

# Role of the Initial Temperature in the Equations of State of an Elastic Dielectric\*

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Partial differential equations are derived which describe the initial-temperature dependence of the equations of state of an elastic dielectric. These equations are applied to the case in which the equations of state can be represented by polynomials of degree 2 in the independent field variables—the displacement gradient and the electric displacement field. The special case of material symmetry  $m3m$  is introduced and applied to NaCl. It is found that for this crystal the initial temperature and the temperature of the system play equally significant roles in the equations of state.

## I. INTRODUCTION

IN this paper, we discuss the role of the temperature of the reference or initial state—the so-called initial temperature—in the equations of state of materials.<sup>1</sup> We shall be concerned only with the static elastic, dielectric, and thermal properties and we shall restrict the discussion to the case in which these properties are described by the following fields—the displacement gradient, the electric displacement field, the electric field, the absolute temperature, the entropy density, and an energy density.

The first part of the paper, Secs. II–IV, deals with the partial differential equations which describe the initial-temperature dependence of the equations of state. These equations are applied, in Secs. V–VII, to the case in which the equations of state can be represented by polynomials of order 2 in the independent field variables, namely the components of the displacement gradient and the electric displacement field. In Sec. VIII, we discuss the special case of a polynomial representation with material symmetry  $m3m$ . Section IX contains a discussion of the implications of the initial-temperature dependence of the coefficients describing a polynomial representation. In the final section, Sec. X, we apply the results of Sec. VIII to the special case of NaCl and show that the initial temperature and the temperature of the system play equally significant roles in the equation of state.

## II. DEFORMATION

The deformation and displacement of an elastic dielectric are completely described by two fields: (a) the set of position coordinates  $X_i$  ( $i=1, 2, 3$ ) specifying the positions of the volume elements making up the body in some initial or reference state and (b) the analogous set of position coordinates  $x_i$  ( $i=1, 2, 3$ ) describing their positions in the final configuration of interest. We shall suppose that  $x_i$ ,  $X_i$  are measured in the same rectangular coordinate system. Set

$$x_i = X_i + u_i, \quad (1)$$

where  $u_i$  are the components of the displacement vector.

If we regard the  $u_i$  as functions of the  $X_i$ , then

$$\left(\frac{\partial x_i}{\partial X_j}\right) = \delta_{ij} + \left(\frac{\partial u_i}{\partial X_j}\right), \quad (2)$$

where  $\delta_{ij}$  is the Kronecker delta.  $(\partial x_i / \partial X_j)$  and  $(\partial u_i / \partial X_j)$  are, respectively, the deformation and displacement gradients. We shall use the latter quantity to describe the deformation. Let us introduce a second initial state described by the set of coordinates  $X'_i$  and define the corresponding displacement vector as above;

$$x_i = X'_i + u'_i. \quad (3)$$

Since Eqs. (1) and (3) refer to the same volume element,

$$X_i + u_i \equiv X'_i + u'_i \quad (4)$$

and, hence,

$$\left(\frac{\partial u_i}{\partial X_j}\right) = \left[ \delta_{ik} + \left(\frac{\partial u'_i}{\partial X'_k}\right) \right] \left(\frac{\partial X'_k}{\partial X_j}\right) - \delta_{ij}, \quad (5)$$

where the Einstein summation convention is used here and in all later expressions. We set  $(\partial u_i / \partial X_j) = u_{ij}$ ,  $(\partial u'_i / \partial X'_j) = u'_{ij}$ , and replace (5) with

$$u_{ij} = (\delta_{ik} + u'_{ik}) \left(\frac{\partial X'_k}{\partial X_j}\right) - \delta_{ij}. \quad (6)$$

Consider now a set of zero-stress states of the dielectric, obtained by heating the sample and at the same time keeping it free of applied surface tractions and electric displacement fields. Provided rigid translations and/or rotations of the sample are excluded, this set of states is uniquely determined by (a) the choice of zero-stress state prior to the heating and (b) the thermoelastic properties peculiar to the sample. Within the set, each state is uniquely specified by its temperature  $\theta$ . In what follows, we shall only use initial states which are zero-stress states<sup>1a</sup> and we shall only consider changes of initial states involving two zero-stress states belonging to the same set in the sense described above. (Thus, we specifically exclude trivial changes of initial state achieved by rigid translations and/or rotations of the

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<sup>1</sup> R. A. Toupin, *J. Rat. Mech. Anal.* **5**, 849 (1956).

