

THERMAL ANALYSIS AND KINETICS OF THE OXIDATION OF VANADIUM AND  
TITANIUM SULFIDES

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ABSTRACT

The kinetics of the oxidation of "V<sub>5</sub>S<sub>8</sub>" and V<sub>3</sub>S<sub>4</sub> to V<sub>2</sub>O<sub>3</sub>, and "TiS<sub>2</sub>" and "Ti<sub>2</sub>S<sub>3</sub>" to TiO<sub>2</sub> was studied by using both isothermal and nonisothermal thermogravimetry. The kinetic equations are

$$1 - (1 - \alpha)^{1/1.5} = kt \text{ for the vanadium sulfides and}$$
$$\ln(1 - \alpha)^{1/1.5} = -kt \text{ for the titanium sulfides}$$

INTRODUCTION

Oxidation processes of some metal-sulfide systems (Fe-S, Cu-S, Zn-S, Ni-S, etc.) have been studied vigorously, but others, such as V-S and Ti-S systems, yet warrant special attention. Although several authors [1,2,3] have studied the oxidation of VS, V<sub>4</sub>S<sub>5</sub> and V<sub>2</sub>S<sub>3</sub>, there are no reports on the oxidation of V<sub>5</sub>S<sub>8</sub> and V<sub>3</sub>S<sub>4</sub>, the two other most important phases of the V-S system. In the present report, we have made an effort to study the thermal oxidation process and the kinetics of oxidation of the V<sub>5</sub>S<sub>8</sub>, V<sub>3</sub>S<sub>4</sub>, TiS<sub>2</sub> and Ti<sub>2</sub>S<sub>3</sub> phases.

EXPERIMENTAL

Measurement method: TG-DTA measurements were done with a rapid heating Rigaku-Thermoflex TG-DTA unit. Five, ten or twenty mg of the sample was weighed accurately in a platinum crucible of 2.5 x 5 mm diameter, distributed evenly without pressing and was tapped 2 or 3 times on a metal surface. High purity "dead burnt"  $\alpha$ -alumina was used as the standard reference material. The oxygen partial pressure (P<sub>O<sub>2</sub></sub>) in the reaction chamber was controlled by mixing air and N<sub>2</sub> [4].

Sample preparation: Nonstoichiometric "V<sub>5</sub>S<sub>8</sub>" (VS<sub>1.567</sub>) was obtained by heating [400°C(6h) → 950°C(20h) → 400°C(24h)] reagent grade NH<sub>4</sub>VO<sub>3</sub> powder (99% pure) in a mullite boat in a flow of H<sub>2</sub>S gas (1 atm). Stoichiometric V<sub>3</sub>S<sub>4</sub> (VS<sub>1.342</sub>) was prepared by heating the "V<sub>5</sub>S<sub>8</sub>" sample in a flow of H<sub>2</sub>S/H<sub>2</sub> (P<sub>S<sub>2</sub></sub>=10<sup>-4</sup>atm) at 900°C for 3h.

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Nonstoichiometric "TiS<sub>2</sub>" (TiS<sub>1.972</sub>) was prepared by heating [400°C (1 day) → 800°C (6 days)] a stoichiometric weighed mixture (for TiS<sub>2</sub>) of Ti (99.9% pure) and S (guaranteed reagent) in an evacuated quartz tube. The mass was then heated again for 4 days in a furnace which has a temperature gradient (360°-550°C). In order to obtain non-stoichiometric "Ti<sub>2</sub>S<sub>3</sub>" (TiS<sub>1.740</sub>) weighed mixture of Ti and S was heated [400°C (1 day) → 950°C (1 day)] in an evacuated quartz tube.

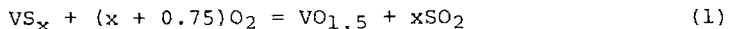
The phases were identified by X-ray powder diffractometry, and the compositions were determined by oxidizing the V-sulfides to V<sub>2</sub>O<sub>5</sub> and Ti-sulfides to TiO<sub>2</sub> in flowing air.

