AND DISCUSSION**

The TG curve of  $N_1(xan)_2$ , Fig. 1, exhibits a major decomposition step between 190 and 240°C. The weight loss for this step is 70% and the residue analysed to be NiS. The second step from 650 to 700°C corresponds to a loss of 5.3% giving the stoichiometric oxide, NiO (a green \_:norphous powder). It was further confirmed from X-ray powder patterns.

The TG curve of  $Fe(xan)_3$ , Fig. 1, shows two steps. The first major decomposition step occurs in the range 110 to 140°C and the second in the range 200 to 240°C. The residues at these two steps were analysed to 1 ave the compositions  $FeS_3$  and  $FeS_2$ , respectively.

DTA showed that the two xanthato complexes meit at low temperatures. The mixtures of the two complexes in the molter state gave a homogeneous phase as evidenced from DTA studies, Fig. 2. Further decomposition of the melt leads to the formation of mixed metal sulphides and finally to the mixed metal oxides which are normally obtained by ceramic techniques [11]. The retention of the homogeneity in the solid phase of mixed metal sulphides could be presumed because of the isomorphous nature of the iron-sulphur and nickel-sulphur systems [12]. It was considered appropriate at this stage to evaluate the energetics of these decomposition reactions since these may throw light on the kinetics and mechanism.



Fig 1 TG, DTG and DTA curves of (a) Fe(xan)<sub>3</sub> and (b) Ni(xan)<sub>2</sub>





The kinetics of this reaction has, therefore, been studied using the methods outlined by Arrhenius [13] Freeman and Carroll [14] and Borchardt and Daniels [15]. The formation of mixed metal oxides has been studied by applying the methods of thermal analysis to samples containing mixtures of complexes in varying atom percentages of the two metals. A perspective view may be obtained from the TG/DTG/DTA curves in Fig. 2 and Tables 1 and 2.

The examination of the TG/DTA curves and the characterization of the residues at different stages for pure complexes and for their mixtures reveal the following interesting observations:

(i) The first endothermic DTA peak appears at 70°C for pure  $Fe(xan)_3$  and at 148°C for pure Ni(xan)<sub>2</sub>. It usually corresponds to the melting of the substance or some similar change leading to the destabilization of the state of the substance. The part of the DTA curves for the mixtures containing 10 to 40% of iron show a complex multiplet structure in this region; on the other hand the mixtures containing 50 to 70% of iron do not show such a structure. This is indicative of the fact that the melting of the substance is governed mostly by the content of the low melting Fe(xan)<sub>3</sub> in the mixture. The intensity of this peak is a maximum for the pure nickel complex. The position of the endothermic change remains fairly constant at 104°C for mixtures containing over 50% iron.

(ii) The two other DTA peaks of interest are the exothermic peaks; one in the decomposition region and the other in the first plateau region of the TG curve. These two peaks appear for pure  $Fe(xan)_3$  at 132 and 180°C and those for pure  $N_1(xan)_2$ , at 172 and 228°C. The sample containing 10% iron shows a DTA decomposition peak at 184°C which recedes towards lower temperatures with increasing iron content. The value of 152°C for the mixture containing 80% iron is slowly nearing the value of 132°C for pure Fe(xan)\_3. The trend observed in the DTA

TABLE I

Sample no	Composition	Temp range for loss (°C)	F Weight loss	Probable composition of the residue
1	Pure Ni(xan)2	188-260	70 0	NiS
2	10% Fe(xan)3 + 90% N1(xan)2	112-240	70 2	$N_1S + FeS_3$
3	20% Fe(xan) <sub>3</sub> + 80% Ni(xan) <sub>2</sub>	108-192	70 8	$N_1S + FeS_3$
4	30% Fe(xan) <sub>3</sub> + 70% N1(xan) <sub>2</sub>	96-176	715	$N_1S + FeS_3$
5	40% Fe(xan) <sub>3</sub> +60% N1(xan) <sub>2</sub>	104180	72 2	NIS+FeS3
6	50% Fe(xan)3 + 50% Ni(xan)2	112-176	716	$N_1S + FeS_3$
7	60% Fe(xan) <sub>3</sub> +40% N1(xan) <sub>2</sub>	104-172	64 07	NiS+FeS
8	70% Fe(xan)3 + 30% Ni(xan)2	120-180	65 4	$N_1S + FeS_3$
9	80% Fc(xan) <sub>3</sub> + 20% Ni(xan) <sub>2</sub>	128-200	68 2	$N_1S + FeS_3$
10	90% Fe(xan) <sub>3</sub> + 10% Ni(xan) <sub>2</sub>	120-180	68 7	$NiS + FeS_3$
11	Pure Fe(xan) <sub>3</sub>	108-140	69 8	FeS <sub>3</sub>
		200-240	53	$FeS + Fe_2O_3$ etc

