

## Note

### AN EXTENSION OF THE METHOD OF ABOU-SHAABAN AND SIMONELLI FOR OBTAINING KINETIC PARAMETERS FROM TG DATA

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Numerous methods have been proposed for analyzing TG data to determine kinetic parameters. Abou-Shaaban and Simonelli have developed techniques based on several reaction cases [1]. In one of these, the reaction treated is



where  $A_s$  and  $B_s$  are solids and  $C_g$  is a gaseous product. These authors derived the relationship

$$\log \left[ \frac{-d(W'_{\text{obs}})dT}{(W^0_{\text{obs}}) - (W^0_{\text{obs}})/r} \right] = \log \frac{Z}{\beta} - \frac{E}{2.303RT} \quad (2)$$

where  $W'_{\text{obs}}$  is the observed sample weight at time  $t$ ,  $r$  is the ratio of the molecular weight of A to that of B,  $T$  is the temperature (K),  $\beta$  is the heating rate,  $Z$  is the frequency factor, and  $E$  is the activation energy. Thus, a plot of the left-hand side of eqn. (2) vs.  $1/T$  will yield a linear plot having a slope of  $-E/2.303R$ . However, the rate law assumed is

$$\frac{d(A'_s)}{dt} = -k(A'_s) \quad (3)$$

where  $A'_s$  is the weight of A present at time  $t$ . This rate law is that of a first-order process. The purpose of this communication is to provide an extension of this method to deal with cases other than the first-order case. We also present a computational scheme to carry out the process iteratively.

#### METHODS

Assuming the reaction to be studied is given by eqn. (1), it can be shown that

$$\alpha = \frac{W^0_{\text{obs}} - W'_{\text{obs}}}{W^0_{\text{obs}} - W^0_{\text{obs}}/r} \quad (4)$$

where  $W_{\text{obs}}^0$  is the initial weight of the sample,  $W_{\text{obs}}^t$  is the sample weight at time  $t$ , and  $r$  is the ratio of molecular weights of A and B. We now make use of the first order rate law

$$\frac{d\alpha}{dT} = \frac{A}{\beta} (1 - \alpha) e^{-E/RT} \quad (5)$$

Taking logarithms of both sides of eqn. (5) and substituting  $d\alpha/dT$  obtained from eqn. (4) into the resulting equation yields

$$\ln \frac{d\alpha/dT}{1 - \alpha} = \ln(A/\beta) - \frac{E}{RT} \quad (6)$$

which is equivalent to eqn. (2). Using the more general rate equation

$$\frac{d\alpha}{dT} = \frac{A}{\beta} (1 - \alpha)^n e^{-E/RT} \quad (7)$$

gives

$$\ln \left[ \frac{d\alpha/dT}{(1 - \alpha)^n} \right] = \ln \frac{A}{\beta} - \frac{E}{RT} \quad (8)$$

It can be seen that a plot of the left-hand side of eqn. (8) vs.  $1/T$  should be linear with a slope of  $-E/R$  and an intercept of  $\ln(A/\beta)$  for the correct value of  $n$ . This constitutes the first method of applying this extension of the method of Abou-Shaabab and Simonelli.

In order to obtain a numerical method that can be applied iteratively, a second method similar to that of Reich and Stivala was developed [2]. Considering two data sets,  $(\alpha_i, T_i, (d\alpha/dT)_i)$  and  $((\alpha_{i+1}, T_{i+1}, (d\alpha/dT)_{i+1}))$ , we obtain

$$\ln \left[ \frac{(d\alpha/dT)_i}{(d\alpha/dT)_{i+1}} \left( \frac{1 - \alpha_i}{1 - \alpha_{i+1}} \right)^n \right] = \frac{E}{R} \left( \frac{1}{T_{i+1}} - \frac{1}{T_i} \right) \quad (9)$$

For successive data sets, a plot of the left-hand side of eqn. (9) vs.  $((1/T_{i+1}) - (1/T_i))$  should be linear with an intercept of zero and a slope of  $E/R$  for the correct value of  $n$ . The analysis is performed iteratively using an initial value of  $n = 0$  and  $n$  is incremented until the intercept closest to zero is found [2,3]. The method was implemented using a Texas Instruments TI-58 or TI-59 programmable calculator.

