# THERMAL DECOMPOSITION STUDIES ON ETHYLXANTHATO **COMPLEXES OF IRON AND NICKEL**

G N. NATU, S B KULKARNI and P S DHAR

Department of Chemistry, University of Poona, Pune-411007 (India) (Received 20 May 1981)

## **ABSTRACT**

Thermal decompositional studies on bis-ethylvanthato-nickel(II) and tris-ethylxanthato-iron(III) were carried out leading to stoichiometric, dirty green-coloured, NiO and  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> When a mixture of the xanthato complexes containing a Ni Fe atom ratio of 1-2 was decomposed, a mixed metal oxide nickel ferrite, NiFe<sub>2</sub>O<sub>4</sub>, could be obtained at about 700°C Kinetic parameters such as the activation energy,  $E_a$ . and the order of the reaction, n, were calculated using the methods of Freeman and Carroll, Arrhenius, and Borchardt and Daniels The composition,  $E_a$ , and composition-decomposition temperature diagrams were found to be clearly indicative of the formation of a definite reaction product at a certain composition Mechanistic and non-mechanistic approaches have been compared and it was found that most of the processes were explained by the Mampel relation. The charactenzation of the decomposition products was made using X-ray and Mossbauer studies.

#### **INTRODUCTION**

The thermal analysis of metal complexes containing sulphur ligands are rather less extensively studied. For example, tris-ethylxanthato-iron(III),  $Fe(xan)<sub>3</sub>$ , has been overlooked [1] for thermal studies, may be because of its impure nature even after repeated recrystallisations. The thermal decomposition of metal xanthates yields corresponding metal sulphides and volatile organic matter, containing CS<sub>2</sub>, COS etc. The study of volatile organic matter has been done [2] by gas chromatography and mass spectrometry. To explain the formation of gaseous products it has been proposed that the first step involves the rupture of C-S bonds producing metal sulphides and a mixture of gases. But there are few reports about the characterization of the residues containing the metal. A number of reports [3-6] may be found on the thermal decomposition of  $Ni(xan)_2$ . The xanthates appear to be suitable for studying the formation of metal sulphides and/or oxides because of their low decomposition temperatures compared with other complexes.

The present study hopes to elucidate more of the kinetic and mechanistic aspects of the thermal decompositions of the pure metal xanthates of nickel(II) and iron(III) and their mixtures. The data on activation energies,  $E_a$ , have been interpreted on the basis of different methods of calculations.

## **EXPERIMENTAL**

The complexes. Fe(xan), [7,8] and  $N_1(xan)$ , [3] were prepared by the procedures reported. Fe(xan), was recrystallized twice from diethyl ether and was used immediately for subsequent studies. The elemental analyses of the starting compounds and of the major decomposition products were performed using standard methods 191.

The TG/DTA studies were performed on the thermobalance set up in the author's laboratory [IO]. The characterization of the residues were based on Mossbauer and X-ray powder studies on typical samples.

## **RESULTS AND DISCUSSIOh**

The TG curve of  $N_1(xan)_2$ , Fig. 1, exhibits a major decomposition step between 190 dntl **240°C.** The weight loss for this step IS 70% and the residue analysed to be NIS. The second step from 650 to 700°C corresponds to a loss of 5.3% givmg the stoichiometric oxide. NiO (a green .:norphous powder). It was further confirmed from X-ray powder patterns.

The TG curve of  $Fe(xan)<sub>3</sub>$ , Fig. 1, shows two steps. The first major decomposition step occurs in the range 110 to 140°C and the ,econd m the range **200** to **240°C.** The residues at these two steps were analysed to ! ave the compositions  $FeS<sub>3</sub>$  and  $FeS<sub>2</sub>$ , respectively.

DTA showed that the two xanthato complexes meit at low temperatures. The mixtures of the two complexes in the molter state gave a homogeneous phase as evidenced from DTA studies, Fig. 2. Further c'ecomposttion of the melt leads to the formation of mixed metal sulphides and finally to the mixed metal oxides which are normally obtained by ceramic techniques [11]. The retention of the homogeneity in the solid phase of mixed metal sulphides zould be presumed because of the isomorphous nature of the iron-sulphur and nickel-sulphur systems [12]. It was considered appropriate at this stage to evalua.e the energetics of these decomposition reactions since these may throw light on the kinetics and mechanism.