<sup>1a</sup> For a general discussion of the initial-configuration dependence of the equation of state, see W. Noll, *Arch. Rat. Mech. Anal.* **27**, 1 (1967).

sample). Let us choose a zero-stress state as the initial state and let its temperature be denoted by  $\theta_i$ . We shall assume that the properties of the dielectric are such that the displacement gradients describing the deformations of the remaining zero-stress states of this set are uniform, i.e.,  $(\partial^2 u_i / \partial X_j \partial X_k) = 0$  for all  $i, j, k$ , and  $X_j$ . Thus, if we denote the displacement gradient of a zero-stress state by  $\gamma_{ij}$ , we can then write the position coordinates in these states in the form, Eq. (1),

$$x_i = (\delta_{ij} + \gamma_{ij})X_j.$$

$\gamma_{ij}$  is the thermal expansion tensor. It is a function of the zero-stress state of interest and the initial state, i.e.,  $\gamma_{ij} = \gamma_{ij}(\theta, \theta_i)$ . In particular, since  $x_i = X_i$  when  $\theta = \theta_i$ ,

$$\gamma_{ij}(\theta_i, \theta_i) = 0, \quad \text{for all } i, j. \quad (7)$$

Similarly, for some other choice of initial state with temperature  $\theta'_i$ , we have

$$x_i = [\delta_{ij} + \gamma'_{ij}(\theta, \theta'_i)]X'_j, \quad (8a)$$

with

$$\gamma'_{ij}(\theta'_i, \theta'_i) = 0.$$

Equation (6) holds for all states; when applied to zero-stress states, we find

$$\gamma_{ij}(\theta, \theta_i) = [\delta_{ik} + \gamma'_{ik}(\theta, \theta'_i)] \left( \frac{\partial X'_k}{\partial X_j} \right) - \delta_{ij}.$$

In particular, by (7),

$$\gamma_{ij}(\theta'_i, \theta_i) + \delta_{ij} = \left( \frac{\partial X'_i}{\partial X_j} \right). \quad (8b)$$

Eliminating  $(\partial X'_k / \partial X_j)$  from (6) by means of (8a), we get

$$u_{ij} = u'_{ik} [\gamma_{kj}(\theta'_i, \theta_i) + \delta_{kj}] + \gamma_{ij}(\theta'_i, \theta_i). \quad (9)$$

Equation (9) describes the transformation law for a change in initial state. The inverse transformation is

$$u'_{ij} = [u_{ik} - \gamma_{ik}(\theta'_i, \theta_i)] \Delta_{kj}(\theta'_i, \theta_i), \quad (10)$$

where  $\Delta_{ij}$  is the inverse tensor to  $\delta_{ij} + \gamma_{ij}$ , i.e.,

$$[\delta_{ik} + \gamma_{ik}(\theta'_i, \theta_i)] \Delta_{kj}(\theta'_i, \theta_i) = \delta_{ij}. \quad (11)$$

### III. EQUATION OF STATE

It is a characteristic of theories<sup>1-4</sup> of the elastic dielectric that the stress vector  $t^0$  describing the surface tractions satisfies a boundary condition of the form

$$t_i^0 = \tau_{ij} n_j, \quad (12)$$

where  $\tau_{ij}$  is some tensor function of the field components chosen to describe the response of the dielectric and the  $n_i$  are the direction cosines of the outward normal at the point of interest at the surface.

We shall assume that the independent field variables

are the displacement gradients  $u_{ij}$ , the electric displacement field components  $D_i$ , and the temperature  $\theta$ ; we then write

$$\tau_{ij} = \tau_{ij}(u_{ij}, D_i, \theta, \theta_i), \quad (13)$$

$$E_i = E_i(u_{ij}, D_i, \theta, \theta_i), \quad (14)$$

$$\sigma' = \sigma'(u_{ij}, D_i, \theta, \theta_i), \quad (15)$$

where  $E_i$  and  $\sigma'$  are the electric field components and the entropy density (per unit mass), respectively. We shall regard Eqs. (13)–(15) as equations of state. It is clear from the following remarks why the initial temperature  $\theta_i$  must appear as an explicit argument in the functions  $\tau_{ij}$ ,  $E_i$ , and  $\sigma'$ ; the *values* of the displacement gradients are functions of  $\theta_i$  whereas the *values* of  $\tau_{ij}$ ,  $E_i$ , and  $\sigma'$  in any given state cannot depend on  $\theta_i$ ; therefore, the functions in (13)–(15) must contain an explicit  $\theta_i$  dependence sufficient to cancel the implicit  $\theta_i$  dependence introduced by the  $u_{ij}$ . This argument provides the basis of the analysis given below.

The equation of state (13) has some unusual aspects: (i) The field  $\tau_{ij}$  is defined only on the surface of the dielectric; (ii) the function  $\tau_{ij}$  is in general a function of the  $n_i$ , the direction cosines of the normal to the surface at a point in question; (iii) there are nine  $\tau_{ij}$ 's and nine  $u_{ij}$ 's, but in the region of a state with  $D_i = 0$  ( $i = 1, 2, 3$ ) we cannot, in general, invert Eq. (13) to obtain a unique equation of state for the  $u_{ij}$ .

