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## Effect of rapid sintering on the densification and the thermal diffusivity of  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet

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#### **Abstract**

Effect of a rapid sintering on the densification and the thermal diffusivity of undoped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet has been studied and compared with those of TiO<sub>2</sub>-doped Li<sub>2</sub>TiO<sub>3</sub> pellet by using a push rod type vertical furnace and a laser flash method. The density of a rapidly sintered undoped Li<sub>2</sub>TiO<sub>3</sub> pellet was remarkably increased and it was similar to those of the conventionally sintered  $TiO<sub>2</sub>$ -doped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellets. The thermal diffusivity of the rapidly sintered undoped  $Li_2TiO_3$  pellet was also increased. It was similar to those of the conventionally sintered  $TiO_2$ -doped  $Li_2TiO_3$  pellets. Rapid sintering technique appears to be a possible means of improving the densification and the thermal properties of  $Li<sub>2</sub>TiO<sub>3</sub>$  without a TiO<sub>2</sub> doping.

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#### **1. Introduction**

Lithium-based ceramics, such as  $Li<sub>2</sub>O$ ,  $LiAlO<sub>2</sub>$ ,  $Li<sub>4</sub>SiO<sub>4</sub>$ ,  $Li<sub>2</sub>ZrO<sub>3</sub>$  and  $Li<sub>2</sub>TiO<sub>3</sub>$ , are being considered as promising solid breeder materials in the tritium breeding blanket of thermonuclear fusion reactors. The breeder material plays an important role in producing tritium atoms by a lithium transmutation,  ${}^{6}$ Li + n  $\rightarrow$  <sup>4</sup>He + T, where n is the neutron and T is the tritium. Among these candidates,  $Li<sub>2</sub>TiO<sub>3</sub>$  has been recently recognized as the leading candidate because of its prominent tritium release rate at low temperatures between 200 and 400  $°C$  [1,2] and its low activation characteristics.

Alvani et al. [3] reported that both the density and the grain size are key parameters in determining the tritium release rates. Provided the tritium release is not undul[y affect](#page-3-0)ed, a higher density is favorable from the viewpoint of the lithium loading and the lit[hium](#page-3-0)-6 enrichment. The density of lithium-based ceramics also has an effect on its thermo-mechanical performance which is a critical issue for assessing the reliability of solid breeder blanket concepts over the lifetime of the component [4].

For dense pebbles with a low open porosity (above 85% of the theoretical density), the grain size plays a major role in the tritium release rate, which is increased by decreasing the grain size and consequently by increasing the [grain](#page-3-0) boundaries. It is

suggested that the microstructural requirements of the  $Li<sub>2</sub>TiO<sub>3</sub>$ pebbles in the European Helium Cooled Pebble Bed (HCPB) Blanket design for a DEMO Fusion Reactor were 0.3–1.2 mm in diameter and ∼90% of the theoretical density.

Many studies on manufacturing  $Li<sub>2</sub>TiO<sub>3</sub>$  pebbles or pellets have reported that the sintering temperatures are from 1050 to  $1400\degree$ C and the sintering times are from 1 to 4 h. Lulewicz et al. [2] reported that a lithium deficient composition shows an improved microstructural stability and small grains during fabrication. However, there are few reports on the effect of the heating rate.

Rapid sintering, a sintering technique with a heating rate much faster than that in a conventional sintering, was proposed by Harmer and Brook [5] as a technique to suppress grain growth and to enhance densification. Recently, Chen and Wang [6] reported that fully dense cubic  $Y_2O_3$  with a grain size of 60 nm can be prepared by simple two-step sintering, a modified rapid sinterin[g](#page-3-0) [tech](#page-3-0)nique. In this study, a rapidly heated two-step sintering technique was conducted in undoped and  $TiO<sub>2</sub>$ -doped  $Li<sub>2</sub>TiO<sub>3</sub>$  systems in order to increase the sintered density. The thermal diffusivities of the two kinds of samples prepared by the different sintering schedules were compared.