TG Data for the  $Fe(xan)_3 - N_1(xan)_2$  system

# TABLE 2

Thermal parameters calculated using different relations

Simple	TG ª		DTG			DTA		
	n	$E_a$	A <sup>b</sup>		В <sup>с</sup>	A <sup>b</sup>		B '
			n	$E_{a}$ (kJ mole <sup>-1</sup> )	L <sub>a</sub> (kJ mole <sup>-1</sup> )	n	L <sub>a</sub> (kJ mole <sup>-1</sup> )	$L_{a}$ (kJ mole $^{-1}$ )
1	0 43	134 6	1 03	248 0	240 7	0 87	183 1	283 8
2	0 98	153 3	1.08	196 3	150 0	1 01	2116	1970
3	0 35	170 3	1 04	253 0	237 5	1 03	226 2	200 0
4	0 54	72 2	0 75	710	92 8	0 98	70 7	716
5	0 34	85.5	0 84	98 0	137 0	0 78	519	60 2
6	0 43	131 0	0 33	104 9	150 9	1 22	62 5	75 4
7	0 77	139.0	0 88	77 8	82 1	0 89	38 2	50 3
8	1 08	2197	1 40	1218	109 3	2 48	1816	90 1
9	0 80	180 0	1.03	101.2	85.5	0 87	69 6	79.6
10	0.78	164 0	1.08	109.0	92 5	0 82	92 1	101 ?
11	0 59	127 0	1 49	169 2	133 7	1 04	213 2	141 8

n =order of reaction;  $E_a =$ Activation energy

<sup>a</sup> using Freeman and Carroll's relation

<sup>b</sup> using Arrhenius relation

<sup>4</sup> using Borchardt and Daniels' relation

peak for structural transformations in the plateau region of a TG curve is peculiar for the three compositions, with increasing iron content from 50-70%. It appears that the structural and compositional changes have overlapped on each other producing a broad DTA peak extending beyond the limit of the TG loss curve. For the other compositions there is a multiplet structure of DTA peaks. This supports the idea of the formation of a definite composition over this region. Compared with the DTA curves of other compositions, those of these three compositions are simple in appearance.

(iii) The examination of the TG curves gives the changes observable due to the addition of increasing amounts of  $Fe(xan)_3$  to  $Ni(xan)_2$ . For both pure complexes there is a clear single step loss with a steep slope. The temperature range of decomposition for the first step is between 50°C for  $Fe(xan)_3$  and 80°C for the Ni(xan)<sub>2</sub>, given in Table 1. Such a single step is observable for the TG curves of the mixtures containing 50–80% iron, but the slopes are not as steep as those for pure complexes. The DTG curves for all the remaining compositions are suggestive of two components in the decomposition process, as the two slopes are evident from TG curves. However, the two steps are not separated but appreciably overlap each other.

(iv) The plot of the starting temperature of the decomposition for different compositions exhibits a fairly good trend similar to the variation in boiling point of two miscible liquids [16]. Figure 3 shows a fall in temperature for the mixtures containing 0-40% iron. A small increase is observed for 50\% iron composition and



Fig 3 A plot of the decomposition temperatures of Fe(xan)3 and Ni(xan)2 against atom percent of Fe

again at the compositions of 70 and 80%. This shows a break in the general trend possibly because a different chemical process may be operating at these compositions.

Table 1 gives the TG data on the pure complexes and their mixtures. The probable composition of the residues has been ascertained on the basis of elemental analysis. Table 2 contains a comparative account of the kiretic parameters, such as the activation energy and the order of reaction calculated using the different relations referred to previously. Figure 4 presents a comparative account of these methods as a plot of activation energy against composition. The three methods do not agree in the magnitude of the activation energy but the data from any relationship do show a deviation at composition 50% and 60-80% of iron. The large deviation in the magnitude of  $E_a$ , may be due to the over simplification of the basic assumptions of each method and the inaccuracies in obtaining data for the different parameters. In Fig. 4, a subscript m signifies the  $E_a$  calculated manually, while c stands for computer tit, using the method of least squares; it has been found that the fitting parameter,  $\chi$  (chi) was always less than 0.05.



Fig 4 A plot of activation energy against composition

The inspection of the  $E_a$  values in Table 2 suggests that the trend observed in it is similar to the one reported [17].

It was worth attempting to elucidate the mechanism of these thermal decompositions. Satava [18] and Nair and Madhusudanan [19] have reviewed the different methods of thermal decompositions and proposed a unified approach to the elucidation of the different modes of decompositions on the basis of the fractions decomposing at unit time. The data on the fraction,  $\alpha$ , of the substance decomposed at temperature T were obtained from TG curves and were manipulated using the proposed relations. The relation that gives a straight line plot for log  $g(\alpha)$  against 1/T indicates the appropriate mechanism. It is found in the present work that the random nucleation mechanism [19] operates consistently with the Mampel equation. The agreement between the  $E_a$  values obtained from mechanism invoking and mechanism non-invoking relations was considered as the test for the correct operating mechanism (Table 3).