### RESULTS AND DISCUSSION

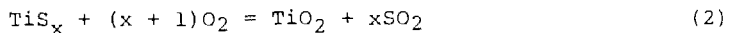
Thermal analysis: Fig. 1a shows the TG-DTA curves of "V<sub>5</sub>S<sub>8</sub>" (250-325 mesh) in air flow at 0.5° and 10°C/min. At lower heating rate, the TG curve (A) shows 5 steps of weight change. V<sub>3</sub>S<sub>4</sub> also shows the same oxidation steps. The X-ray analysis of the products at the end of each step, except step I, together with the weight change calculated for these steps suggests that the oxidation steps are VS<sub>x</sub> <sup>I</sup> → O<sub>2</sub> (absorption) <sup>II</sup> → VO<sub>2</sub> + VS<sub>x</sub> (unreacted) <sup>III</sup> → V<sub>2</sub>O<sub>3</sub> <sup>IV</sup> → VO<sub>2</sub> <sup>V</sup> → V<sub>2</sub>O<sub>5</sub>. Weight chemical analysis revealed that traces of VOSO<sub>4</sub> form at step II. At higher heating rate (B), step III is absent; however, the rise of sample temperature at step III (starting temperature is around 355°C), is much higher than that at lower heating rates.

Fig. 2b shows the TG-DTA curves of "TiS<sub>2</sub>" (250-275 mesh) in air flow at 10°C/min. Both TG and DTA curves show a single step. X-ray analysis of the end product showed the presence of only TiO<sub>2</sub> (Anatase) phase. The weight change calculated for this step shows that the sample (also "Ti<sub>2</sub>S<sub>3</sub>") oxidizes stoichiometrically to TiO<sub>2</sub>.

It can be concluded from the above results that the kinetic study of the oxidation of V-sulfides to V<sub>2</sub>O<sub>3</sub> and Ti-sulfides to TiO<sub>2</sub> according to eqns (1) and (2) is possible if the rise of sample temperature during oxidation can be prevented, and it can actually be done by reducing the P<sub>O<sub>2</sub></sub>.



where, x=1.567 for "V<sub>5</sub>S<sub>8</sub>" and 1.342 for V<sub>3</sub>S<sub>4</sub>



where, x=1.972 for "TiS<sub>2</sub>" and 1.740 for "Ti<sub>2</sub>S<sub>3</sub>"

Kinetic study: Fig. 2a shows the fraction reacted (α) vs time (t) curves for "V<sub>5</sub>S<sub>8</sub>" at a P<sub>O<sub>2</sub></sub> of 0.01 atm when heated isothermally. It

has been found that equation (3), which corresponds to "index of reaction" [5] (superficially analogous to rate of reaction) of  $m=1/3$  ( $z$  and  $\beta=1$ ) indicating the unidirectional kinetic of a sphere,

$$1-(1-\alpha)^{1/1.5} = kt \quad (3)$$

gives the best straight line fit for both " $V_5S_8$ " and  $V_3S_4$  ( $\alpha = 0$  to 70-90%) and hence controls the oxidation reaction. Fig.3 shows the Arrhenius plots for " $V_5S_8$ " and  $V_3S_4$ . Fig.2b shows the  $\alpha$  vs.  $t$  curves for " $TiS_2$ ". It has been found that equation (4), which corresponds

$$[-\ln(1-\alpha)]^{1/1.5} = kt \quad (4)$$

to random nucleation and subsequent growth mechanism, gives the best straight line fit for the oxidation. A knee appears in the Arrhenius plot (fig.4) for the Ti-sulfides. There are two well accepted reasons for this; the introduction of a new phase during the progress of the reaction [3], and the alteration of reaction-site energy distribution going from one Arrhenius region to another [6]. The latter one seems to be applicable here, since repeated X-ray analysis of the oxidation product failed to detect the presence of any other phase but  $TiO_2$  (Anatase).