#### **2. Experimental procedure**

Samples of TiO<sub>2</sub>-doped Li<sub>2</sub>TiO<sub>3</sub> pellets were prepared from  $Li<sub>2</sub>TiO<sub>3</sub>$  (Kosundo chemicals, 99.9% in purity) and  $TiO<sub>2</sub>$ 

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(Degussa, 99.9% in purity) powders. The  $0, 5$  and  $10$  mol% TiO<sub>2</sub>doped  $Li<sub>2</sub>TiO<sub>3</sub>$  powder mixtures were wet-milled for 24 h in ethyl alcohol using a polyethylene bottle and high purity zirconia balls. The dried slurry was isostatically pressed under 200 MPa into cylindrical compacts of about 8 mm in diameter and about 10 mm in height. The green densities of the compacts were about 58% of the theoretical density. The shrinkage behavior of the 0%, 5% and 10%  $TiO<sub>2</sub>$ -doped compacts in air was studied by using a push rod type dilatometer (Netzsch, Dil402C).

For the microstructural observation, the dried slurry was isostatically pressed under 200 MPa into discs of about 10 mm in diameter and about 2 mm in height. Some of the compacts were sintered at  $1050^{\circ}$ C for 1 h in air. The heating rate used for the above studies was 5 K/min. Others were rapidly heated to 1300  $\degree$ C, held for 10 min and immediately cooled to 1000  $\degree$ C. And then they were annealed at  $1000\degree C$  for 1 h in air. The heating rate of the rapid sintering was about 150 K/min. The sintered density was measured using the water immersion method. The microstructure and crystalline form were determined by an optical microscope and X-ray diffraction (XRD), respectively.

Sintered pellets were ground to around 1 mm in thickness, 8 mm in diameter and polished slightly to prepare the thermal diffusivity measurement. The thermal diffusivity was measured in the temperature range of 298–773 K by using a Laser Flash Apparatus (Netzsch, LFA-427). The measurements of the thermal diffusivity were performed three times at every test temperature step in a vacuum ( $10^{-4}$  to  $10^{-5}$  Pa).

#### **3. Results and discussion**

Fig. 1 shows the shrinkage behaviors of the 0%, 5% and 10% TiO<sub>2</sub>-doped Li<sub>2</sub>TiO<sub>3</sub> pellets in air plotted in the form of a percentage of the shrinkage versus the temperature. The onset of shrinkage occurs for the 0%  $TiO<sub>2</sub>$ -doped  $Li<sub>2</sub>TiO<sub>3</sub>$  at around  $1000$  °C. Those for the 5% and 10% TiO<sub>2</sub>-doped Li<sub>2</sub>TiO<sub>3</sub> occur at about 900  $\degree$ C, which is about 100  $\degree$ C lower than that for the  $0\%$  TiO<sub>2</sub>-doped Li<sub>2</sub>TiO<sub>3</sub>.



92 90 Density in % TD 88 86 84 82 80  $\mathbf 0$ 5 10 TiO<sub>2</sub> Content in mol %

Fig. 2. Sintered density of the conventionally sintered  $Li<sub>2</sub>TiO<sub>3</sub>$  pellets with various TiO<sub>2</sub> contents.

The addition of  $TiO<sub>2</sub>$  also results in a remarkable increase in the density during isothermal sintering. Fig. 2 shows the densities of the samples sintered at  $1050\,^{\circ}\text{C}$  for 1 h in air. Since the sintering temperature is considerably lower than the eutectic temperature of the  $Li_2O$ –TiO<sub>2</sub> system [7], the possibility of liquid phase sintering due to excess  $TiO<sub>2</sub>$  can be excluded. In the absence of a liquid phase, an enhancement of the densification by the excess  $TiO<sub>2</sub>$  can be accounted for by one of two possible mechanisms [8]. Firstly, the [exce](#page-3-0)ss  $TiO<sub>2</sub>$  may form point defects in the  $Li<sub>2</sub>TiO<sub>3</sub>$  lattice and thereby increase the diffusivities. Secondly, the excess  $TiO<sub>2</sub>$  may significantly retard the grain growth or inhibit an abnormal grain growth so that the pores are linked to [the g](#page-3-0)rain boundaries.