Fig 1 TG, DTG and DTA curves of (a) Fe(xan)<sub>2</sub> and (b) N<sub>1</sub>(xan)<sub>2</sub>



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Fig 2 TG (------), DTG ( $\times$  -------  $\times$ ) and DTA (--) curves of the mixtures of complexes in varying atom percentages of Fe and Ni. (a) 10% Fe(xan)<sub>3</sub>, 90% Ni(xan)<sub>2</sub>, (b) 20% Fe(xan)<sub>3</sub>, 80% N<sub>1</sub>(xan)<sub>2</sub>: (c) 30% Fe(xan)<sub>3</sub>, 70% Ni(xan)<sub>2</sub>, (d) 40% Fe(xan)<sub>3</sub>, 60% Ni(xan)<sub>2</sub>, (e) 50% Fe(xan)<sub>3</sub>, 50% Ni(xan)<sub>2</sub>, (f) 60% Fe(xan)<sub>3</sub>, 40% Ni(xan)<sub>2</sub>; (g) 70% Fe(xan)<sub>3</sub>, 30% Ni(xan)<sub>2</sub>; (h) 80% Fe(xan)<sub>3</sub>, 20%  $Ni(xan)<sub>2</sub>$ , (i) 90% Fe(xan)<sub>3</sub>, 10% N<sub>1</sub>(xan)<sub>2</sub>.

The kinetics of this reaction has, therefore, been studied using the methods outlined by Arrhenius [13] Freeman and Carroll [ 141 and Borchardt and Daniels [IS]. The formation of mixed metal oxides has been studied by applying the methods of thermal analysis to samples containing mixtures of complexes in varying atom percentages of the two metals. A perspective view may be obtained from the TG/DTG/DTA curves in Fig. 2 and Tables 1 and 2.

The examination of the  $TG/DTA$  curves and the characterization of the residues at different stages for pure complexes and for then mixtures reveal the following Interesting observations:

(i) The first endothermic DTA peak appears at 70 $\degree$ C for pure Fe(xan)<sub>3</sub> and at 148°C for pure  $Ni(xan)_2$ . It usually corresponds to the melting of the substance or some similar change leading to the destabilization of the state of the substance. The part of the DTA curves for the mixtures containing 10 to 40% of iron show a complex multipiet structure m this region; on the other hand the mixtures containing 50 to **70%** of iron do not show such a structure. This is indicative of the fact that the melting of the substance is governed mostly by the content cf the low melting  $Fe(xan)$ , in the mixture. The intensity of this peak is a maximum for the pure nickel complex. The position of the endothermic change remains fairly constant at  $104^{\circ}$ C for mixtures containing over 50% iron.

(ii) The two other DTA peaks of interest are the exotherrmc peaks; one in the decomposition region and the other in the first plateau region of the TG curve. These two peaks appear for pure  $Fe(xan)_3$  at 132 and 180°C and those for pure  $Ni(xan)$ , at 172 and 228°C. The sample containing 10% iron shows a DTA decomposition peak at  $184^{\circ}$ C which recedes towards lower temperatures with increasing iron content. The value of 152°C for the mixture containing 80% iron is slowly nearing the value of 132°C for pure  $Fe(xan)$ , The trend observed in the DTA

TABLE I

Sample no.	Composition	Temp range for loss $(^{\circ}C)$	<b>E</b> Weight loss	Probable composition of the residue.
	Pure $Ni(xan)$ <sub>2</sub>	188–260	700	$N_{1}S$
2	10% Fe(xan), $+90\%$ N <sub>1</sub> (xan),	$112 - 240$	70.2	$N_1S + FcS_1$
3	20% Fe(xan), $+80\%$ Ni(xan),	$108 - 192$	708	$N_1S + FeS_2$
4	30% Fe(xan) <sub>3</sub> + 70% N <sub>1</sub> (xan) <sub>2</sub>	$96 - 176$	715	$N_1S + FeS_2$
5	40% Fe(xan), $+60\%$ N <sub>1</sub> (xan),	$104 - 180$	722	$N_1S + FcS_1$
6	50% Fe(xan) <sub>3</sub> + 50% N <sub>1</sub> (xan) <sub>2</sub>	$112 - 176$	716	$N_1S + FcS_3$
7	60% Fe(xan) <sub>3</sub> + 40% N <sub>1</sub> (xan) <sub>2</sub>	$104 - 172$	64.07	$N_1S + FeS_2$
8	70% Fe(\an) <sub>3</sub> + 30% N <sub>1</sub> (xan) <sub>2</sub>	$120 - 180$	654	$N_1S + FeS_2$
9	$80\%$ Fe(\an), $+20\%$ Ni(\an),	$128 - 200$	68.2	$N_1S + FeS_2$
10	90% Fe(xan), $+10\%$ Ni(xan),	120-180	687	$N_1S + FeS_2$
п	Pure $Fe(xan)3$	$108 - 140$	69 8	Fes <sub>1</sub>
		$200 - 240$	53	$FeS + Fe2O3$ etc