The last two points are best illustrated by considering a particular form for the  $\tau_{ij}$ . From Refs. 4 and 5,

$$\tau_{ij} = \rho \left( \frac{\partial F}{\partial u_{ik}} \right) (\delta_{jk} + u_{jk}) - \left[ \frac{D_k^A D_k^A}{2\epsilon_0} + \frac{1}{2} (E_k^V + E_k^A) (D_k^V - D_k^A) \right] \delta_{ij}, \quad (16)$$

where  $\rho$  is the mass density,  $F$  the free energy density, and  $\epsilon_0$  the permittivity of free space. The superscripts  $V$  and  $A$  refer to the field values in the dielectric and vacuum, respectively. The quantity in square brackets, and, hence,  $\tau_{ij}$ , is a function of the  $n_i$  because  $D_i^A$  and  $E_i^A$  are related to  $D_i^V$  and  $E_i^V$  by the boundary conditions  $n_i (D_i^V - D_i^A) = 0$  and  $e_{ijk} (E_j^V - E_j^A) n_k = 0$ , where  $e_{ijk}$  is the Levi-Civita density.

To prove (iii), consider the case in which  $D_i^V = 0$  ( $i = 1, 2, 3$ ); then, since  $F$  is a function of the  $u_{ij}$  only through the six Lagrangian strain components<sup>1</sup>  $\eta_{ij} = \frac{1}{2} (u_{ij} + u_{ji} + u_{ki} u_{kj})$ ,

$$\left( \frac{\partial F}{\partial u_{ik}} \right) (\delta_{jk} + u_{jk}) = \frac{1}{2} \left( \frac{\partial F}{\partial \eta_{kl}} \right) [(\delta_{ik} + u_{ik})(\delta_{jl} + u_{jl}) + (\delta_{il} + u_{il})(\delta_{jk} + u_{jk})]. \quad (17)$$

Hence,

$$\tau_{ij} |_{D_i^V=0} = \tau_{ji} |_{D_i^V=0}, \quad (18)$$

<sup>5</sup> J. Grindlay and A. R. Redlack (unpublished).

<sup>2</sup> R. A. Toupin, Int. J. Eng. Sci. 1, 101 (1963); see also Ref. 1.

<sup>3</sup> A. C. Eringen, Int. J. Eng. Sci. 1, 127 (1963).

<sup>4</sup> J. Grindlay, Phys. Rev. 149, 637 (1966).

i.e., the functions  $\tau_{ij}$  are symmetric. Set

$$\tau_{ij} - \tau_{ij}(u_{ij}, D_i^V, \theta, \theta_i) = f_{ij}.$$

From (18), the Jacobian

$$\frac{\partial(f_{11}, f_{22}, f_{33}, f_{12}, f_{13}, f_{21}, f_{23}, f_{31}, f_{32})}{\partial(u_{11}, u_{22}, u_{33}, u_{12}, u_{13}, u_{21}, u_{23}, u_{31}, u_{32})}$$

vanishes when  $D_i^V = 0$  ( $i = 1, 2, 3$ ); therefore, in the region of any state with  $D_i^V = 0$  ( $i = 1, 2, 3$ ), there is no unique inversion<sup>6</sup> of Eq. (13) for the  $u_{ij}$ 's in terms of the  $\tau_{ij}$ 's. This result is particularly relevant in the theory of the elastic dielectric because it is customary to represent the functions  $\tau_{ij}$  by a truncated power series in  $u_{ij}$  and  $D_i^V$  about the values  $u_{ij} = 0$ ,  $D_i^V = 0$ , and, hence, from the comments made above, we see that we cannot invert this series to obtain the  $u_{ij}$ 's in terms of the  $\tau_{ij}$ 's.<sup>7</sup>

It has been remarked above that the value of  $\tau_{ij}$  cannot be a function of the choice of initial state, i.e., of  $\theta_i$ . Thus, if we choose to describe the deformation of some state relative to two different initial states  $\theta_i$ , and  $\theta_i'$ , we must have

$$\tau_{ij}(u_{kl}, D_k, \theta, \theta_i) \equiv \tau_{ij}'(u_{kl}', D_k, \theta, \theta_i'), \quad (19)$$

where  $u_{kl}$  and  $u_{kl}'$  are related by Eq. (9) and  $\tau_{ij}'$  is the function appropriate to the equation of state for which the displacement gradients are measured relative to the primed initial state. Substituting for  $u_{kl}$  from (9), we write (19) in the form

$$\tau_{ij}\{\gamma_{kl}(\theta_i', \theta_i) + u_{km}'[\delta_{ml} + \gamma_{ml}(\theta_i', \theta_i)], D_k, \theta, \theta_i\} \equiv \tau_{ij}'(u_{kl}', D_k, \theta, \theta_i'). \quad (20)$$

Let us differentiate both sides of this identity with respect to  $\theta_i$ , holding  $\theta_i'$ ,  $\theta$ ,  $D_k$ , and  $u_{kl}'$  constant; hence,

$$\left(\frac{\partial \tau_{ij}}{\partial u_{kl}}\right)_{D, \theta, \theta_i} \left(\frac{\partial \gamma_{kl}}{\partial \theta_i}(\theta_i', \theta_i) + u_{km}' \frac{\partial \gamma_{ml}}{\partial \theta_i}(\theta_i', \theta_i)\right) + \left(\frac{\partial \tau_{ij}}{\partial \theta_i}\right)_{u, D, \theta} = 0. \quad (21)$$

