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AN AUTOMATED CALORIMETER FOR SOLID SUBSTANCES\*

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#### ABSTRACT

An automated low temperature adiabatic calorimeter for solid samples is described. It operates in the 10-370 K temperature range with an stablished accuracy of 0.1% in  $C_p$  measurements. Data are also presented of the heat capacity in  $(C_n H_{2n+1} N H_3)_2 ZnC1_4$ , with n=2,4. Thermodynamic functions of new phase transitions and thermal relaxation results are also shown.

### INTRODUCTION

In the last few years microcomputer automated calorimeters using the adiabatic technique have been described /1,2,3/ and the calibration results show similar accuracy features than those found in the manually operated ones. Here we describe an automated system for data acquisition and process control of an adiabatic calorimeter whose calibration results have been previously presented /4/. The computer programs allows a simple operation mode for pulse measurements as well as a continuous heating/cooling method specially indicated when  $C_p$  anomalies near solid-solid phase transitions are found. Moreover, thermal relaxation analysis can be easily performed.

# AUTOMATIC SYSTEM

Fig.1 is a scheme of the data acquisition and the control system. The microcomputer (HP9836) is primarily interfaced with the multiplexer-actuator (HP8497A) for the main operation functions and data acquisition. Only the temperature data is obtained directly from an independent DVM, as the multiplexer thermal noise has been found inadequate for the required accuracy. 1 mK sensibility is then achieved by an averaging program which smoothes the DVM original data. A digital-analog converter provides the heater power supply in the range 0-40 mA., while time measurements are obtained from the computer internal clock.

The four element adiabatic jacket is also controlled by PID's \* Work sponsored by CAICYT (Spanish Government) Proceedings of ICTA 85, Bratislava amplifiers. However an additional DC signal which favours the adiabatic control can also be programmed both for heating and equilibrium intervals. Periodic controls of the vacuum detectors, rotatory and difussion pump refrigeration, etc., assures a safe operation mode.

Finally, the microcomputer speed also permits a simultaneous data process for a rapid determination of the  $C_p$  results. The final most important data are then recorded on a magnetic disc.



Fig.1 Automatic System Block Diagram.

## OPERATION MODE

Once the desired temperature is reached and the adiabatic control is assured, a continuous check of the sample temperature takes place. Simultaneous time measurements determine the calorimeter temperature drift. Values of  $10^{-6} - 10^{-7}$  gC/sec. are commonly found when thermal equilibrium is attained. Then a heating period starts and power mesurements are periodically performed as well as the above refered operation controls. The initial and final temperature are fixed trough the extrapolated temperature drift before and after the heating pulse.

An alternative heating/cooling method can also be used for Cp measurements. This method is notoriously improved when automatic data acquisition is available.

### RESULTS

Fig.2 shows the measurements results for the phase transition found in  $(C_4H_9NH_3)_2ZnCl_4$ . The heating rates used as well as the thermodynamic functions values are included in the figure. The same calorimetric technique have showed a new phase transition at T=234 K in  $(C_2H_5NH_3)ZnCl_4$ . Experimental investigations are now in progress in order to clarify the physical mechanisms present in these new phase transitions found in both layer compounds.



Fig.2 (C4H9NH3)2ZnCl4 specific heat near the phase transition.

In fig.3 we can see the characteristic shape of the relaxation T -t curve after a heating pulse. Although this result must be strongly dependent on the sample characteristics and on the heat exchanger helium gas content, it provides a relative measurement of the sample thermal relaxation and conductivity. As we can expect a different thermal behaviour among the calorimeter vessel and the sample, we can crudely aproximate the observed relaxation to a simple sum of exponential functions each one being related with each system. The found relaxation times are shown in the figure, the first one in good agreement with the observed equilibrium time of the empty vessel.



Fig.3 Sample + vessel thermal relaxation.

### REFERENCES

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