TG Data for the Fe(xan)<sub>3</sub> - N<sub>1</sub>(xan)<sub>2</sub> system

## TABLE 2

Thermal parameters calculated using different relations

Sample no	TG <sup>a</sup>		<b>DTG</b>			<b>DTA</b>			
	$\boldsymbol{n}$	$E_a$ $(kJ \text{ mole}^{-1})$	$A^b$		$B^{\mu}$	A <sup>b</sup>		$B^{\mu}$	
			$\boldsymbol{n}$	$E_{\rm a}$	$L_{\rm a}$ (kJ mole <sup><math>-1</math></sup> ) (kJ mole <sup><math>-1</math></sup> )	$\boldsymbol{\mathcal{H}}$	$L_{\rm a}$ $(kJ \text{ mole}^{-1})$	$L_{\rm a}$ $(kJ \text{ mole}^{-1})$	
	043	1346	103	2480	2407	087	1831	2838	
2	098	1533	1.08	1963	1500	101	2116	1970	
3	0 3 5	1703	104	2530	2375	103	2262	2000	
4	054	722	075	710	928	098	70 7	716	
5	034	85.5	084	980	1370	078	519	602	
6	043	1310	033	1049	1509	122	62 <sub>5</sub>	754	
7	077	139.0	088	778	821	089	382	503	
8	108	2197	140	1218	1093	248	1816	90 1	
9	080	1800	1.03	101.2	85.5	087	696	79,6	
10	0.78	1640	1.08	109.0	925	082	921	101.2	
11	059	1270	<b>149</b>	1692	1337	104	2132	1418	

 $n =$  order of reaction;  $E_a =$  Activation energy

<sup>a</sup> using Freeman and Carroll's relation

<sup>b</sup> using Arrhenius relation

' using Borchardt and Daniels' relation

peak for structural transformations in the plateau region of a TG curve is peculiar for the three compositions, with increasing iron content from 50-70%, It appears that the structural and compositional changes have overlapped on each other producing a broad DTA peak extending beyond the limit of the TG loss curve. For the other compositions there is a multiplet structure of DTA peaks. This supports the idea of the formation of a definite composition over this region. Compared with the DTA curves of other compositions, those of these three compositions are simple in appearance.

(iii) The examination of the TG curves gives the changes observable due to the addition of increasing amounts of  $Fe(xan)_3$  to Ni $(xan)_2$ . For both pure complexes there is a clear single step loss with a steep slope. The temperature range of decomposition for the first step is between 50°C for Fe(xan)<sub>3</sub> and 80°C for the Ni(xan),, given in Table 1. Such a single step is observable for the TG curves of the mixtures containing SO-80%iron, but the slopes are not as steep as those for pure complexes. The DTG curves for all the remaining compositions are suggestive of two components in the decomposition process, as the two slopes are evident from **TG curves.** However, the two steps are not separated but appreciably overlap each other.

(iv) The plot of the starting temperature of the decomposition for different compositions exhibits a fairly good trend similar to the variation in boiling point of two miscible liquids (161. Figure 3 shows a fall in temperature for the mixtures containing 040% iron. A small increase is observed for 50% iron composition and



Fig 3 A plot of the decomposition temperatures of  $Fe(xan)$ , and N<sub>1</sub>(xan), against atom percent of Fe

again at the compositions of 70 and 80%. This shows a break m the general trend possibly because a different chemical process may be operating at these compos tions.

Table 1 gives the TG data on the pure complexes and their mixtures. The probable composition of the restdues has been ascertained on the basis of elemental analysis. Table 2 contams a comparative account of the kinetic parameters, such as the activation energy and the order of reactron calculated usmg the different relations referred to previously. Figure 4 presents a comparative account of these methods as a plot of activaticn energy egamst composition. The three methods do not agree m the magnitude of the activation energy but the data from any relationship do show a deviation at composition 50% and 60-808 of iron. The large deviation in the magnitude of  $E<sub>a</sub>$ , may be due to the over simplification of the basic assumptions of each method and the inaccuracies in obtaining data for the different parameters. In Fig. 4, a subscript m signifies the  $E_a$  calculated manually, while c stands for computer fit, usmg the method of least squares; it has been found that the fitting parameter,  $\chi$  (chi) was always less than 0.05.



Fig 4 A plot of activation energy against composition

The inspection of the  $E_a$  values in Table 2 suggests that the trend observed in it is similar to the one reported [17].

It was worth attempting to elucidate the mechanism of these thermal decompositions. Satava 1181 and Nair and Madhusudanan [19] have reviewed the different methods of thermal decompositions and proposed a unified approach to the elucldation of the different modes of decompositions on the basis of the fractions decomposing at unit time. The data on the fraction,  $\alpha$ , of the substance decomposed at temperature *T* were obtained from TG curves and were manipulated **using** the proposed relations. The relation that gives a straight line plot for  $\log g(\alpha)$  against **l/T indicates the appropriate mechanism. It is found** in the present work that the random nucleation mechanism [19] operates consistently with the Mampel equation. The agreement between the  $E_a$  values obtained from mechanism invoking and mechanism non-invoking relations was consldered as the test for the correct operating mechanism (Table 3).