Substituting for  $u_{km}'$  from (10),

$$\left(\frac{\partial \tau_{ij}}{\partial u_{kl}}\right)_{D, \theta, \theta_i} \left[ \Delta_{nm}(\theta_i', \theta_i) \frac{\partial \gamma_{ml}}{\partial \theta_i}(\theta_i', \theta_i) \right] \times (\delta_{kn} + u_{kn}) + \left(\frac{\partial \tau_{ij}}{\partial \theta_i}\right)_{u, D, \theta} = 0. \quad (22)$$

Equation (22) holds for all values of  $D_k$ ,  $u_{kn}$ ,  $\theta$ ,  $\theta_i$ , and  $\theta_i'$ . The variable  $\theta_i'$  occurs only within the square bracket

<sup>6</sup> See, for example, G. A. Gibson, *Advanced Calculus* (MacMillan and Co. Ltd., London, 1948), Chap. 5.

<sup>7</sup> The occurrence of a symmetric  $\tau_{ij}$  does not reduce the number of independent boundary conditions because the  $\tau_{ij}$  appear as linear combinations in these conditions [see Eq. (12)].

and, hence, this combination of quantities is independent of  $\theta_i'$ .

We set

$$\Delta_{km}(\theta_i', \theta_i) \frac{\partial \gamma_{ml}}{\partial \theta_i}(\theta_i', \theta_i) = A_{kl}(\theta_i), \quad (23)$$

where  $A_{kl}$  is a tensor function with a single temperature argument. Using the properties of  $\Delta_{km}$ , Eq. (11), we solve for  $(\partial \gamma_{ml} / \partial \theta_i)$ :

$$\frac{\partial \gamma_{ij}}{\partial \theta_i}(\theta_i', \theta_i) = A_{ij}(\theta_i) + \gamma_{ik}(\theta_i', \theta_i) A_{kj}(\theta_i). \quad (24)$$

It is clear that the prime and the subscript in the first temperature argument in  $\gamma_{ij}$  is redundant in (24), as these equations hold for all  $\theta_i'$ , i.e., all temperatures. With the introduction of the tensor  $A_{ij}$ , Eq. (22) takes the form

$$\left(\frac{\partial \tau_{ij}}{\partial u_{kl}}\right)_{D, \theta, \theta_i} A_{nl}(\theta_i)(\delta_{kn} + u_{kn}) + \left(\frac{\partial \tau_{ij}}{\partial \theta_i}\right)_{D, \theta, u} = 0. \quad (25)$$

Similar considerations for  $E_i$  and  $\sigma'$  yield

$$\left(\frac{\partial E_i}{\partial u_{kl}}\right)_{D, \theta, \theta_i} A_{nl}(\theta_i)(\delta_{kn} + u_{kn}) + \left(\frac{\partial E_i}{\partial \theta_i}\right)_{D, \theta, u} = 0, \quad (26)$$

$$\left(\frac{\partial \sigma'}{\partial u_{kl}}\right)_{D, \theta, \theta_i} A_{nl}(\theta_i)(\delta_{kn} + u_{kn}) + \left(\frac{\partial \sigma'}{\partial \theta_i}\right)_{D, \theta, u} = 0. \quad (27)$$

Equations (25)–(27) are partial-differential equations describing the  $\theta_i$  dependence of the functions  $\tau_{ij}$ ,  $E$ , and  $\sigma'$ .

#### IV. THERMAL EXPANSION

In this section, we discuss Eq. (24) and its solution. Let  $f_{ij}(\theta_i)$  be a second-rank tensor which is a solution to the equation

$$\frac{df_{ij}}{d\theta_i} = -A_{ik}(\theta_i) f_{kj}(\theta_i). \quad (28)$$

Set

$$\gamma_{ij}(\theta, \theta_i) = \mu_{ik}(\theta, \theta_i) f_{kj}^{-1}(\theta_i), \quad (29)$$

where

$$f_{ij}(\theta_i) f_{jk}^{-1}(\theta_i) = \delta_{ik}. \quad (30)$$

Then, from (28) and (29),

$$\frac{\partial \gamma_{ij}}{\partial \theta_i}(\theta, \theta_i) = \left(\frac{\partial \mu_{ik}}{\partial \theta_i}(\theta, \theta_i)\right) f_{kj}^{-1}(\theta_i) + \mu_{ik}(\theta, \theta_i) f_{kl}^{-1}(\theta_i) A_{lj}(\theta_i). \quad (31)$$

Substituting for  $\gamma_{ij}$  and its derivative from (29) and

(31) in (24), we obtain

$$\frac{\partial \mu_{ij}}{\partial \theta_i}(\theta, \theta_i) = A_{il}(\theta_i) f_{lj}(\theta_i),$$

or

$$\gamma_{ij}(\theta, \theta_i) = \left( \int_0^{\theta_i} A_{il}(\theta_i) f_{lj}(\theta_i) d\theta_i \right) f_{kj}^{-1}(\theta_i), \quad (32)$$

since  $\gamma_{ij}(\theta_i, \theta_i) = 0$ . The integrand in (32) is  $-df_{ik}/d\theta_i$  and, hence,

$$\gamma_{ij}(\theta, \theta_i) = f_{ik}^{-1}(\theta_i) f_{kj}(\theta) - \delta_{ij}. \quad (33)$$

Thus, the demands placed by Eq. (24) on the thermal expansion  $\gamma_{ij}$  are satisfied if and only if  $\gamma_{ij}$  can be expressed in terms of a function of a single argument as shown in (33).