In order to test the method, eqn. (7) was solved numerically using a fourth-order Runge-Kutta method [4]. The  $(\alpha, T, d\alpha/dT)$  data thus obtained were analyzed by both of the methods described above. In order to test the methods with actual TG data, the decomposition of  $\text{CaCO}_3$  was studied using a Perkin-Elmer thermogravimetric system (Model TGS-2). Procedures used were similar to those previously described [5].

## RESULTS AND DISCUSSION

The data obtained from the numerical solution of eqn. (7) using values of  $n = 1/2, 1/2, 2/3$  and 1 are shown in Table 1. In carrying out the numerical solutions, the values of  $E = 100 \text{ kJ mol}^{-1}$  and  $A/\beta = 3 \times 10^{10}$  were used. These data were then used to test the computational methods. The results obtained using linear regression with a specific value for  $n$  (the first method) showed that analysis of these data gave linear plots for the correct  $n$  value and yielded the correct activation energy. Thus, one could test TG data using this technique employing various values of  $n$  to see which gives the most nearly linear plot.

Since it is difficult to iterate on  $n$  using the correlation coefficient as a criterion, the iterative method that searches for the  $n$  value resulting in an intercept closest to zero was developed. Table 2 shows the kinetic parameters computed using the iterative method with calculated ( $\alpha, T, (d\alpha/dT)$ ) data. The iterative method easily identifies the correct value of  $n$  and yields an  $E$  value that is virtually identical to that used in the numerical solution of the rate equation.

The results of the analysis of data for the decomposition of  $\text{CaCO}_3$  are also shown in Table 2. Both the iterative method and the method using a fixed  $n$  value with linear regression gave virtually identical results. The results shown in Table 2 are those obtained using the iterative method. Kinetic parameters obtained are in reasonable agreement with those previously reported [6–8]. It is readily apparent, however, that the problem of sample-to-sample variation persists [9]. The present extension of the method of Abou-Shaaban and Simonelli allows that approach to be used for reac-

TABLE 1

Values of  $\alpha$  and  $d\alpha/dT$  computed from eqn. (7) using a fourth-order Runge-Kutta method <sup>a</sup>

$T$ (K)	$\alpha$	$d\alpha/dT$	$\alpha$	$d\alpha/dT$
	$n = 1/3$		$n = 1/2$	
410	0.07056	0.0053277	0.07015	0.0052643
420	0.14676	0.010411	0.14493	0.010150
430	0.29065	0.019054	0.28338	0.018086
440	0.53996	0.031144	0.51426	0.028117
450	0.89313	0.035145	0.82452	0.031024
	$n = 2/3$		$n = 1$	
410	0.06974	0.0052024	—	—
420	0.14317	0.0099022	0.13981	0.0094420
430	0.27660	0.017216	0.26430	0.015718
440	0.49189	0.025689	0.45453	0.022006
450	0.77010	0.027793	0.68720	0.023166
460	—	—	0.88562	0.015145

<sup>a</sup> Computed using  $E = 100 \text{ kJ mol}^{-1}$ ,  $R = 8.31441 \text{ J mol}^{-1} \text{ K}^{-1}$ , and  $A/\beta = 3 \times 10^{10}$ .

TABLE 2

Results obtained using the iterative method

$n$ (actual) <sup>a</sup>	$n$ (calcd)	$E$ (kJ mol <sup>-1</sup> )
<i>Calculated (<math>\alpha</math>, <math>T</math>, (<math>d\alpha/dT</math>)) data</i>		
1/3	0.33	99.79
1/2	0.50	100.00
2/3	0.67	100.14
1	1.00	100.00
Run	$n$	$E$ (kJ mol <sup>-1</sup> )
<i>Data from decomposition of CaCO<sub>3</sub></i>		
1	0.50	177.0
2	0.47	194.8
3	0.27	180.8
4	0.23	170.3
5	0.34	172.3
Average	0.36	179.0

<sup>a</sup> Value used in the numerical solutions of eqn. (7).

tions which do not follow a first-order rate law and the computational methods greatly increase the speed and accuracy of the analysis of the data.

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