Fig. 3 shows the results of the XRD analysis of the isothermally sintered  $Li<sub>2</sub>TiO<sub>3</sub>$  pellets with various  $TiO<sub>2</sub>$  contents. The composition of the 5%  $TiO<sub>2</sub>$ -doped Li<sub>2</sub>TiO<sub>3</sub> is located near the TiO<sub>2</sub>-rich phase boundary of  $\beta$ -Li<sub>2</sub>TiO<sub>3</sub>. A small amount of the excess  $TiO<sub>2</sub>$  appears to be form the  $Li<sub>4</sub>Ti<sub>5</sub>O<sub>12</sub>$  phase. Small peaks of  $Li_4Ti_5O_{12}$  were observed in the TiO<sub>2</sub>-doped samples



Fig. 1. Shrinkage curves as a function of the temperature for various  $TiO<sub>2</sub>$ contents.

Fig. 3. X-ray diffraction patterns of sintered  $Li<sub>2</sub>TiO<sub>3</sub>$  pellets with various TiO<sub>2</sub> contents.



Fig. 4. Sintered density of the rapidly sintered  $Li_2TiO_3$  pellets with various  $TiO_2$ contents.

and the peak intensity of  $Li<sub>4</sub>Ti<sub>5</sub>O<sub>12</sub>$  became larger by increasing the excess  $TiO<sub>2</sub>$  content.

In order to increase the sintered density and to ensure a small grain size, the rapid sintering was conducted first in the  $Li<sub>2</sub>TiO<sub>3</sub>$ system. The samples were rapidly heated to  $1300\degree C$  and then annealed at  $1000\degree$ C for 1 h in air. The heating and cooling rates of the rapid sintering were about 150 K/min. Solid line in Fig. 4 indicates the densities of the rapidly sintered undoped and  $TiO<sub>2</sub>$ doped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellets. Dashed line refers to the densities of the conventionally sintered pellets.

The rapidly sintered undoped  $Li<sub>2</sub>TiO<sub>3</sub>$  sample has a very high density, around 89% of the theoretical density, without  $TiO<sub>2</sub>$  addition. This value is similar to those of the conventionally sintered  $TiO_2$ -doped  $Li_2TiO_3$  samples. In the case of the  $TiO<sub>2</sub>$ -doped  $Li<sub>2</sub>TiO<sub>3</sub>$ , the rapid sintering has little effect on the densification when compared with the conventionally sintered  $TiO<sub>2</sub>$ -doped  $Li<sub>2</sub>TiO<sub>3</sub>$ . Usually, the activation energy of the densification is larger than that of the grain boundary motion. Therefore, an effective densification can be achieved by a rapid heat treatment at high temperature for short time. This result suggests that the rapid sintering appears to be a possible means of improving the sintered density of undoped  $Li<sub>2</sub>TiO<sub>3</sub>$ .

Fig. 5 shows the optical micrographs of the polished and etched surfaces of the conventionally and rapidly sintered  $Li<sub>2</sub>TiO<sub>3</sub>$  pellets. The conventionally sintered samples in Fig. 5a–c have small grain sizes of about  $4 \mu m$ , which seemed to be irrelevant to the  $TiO<sub>2</sub>$  contents. However, grain sizes of the rapidly sintered samples in Fig. 5d–f are larger than those of the conventionally sintered samples. They have grain sizes of about  $12 \mu m$  for the undoped one and about 30  $\mu m$  for the TiO<sub>2</sub>-doped ones.

Rapid sintering in the  $Li<sub>2</sub>TiO<sub>3</sub>$  system remarkably enhances the densification, especially for the undoped  $Li<sub>2</sub>TiO<sub>3</sub>$ . The rapid sintering schedule of the present investigation does not ensure a small grain size when compared with those of the conventionally sintered samples. However, even if the densities of the rapidly sintered samples have similar values among the undoped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet and the TiO<sub>2</sub>-doped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellets, the grain size of the undoped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet is much smaller than those of the TiO<sub>2</sub>-doped Li<sub>2</sub>TiO<sub>3</sub> pellets. Rapid sintering appears to be a possible means of improving the densification of  $Li<sub>2</sub>TiO<sub>3</sub>$ with preserving a small grain size.

Temperature dependence on the thermal diffusivity of the  $Li<sub>2</sub>TiO<sub>3</sub>$  pellets is shown in Fig. 6. The thermal diffusivity



Fig. 5. Microstructures of the undoped and the TiO<sub>2</sub>-doped Li<sub>2</sub>TiO<sub>3</sub> pellets: (a–c) conventionally sintered at 1050 °C; (d–f) rapidly sintered at 1300 °C. Numbers indicate the contents of  $TiO<sub>2</sub>$  doping.