On the basis of the compositions of the residues (Table 1) the product obtained at 750°C containing 66% iron was analysed by Mossbauer and X-ray diffraction studies. Table 4 contains the data for Mossbauer parameters for a Fe:Ni composition of 2:1.

The product isolated at 750°C is expected to be nickel ferrite which is known to have  $Fe^{3+}$  (high-spin) configuration. The  $\delta$  values observed in the present work are given in Table 4, and are found to fall in this compound (within an experimental error of  $\pm 0.08$  mm sec<sup>-1</sup>) in the range of  $\delta$  values for  $Fe^{3+}$  [20].

The confirmation of the formation of nickel ferrite may be seen from the close agreement between the X-ray parameters, d, for the compound prepared by the

#### TABLE 3

Sample no	$E_{\rm a}$ (kJ m	Remarks					
	Non-me	chanistic equ	ation	Mechani	stic equation		
	a	b	с	d	e	ſ	
1	134 6	248 0	240 5	3170	139 0	99 0	c (a)
2	153 3	196 0	150 3	438 0	232 0	154 0	f (a and c)
3	170 3	233 0	237 5	247 0	1270	86 0	d (b and c)
4	72 2	710	92 9	73 2	39 2	28 0	d (a and b)
5	85 5	98 0	137 0	<b>99</b> 0			d (b)
6	131 0	104 0	150 9	95 2	46 5	22 0	d (b)
7	1390	77 8	82 I	82 0			d (b and c)
8	219.0	121.8	109 3	92.0			d (c)
9	180.0	101 0	85 5	133 0	86 1		e (c)
10	164.0	109.0	92 5	140 0	72 0		d (a)
11	127.0	169 0	133 7	283 0	131 0	81.9	c (a, c)

Comparative account for  $E_a$  calculated from various relations

a, using Freeman and Carroll, b, using Arrhenius equation. c, using Borchardt and Daniels; d, using Mampel, c, using Avrami-I; f, using Avrami-II

Т	A	B	L	E	4

Set no	Chemical isomer shift (min sec <sup>-t</sup> ) wrt iron (8)	Quadrupole splitting (mm sec $^{-1}$ ) ( $\Delta E$ )	Internal magnetic field KG	Comments
Subsp	ectra A			
ł	0 09		495 09	$\Delta L$ locked to zero
				Line width locked to 0 256 mm sec $^{-1}$
2	0.06	0.21	497 7	Line width locked to 0 256 mm sec $^{-1}$
3	011		496 1	$\Delta E$ locked to zero
				Line width locked to 0 256 mm sec $^{-1}$
Subsp	ectra B			
1	0.44		504 69	$\Delta L$ locked to zero
				Line width locked to 0.32 mm see $^{-1}$
2	0.47		503 8	$\Delta L$ locked to zero
				Line width locked to 0.32 mm see <sup>-1</sup>
3	0.45	0.32	505 8	$\Delta L$ locked to zero

Mössbauer data for the system  $Fe(xan)_3 - Ni(xan)_2 = 2/1$ 

xanthate decomposition method and those reported for nickel ferrite [21] given in Table 5.

In conclusion it may be stated that the study of the variation of kinetic parameters with composition for a binary system appears to be a useful means of investigating phase transformations. The formation of nickel ferrite at low temperatures may be due to the formation of an unstable homogeneous molten phase derived from complexes with a low melting point.

**FABLE 5** 

X-Ray data for NiFe<sub>2</sub>O<sub>4</sub> [Fe(xan)<sub>3</sub> + Ni(xan)<sub>2</sub> (2 1), heated to 750°C]

	1	2	3	4	5	6	7	8	9
Ohsei	l ed		·····						
20	23 2°	25 6°	28 2°	38 4°	45 35°	47 4°	55 4°	69 5°	74 3°
0	11.6°	12.8°	14 0°	19 2°	22 67°	23 7°	27 7°	34 75°	37 15°
sın $ heta$	0 2011	0 2215	0 242	0 328	0 3855	0 4019	0 4648	0 5681	0 6039
d	4 817	4 37	40	2 94	2 512	2 425	2 083	1 725	1 6039
æ	11.0	27 0	150	20 0	100 0	10 0	20.0	150	22 0
Repor	ted								
d	4 82			2 95	2 51	241	2 08	1 70	1 60
ç	70			20 0	100 0	50	23 0	13 0	33.0
hkl	111			220	311	222	400	422	511

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