## V. POLYNOMIAL REPRESENTATION

To explore the demands of Eqs. (25), (26), and (27), we represent the functions  $\tau_{ij}$ ,  $E_i$ , and  $\sigma'$  by the following polynomials:

$$\tau_{ij}(u_{kl}, D_k, \theta, \theta_i) = \tau_{ij}^0 + c_{ijkl} u_{kl} - h_{ijk} D_k + C_{ijklmn} u_{kl} u_{mn} + 2b_{ijklm} u_{kl} D_m + q_{ijkl} D_k D_l, \quad (34)$$

$$E_i(u_{kl}, D_k, \theta, \theta_i) = E_i^0 - \tilde{h}_{kli} u_{kl} + \beta_{ij} D_j + \tilde{b}_{klmni} u_{kl} u_{mn} + 2\tilde{q}_{klji} u_{kl} D_j + \eta_{ijk} D_j D_k, \quad (35)$$

$$\sigma'(u_{kl}, D_k, \theta, \theta_i) = \sigma_0' - \hat{\tau}_{ij}^0 u_{ij} - \hat{E}_i^0 D_i - \frac{1}{2} \hat{c}_{ijkl} u_{ij} u_{kl} + \hat{h}_{ijk} u_{ij} D_k - \frac{1}{2} \hat{\beta}_{ij} D_i D_j. \quad (36)$$

$\tau_{ij}^0$  is the thermal stress,  $c_{ijkl}$  the elastic stiffness  $h_{ijk}$ ,  $\tilde{h}_{ijk}$  the piezoelectric coefficients,  $C_{ijklmn}$  the nonlinear elastic coefficient,  $q_{ijkl}$  and  $\tilde{q}_{ijkl}$  the electrostrictive coefficients,  $E_i^0$  the thermal electric field,  $\beta_{ij}$  the dielectric permeability, and  $\sigma_0'$  the entropy density in zero-displacement gradient and zero-electric displacement. The remaining coefficients have not, to our knowledge, been named. The  $\theta$  and  $\theta_i$  dependence of the functions  $\tau_{ij}$ ,  $E_i$ , and  $\sigma'$  is contained in these coefficients. As Eqs. (34)–(36) stand, the only relations between the coefficients are

$$C_{ijklmn} = C_{ijmnlk}, \quad (37)$$

$$q_{ijkl} = q_{ijlk}, \quad (38)$$

$$\tilde{b}_{klmni} = \tilde{b}_{mnkli}, \quad (39)$$

$$\hat{c}_{ijkl} = \hat{c}_{klij}, \quad (40)$$

$$\hat{\beta}_{ij} = \hat{\beta}_{ji}. \quad (41)$$

With the introduction of an energy density, further identities occur and these (see below) suggest the introduction of the factor 2 and the use of the tilde and circumflex notation in Eqs. (34)–(36).

Inserting these polynomial representations into the partial-differential equations (25)–(27) and treating  $u_{ij}$  and  $D_i$  as independent variables, we obtain the

following differential equations:

$$\left( \frac{\partial \tau_{ij}^0}{\partial \theta_i} \right)_\theta + c_{ijkl} A_{kl}(\theta_i) = 0, \quad (42)$$

$$\left( \frac{\partial c_{ijk}}{\partial \theta_i} \right)_\theta + c_{ijkn} A_{ln}(\theta_i) + 2C_{ijmnlk} A_{mn}(\theta_i) = 0, \quad (43)$$

$$\left( \frac{\partial h_{ijm}}{\partial \theta_i} \right)_\theta - 2b_{ijklm} A_{kl}(\theta_i) = 0, \quad (44)$$

$$\left( \frac{\partial E_i^0}{\partial \theta_i} \right)_\theta - \tilde{h}_{kli} A_{kl}(\theta_i) = 0, \quad (45)$$

$$\left( \frac{\partial \tilde{h}_{kni}}{\partial \theta_i} \right)_\theta + \tilde{h}_{kli} A_{nl}(\theta_i) - 2b_{mklmi} A_{ml}(\theta_i) = 0, \quad (46)$$

$$\left( \frac{\partial \beta_{ij}}{\partial \theta_i} \right)_\theta + 2\tilde{q}_{klji} A_{kl}(\theta_i) = 0, \quad (47)$$

$$\left( \frac{\partial \sigma_0'}{\partial \theta_i} \right)_\theta - \hat{\tau}_{kl}^0 A_{kl}(\theta_i) = 0, \quad (48)$$

$$\left( \frac{\partial \hat{\tau}_{ij}^0}{\partial \theta_i} \right)_\theta + \hat{\tau}_{il}^0 A_{jl}(\theta_i) + \hat{c}_{klij} A_{kl}(\theta_i) = 0, \quad (49)$$

$$\left( \frac{\partial \hat{E}_i^0}{\partial \theta_i} \right)_\theta - \tilde{h}_{kli} A_{kl}(\theta_i) = 0. \quad (50)$$