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Fig. 6. Temperature dependence of thermal diffusivity of  $Li<sub>2</sub>TiO<sub>3</sub>$ .

decreased with the temperature from around  $1.2 \times 10^{-6}$  m<sup>2</sup>/s at room temperature to about  $0.6 \times 10^{-6}$  m<sup>2</sup>/s at 773 K. Only the conventionally sintered undoped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet showed a slightly lower thermal diffusivity value for the whole temperature range. The others show similar values for the whole temperature range.

The lower thermal diffusivity of the conventionally sintered undoped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet could be attributed to the lower density. Saito et al. [9] expressed the density dependence on the thermal conductivity by the modified Maxwell–Eucken equation. They also reported that the thermal diffusivity of the  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet decreased with increasing the porosity.

It appears that the content of the  $TiO<sub>2</sub>$  doping has little effect on the thermal diffusivity of the sintered  $Li<sub>2</sub>TiO<sub>3</sub>$  pellets. The present finding is inconsistent with that of a previous study [10]. Hoshino et al. [10] compared the thermal diffusivity of a Li-deficient  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet with the literature values of a stoichiometric  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet [9,11]. They insisted that the thermal diffusivity of the nonstoichiometric  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet is higher than that of the stoichiometric  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet [10]. However, it seems that the processing variables might affect the thermal diffusivity of the  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet. By comparing the thermal diffusivity of the rapidly sintered undoped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet with those of  $TiO<sub>2</sub>$ -doped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellets, it appears to have similar thermal diffusivities for all the samples in Fig. 6.

### **4. Conclusion**

The densification kinetics of  $TiO<sub>2</sub>$ -doped samples were measured by using a push rod type dilatometer. Excess  $TiO<sub>2</sub>$ enhanced the shrinkage of the  $Li<sub>2</sub>TiO<sub>3</sub>$  compacts and increased the sintered density considerably. The rapid sintering was conducted in an undoped  $Li<sub>2</sub>TiO<sub>3</sub>$  system. The density of the rapidly sintered undoped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet remarkably increased and it was similar to that of the  $TiO<sub>2</sub>$ -doped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet. The thermal diffusivity of the rapidly sintered undoped  $Li<sub>2</sub>TiO<sub>3</sub>$  pellet also increased due to the enhanced densification. The present investigation suggests that the rapid sintering appears to be a possible means of improving the densification of  $Li<sub>2</sub>TiO<sub>3</sub>$  with preserving a small grain size.

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#### **References**

- [1] N. Roux, J. Avon, A. Floreancig, J. Mougain, B. Rasneur, S. Ravel, J. Nucl. Mater. 233–237 (1996) 1431.
- [2] J.D. Lulewicz, N. Roux, G. Piazza, J. Reimann, J. van der Laan, J. Nucl. Mater. 283–287 (2000) 1361.
- [3] C. Alvani, P.L. Carconi, S. Casadio, F. Pierdominici, in: J.V. van der Laan (Ed., NRG), Proceedings of the 7th International Workshop on Ceramic Breeder Blanket Interactions, Petten, 1998, pp. 4-69–4-80.
- [4] M.A. Abdou, N.B. Morley, A.Y. Ying, S. Smolentsev, P. Calderoni, Nucl. Eng. Tech. 37 (2005) 401.
- [5] M.P. Harmer, R.J. Brook, J. Br. Ceram. Soc. 80 (1981) 147.
- [6] I.-W. Chen, X.-H. Wang, Nature 404 (2000) 168.
- [7] H. Kleykamp, Fusion Eng. Des. 61–62 (2002) 361.
- [8] P. Balakrishna, B.P. Varma, T.S. Krishnan, T.R.R. Mohan, P. Ramakrishnan, J. Nucl. Mater. 160 (1988) 88.
- [9] S. Saito, K. Tsuchiya, H. Kawamura, T. Terai, S. Tanaka, J. Nucl. Mater. 253 (1998) 213.
- [10] T. Hoshino, M. Dokiya, T. Terai, Y. Takahashi, M. Yamawaki, Fusion Eng. Deg. 61–62 (2002) 353.
- [11] J.W. Davis, A.A. Haasz, J. Nucl. Mater. 232 (1996) 65.