Apparent activation energy  $E$  and preexponential factor  $A$  were also determined nonisothermally for eqns (1) and (2) in the same  $PO_2$  by employing the graphical method of Coats and Redfern [7] (fig.5). Values of  $E$  and  $A$  from both the isothermal and nonisothermal methods are given in table 1. The use of equations (3) and (4) in fig.5a and 5b respectively, and comparable values of  $E$  and  $A$  left no doubt regarding the authenticity of the observed mechanisms.

The present study reveals that, unlike the decomposition of carbonates which proceeds by a similar mechanism [8], the mechanism of the oxidation of sulfides differs for different sulfides.

TABLE 1

The values of  $E$  ( $\text{kJ mol}^{-1}$ ) and  $A$  ( $\text{sec}^{-1}$ ) for V-sulfides and Ti-sulfides

Sample	Isothermal		Nonisothermal		
	E	A	E	A	Heating Rate
" $V_5S_8$ "	30.9	0.146	32.3	0.095	20°C/m
$V_3S_4$	33.2	0.212	42.2	0.437	20°C/m
" $TiS_2$ "	75.7 (21.5)	575	87.0	3298	2°C/m
" $Ti_2S_3$ "	83.0 (14.8)	3263	86.7	4206	2°C/m

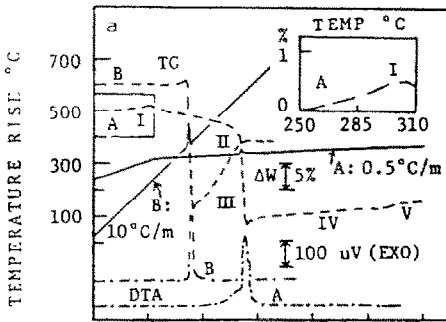


FIG.1 TG-DTA curves in air (2cc/sec); a: "V<sub>5</sub>S<sub>8</sub>" (insert; step I of curve A), b: "TiS<sub>2</sub>"

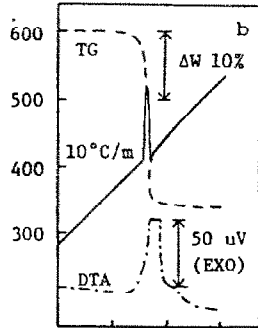


FIG.4 Arrhenius plot for TiS<sub>x</sub>

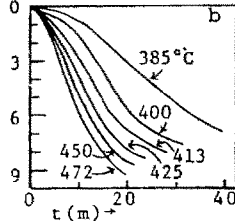
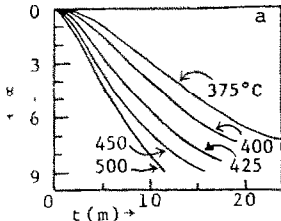


FIG.2  $\alpha$  vs.  $t$  curves; a: "V<sub>5</sub>S<sub>8</sub>", b: "TiS<sub>2</sub>"

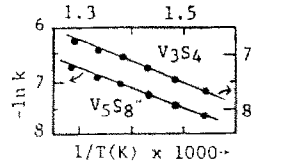


FIG.3 Arrhenius plot for VS<sub>x</sub>

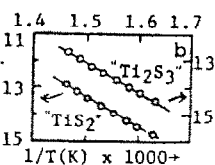
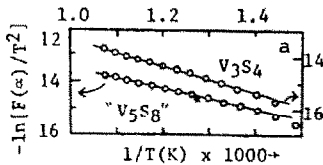


FIG.5 Coats and Redfern's linearization plots; a: VS<sub>x</sub> [ $F(\alpha) = 1 - (1 - \alpha)^{1/1.5}$ ], b: TiS<sub>x</sub> [ $F(\alpha) = (-\ln(1 - \alpha))^{1/1.5}$ ]

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