These results are exact, in the sense that the introduction of higher-order terms in the representations given in Eqs. (34)–(36) would not affect the form of Eqs. (42)–(47). The equations for the  $\theta_i$  derivatives of  $C_{ijklmn}$ ,  $q_{ijkl}$ ,  $\tilde{q}_{ijkl}$ ,  $b_{ijklm}$ ,  $\tilde{b}_{ijklm}$ ,  $\eta_{ijk}$ ,  $\hat{c}_{ijkl}$ ,  $\hat{h}_{ijk}$ , and  $\hat{\beta}_{ij}$  contain the coefficients of the set of next-higher-order terms. Equations (42)–(50) describe the demands imposed by (25), (26), and (27) on the representations in (34), (35), and (36).

We note that the thermal expansion  $\gamma_{ij}$  at a point on the surface of the material satisfies the equations  $\tau_{ij} n_i = 0$  with  $D_j = 0$  ( $j = 1, 2, 3$ ). For the polynomial representation (34), we then have

$$0 = (\tau_{ij}^0 + c_{ijkl} \gamma_{kl} + C_{ijklmn} \gamma_{kl} \gamma_{mn}) n_i, \quad j = 1, 2, 3. \quad (51)$$

For systems which possess homogeneous zero-stress states, this set of equations determine the  $\gamma_{ij}$ .

## VI. ENERGY DENSITY

The introduction of an energy density leads to relations between the coefficients describing the equations of state Eqs. (34)–(36). We shall restrict the discussion to the case of the relations satisfied by the coefficients  $\tau_{ij}^0$ ,  $c_{ijkl}$ ,  $h_{ijk}$ ,  $E_i^0$ ,  $\tilde{h}_{ijk}$ ,  $\beta_{ij}$ ,  $\hat{\tau}_{ij}^0$ ,  $\hat{E}_i^0$ ,  $\hat{h}_{ijk}$ ,  $\hat{c}_{ijk}$ , and  $\hat{\beta}_{ij}$ . Consider a free-energy density  $F(u_{ij}, D_i, \theta, \theta_i)$ . The equa-

tions of state take the form

$$\tau_{ij} = \rho \left( \frac{\partial F}{\partial u_{ijk}} \right)_{D, \theta} (\delta_{jk} + u_{jk}), \quad (52)$$

$$E_i = \rho \left( \frac{\partial F}{\partial D_i} \right)_{\theta, u} \quad (53)$$

$$\sigma' = - \left( \frac{\partial F}{\partial \theta} \right)_{u, D}. \quad (54)$$

In writing (52), we have arbitrarily neglected<sup>8</sup> the Maxwell stress (the square bracket in Eq. (16)); this is a valid procedure in some circumstances.<sup>9</sup> The free-energy density  $F(u_{ij}, D_i, \theta, \theta_i)$  is invariant in form and value with respect to arbitrary changes in axes; hence,  $F = F(\eta_{ij}, \Pi_i, a, \theta_i, \theta)$ , where  $\eta_{ij} = \frac{1}{2}(u_{ij} + u_{ji} + u_{li}u_{lj})$ ,  $\Pi_i = (\delta_{ij} + u_{ij})D_j$ , and  $a = D_i D_i$ .<sup>1</sup> In a polynomial representation of  $F$ , the argument  $a$  is redundant. We set

$$\rho_0 F(\eta_{ij}, \Pi_i, \theta, \theta_i) = \rho_0 F_0 + H_{kl}^0 \eta_{kl} + H_k^1 \Pi_k + \frac{1}{2} H_{klmn}^2 \eta_{kl} \eta_{mn} + H_{klm}^3 \eta_{kl} \Pi_m + \frac{1}{2} H_{kl}^4 \Pi_k \Pi_l, \quad (55)$$

where  $\rho_0$  is the mass density in the initial state and  $F_0 = F(0, 0, \theta, \theta_i)$ . The  $H_{klmn}$ 's have the following properties:

$$H_{kl}^0 = H_{lk}^0, \quad (56)$$

$$H_{klmn}^2 = H_{mnlk}^2 = H_{klmn}^2 = H_{lmkn}^2, \quad (57)$$

$$H_{klm}^3 = H_{lkm}^3, \quad (58)$$

$$H_{kl}^4 = H_{lk}^4. \quad (59)$$

Inserting this representation for  $F$  into (52)–(54) and comparing it with (34)–(36), we find that