On the basis of the compositions of the residues (Table 1) the product obtained at  $750^{\circ}$ C containing 66% iron was analysed by Mossbauer and X-ray diffraction studies. Table 4 contains the data for Mossbauer parameters for a Fe : Ni composition **of 2: 1.** 

The product isolated at  $750^{\circ}$ C is expected to be nickel ferrite which is known to have Fe<sup>3+</sup> (high-spin) configuration. The  $\delta$  values observed in the present work are given in Table 4, and are found to fall in this compound (within an experimental error of  $\pm 0.08$  mm sec<sup>-1</sup>) in the range of  $\delta$  values for Fe<sup>3+</sup> [20].

The confirmation of the formation of nickel ferrite may be seen from the close agreement between the X-ray parameters, *d,* for the compound prepared by the

## TABLE 3

Sample	$E_a$ (kJ mole <sup>-1</sup> ) calculated from	<b>Remarks</b>					
no		Non-mechanistic equation			Mechanistic equation		
	a	b	$\mathbf c$	d	e		
	1346	2480	240 5	3170	1390	990	c(a)
2	1533	1960	1503	4380	2320	1540	$f$ (a and c)
3	1703	2330	237.5	2470	1270	860	$d$ (b and c)
4	722	710	929	73 2	392	280	$d$ (a and b)
5	855	980	1370	990			d(b)
6	1310	1040	1509	952	46.5	220	d(b)
	1390	778	82 I	820			$d$ (b and c)
8	219.0	121.8	1093	92.0			d(c)
9	180.0	1010	855	1330	86 1		c(c)
10	164,0	109.0	92 <sub>5</sub>	1400	720		d(a)
11	127.0	1690	1337	2830	1310	819	c(a, c)

Comparative account for  $E_a$  calculated from various relations

a, using Freeman and Carroll, b, using Arrhenius equation. c. using Borchardt and Daniels; d, using Mampel, c, using Avrami-I; f, using Avrami-II



Set no	Chemical isomer shift $(mm sec-1)$ wrt iron $\langle \delta \rangle$	Quadrupole splitting (mm sec <sup><math>-1</math></sup> ) $(\Delta E)$	Internal magnetic field КG	Comments
	Subspectra 4			
	0.09		495.09	$\Delta L$ locked to zero
				Line width locked to 0.256 mm sec $^{-1}$
$\overline{2}$	0.06	0.21	4977	Line width locked to 0.256 mm sec $^{-1}$
3	011		4961	$\Delta E$ locked to zero.
				Line width locked to 0.255 mm sec $^{-1}$
	Subspectra B			
	() 44		504.69	$\Delta L$ locked to zero.
				Line width locked to 0.32 mm see $^{-1}$
$\mathbf{r}$	$0 - 17$		5038	$\Delta L$ locked to zero
				Line width locked to 0.32 mm sec $^{-1}$
3	045	0.32	505.8	$\Delta L$ locked to zero.

Mössbauer data for the system  $Fer(xan)_x - Nf(xan)_z = 2/4$ 

xanthate decomposition method and those reported for nickel ferrite [21] given in Table 5.

In conclusion it may be stated that the study of the variation of kinetic parameters with composition for a binary system appears to be a useful means of investigating phase transformations. The formation of nickel ferrite at low temperatures may be due to the formation of an unstable homogeneous molten phase derived from complexes with a low melting point.

TABLE 5

X-Ray data for NiFe,  $O_4$  [Fe(xan)<sub>3</sub> + Ni(xan)<sub>2</sub> (2-1), heated to 750°C]

	$\bullet$								
				4	5	6	7	8	9
Ohsen ed									
$2\theta$	$23.2^{\circ}$	$256^\circ$	28.2°	$384^\circ$	$45.35^{\circ}$	$47.4^{\circ}$	$55.4^\circ$	69.5°	$74.3^{\circ}$
0	$116^\circ$	128°	140°	192°	$22.67^{\circ}$	$237^\circ$	$27.7^{\circ}$	3475°	$3715^\circ$
$sin \theta$	0.2011	0.2215	0.242	0.328	03855	0.4019	04648	0.5681	06039
$\boldsymbol{d}$	4817	$-1, 37$	40	294	2512	2425	2083	1725	16039
Æ	110	270	150	200	1000	100	20 O	150	220
Reported									
d	482			295	251	241	208	170	160
ę.	70			<b>200</b>	1000	50	230	130	33.0
hkl	111			220	311	222	400	422	511

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