$$\tau_{ij}^0 = H_{ij}^0, \quad (60)$$

$$c_{ijkl} = (H_{ijkl}^2 - H_{ij}^0 \delta_{kl} + H_{lj}^0 \delta_{ik} + H_{il}^0 \delta_{jk}), \quad (61)$$

$$-h_{ijk} = H_{ijk}^3 + H_j^1 \delta_{ik}, \quad (62)$$

$$E_i^0 = H_i^1, \quad (63)$$

$$-\tilde{h}_{ijk} = H_{ijk}^3 + H_j^1 \delta_{ik} - H_k^1 \delta_{ij}, \quad (64)$$

$$\beta_{ij} = H_{ij}^4, \quad (65)$$

$$\sigma_0' = -(\partial F_0 / \partial \theta)_{\theta_i}, \quad (66)$$

$$\hat{\tau}_{ij}^0 = (\partial H_{ij}^0 / \partial \theta)_{\theta_i} / \rho_0, \quad (67)$$

$$\hat{E}_i^0 = (\partial H_i^1 / \partial \theta)_{\theta_i} / \rho_0, \quad (68)$$

$$\hat{h}_{ijk} = -(\partial H_{ijk}^3 / \partial \theta)_{\theta_i} / \rho_0, \quad (69)$$

$$\hat{c}_{ijkl} = [(\partial H_{ijkl}^2 / \partial \theta)_{\theta_i} + (\partial H_{jl}^0 / \partial \theta)_{\theta_i} \delta_{ik}] / \rho_0, \quad (70)$$

$$\hat{\beta}_{ij} = (\partial H_{ij}^4 / \partial \theta)_{\theta_i} / \rho_0. \quad (71)$$

From (60), (65), (67), (69), (71), and the properties of the  $H_{ijkl}^{\alpha}$ 's, Eqs. (56)–(59), we deduce that

$$\tau_{ij}^0 = \tau_{ji}^0, \quad \beta_{ij} = \beta_{ji}, \quad (72)$$

$$\hat{\tau}_{ij}^0 = \hat{\tau}_{ji}^0, \quad \hat{h}_{ijk} = \hat{h}_{jik}, \quad (73)$$

$$\hat{\beta}_{ij} = \hat{\beta}_{ji}. \quad (74)$$

These conditions on the coefficients appearing in (34)–(36) are a direct result of the introduction of an energy density. It is clear from Eqs. (60)–(71) that the  $\theta_i$  dependence of  $\tau_{ij}$ ,  $h_{ijk}$ , etc. may be deduced from the  $\theta_i$  dependence of the  $H_{ijkl}^{\alpha}$ 's and conversely.

## VII. MATERIAL SYMMETRY $m3m$

In this section, we apply the results obtained above to the special case of material symmetry  $m3m$ . For this symmetry, the tensor invariants of odd rank vanish identically and those of even rank are invariant under the coordinate transformations  $x_1 \rightarrow x_2$ ,  $x_2 \rightarrow -x_1$ ,  $x_3 \rightarrow x_3$  and  $x_1 \rightarrow x_2$ ,  $x_2 \rightarrow x_3$ ,  $x_3 \rightarrow x_1$ <sup>10</sup>; hence,

$$(i) \quad \tau_{11}^0 = \tau_{22}^0 = \tau_{33}^0 \quad (75)$$

and the remaining elements vanish (similarly, for  $H_{ij}^0$ ,  $\beta_{ij}$ ,  $\tau_{ij}^0$  and  $\beta_{ij}$ ).

$$(ii) \quad \begin{aligned} \tilde{q}_{1111} &= \tilde{q}_{2222} = \tilde{q}_{3333} \\ \tilde{q}_{1122} &= \tilde{q}_{2211} = \tilde{q}_{2233} = \tilde{q}_{3322} = \tilde{q}_{3311} = \tilde{q}_{1133} \\ \tilde{q}_{1212} &= \tilde{q}_{2121} = \tilde{q}_{3131} = \tilde{q}_{1313} = \tilde{q}_{2323} = \tilde{q}_{3232} \\ \tilde{q}_{1212} &= \tilde{q}_{2112} = \tilde{q}_{3113} = \tilde{q}_{1331} = \tilde{q}_{2332} = \tilde{q}_{3223} \end{aligned} \quad (76)$$

and the remaining elements vanish (similarly for  $c_{ijkl}$ ).

$$(iii) \quad \begin{aligned} q_{1111} &= q_{2222} = q_{3333} \\ q_{1122} &= q_{2211} = q_{2233} = q_{3322} = q_{3311} = q_{1133} \\ q_{1212} &= q_{2121} = q_{3131} = q_{1313} = q_{2323} = q_{3232} \\ &= q_{1221} = q_{2112} = q_{3113} = q_{1331} = q_{2332} = q_{3223} \end{aligned} \quad (77)$$

and the remaining elements vanish (similarly, for  $H_{ijk}^2$  and  $\tilde{c}_{ijk}$ ).

We shall assume that the thermal expansion tensor  $\gamma_{ij}$  is an invariant of the symmetry group  $m3m$ <sup>11</sup>; hence, we set

$$\gamma_{ij} = \gamma \delta_{ij},$$

where

$$\gamma = [f(\theta) / f(\theta_i) - 1], \quad (78)$$

Eq. (33), is a root of

$$0 = \tau_{11}^0 + (c_{1111} + 2c_{1122})\gamma + (C_{111111} + 4C_{111122} + 2C_{112233} + 2C_{112222})\gamma^2, \quad (79)$$

[see Eq. (51)].

<sup>8</sup> The extension of the calculation to the case of nonvanishing Maxwell stresses is straightforward, in principle, but tedious to carry out explicitly.

<sup>9</sup> J. Grindlay, in *Proceedings of the International Meeting on Ferroelectricity*, edited by V. Dvorak (Czechoslovakian Institute of Physics, Prague, 1966), p. 433.

<sup>10</sup> R. R. Birss, in *Reports on Progress in Physics*, edited by A. C. Strickland (Institute of Physics and Physical Society, London, 1963), Vol. XXVI, p. 307.

<sup>11</sup> The  $\gamma_{ij}$  of a material in a given zero-stress state is the thermodynamically stable root of Eq. (51). Thus, it is possible for  $\gamma_{ij}$  to display a lower symmetry than the material symmetry of the coefficients  $\tau_{ij}^0$ ,  $c_{ijkl}$ , and  $C_{ijklmn}$ .

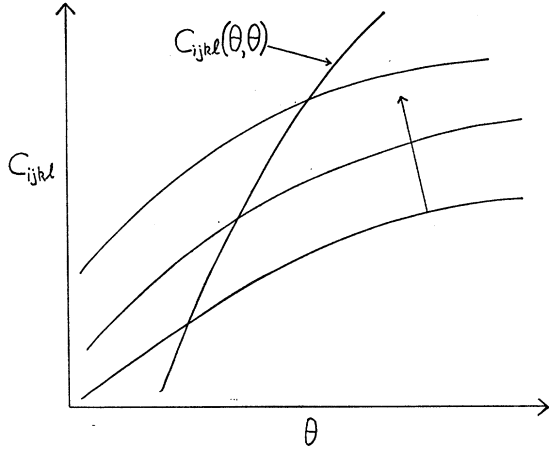


FIG. 1. Sketch of the family of curves  $C_{ijkl}(\theta, \theta_i)$  versus  $\theta$  with parameter  $\theta_i$ .

For  $m3m$ , Eqs. (42)–(50) take the form

$$\left(\frac{\partial \tau_{11}^0}{\partial \theta_i}\right)_\theta + A_{11}(\theta_i)(c_{1111} + 2c_{1122}) = 0, \quad (80)$$

$$\left(\frac{\partial c_{1111}}{\partial \theta_i}\right)_\theta + A_{11}(\theta_i)[c_{1111} + 2(C_{111111} + 2C_{111122})] = 0, \quad (81)$$

$$\left(\frac{\partial c_{1122}}{\partial \theta_i}\right)_\theta + A_{11}(\theta_i)[c_{1122} + 2(C_{111122} + C_{112222} + C_{112233})] = 0, \quad (82)$$

$$\left(\frac{\partial c_{1212}}{\partial \theta_i}\right)_\theta + A_{11}(\theta_i)[c_{1212} + 2(C_{121112} + C_{212111} + C_{211233})] = 0, \quad (83)$$

$$\left(\frac{\partial \beta_{11}}{\partial \theta_i}\right)_\theta + 2A_{11}(\theta_i)(\tilde{g}_{1111} + 2\tilde{g}_{2211}) = 0, \quad (84)$$

$$\left(\frac{\partial \sigma_0'}{\partial \theta_i}\right)_\theta - \tau_{11}^0 A_{11}(\theta_i) = 0, \quad (85)$$

$$\left(\frac{\partial \hat{\tau}_{11}^0}{\partial \theta_i}\right)_\theta + A_{11}(\theta_i)(\hat{\tau}_{11}^0 + \hat{c}_{1111} + 2\hat{c}_{1122}) = 0, \quad (86)$$

with

$$A_{11} = -(df/d\theta_i)/f, \quad (87)$$

and

$$(\partial \gamma / \partial \theta_i)_\theta = A_{11}(\theta_i)(1 + \gamma). \quad (88)$$

The symmetry properties of the  $C_{ijklmn}$  are discussed in Appendix A.

We now solve Eqs. (80)–(82) to obtain the explicit  $\theta$  and  $\theta_i$  dependence of  $\tau_{11}^0$ . Set

$$c = (c_{1111} + 2c_{1122}),$$

$$C = (C_{111111} + 4C_{111122} + 2C_{112233} + 2C_{112222}). \quad (89)$$

Then, Eqs. (79) and (80) and the sum of (81) plus twice

(82) read

$$0 = \tau_{11}^0 + c\gamma + C\gamma^2, \quad (90)$$

$$\left(\frac{\partial \tau_{11}^0}{\partial \theta_i}\right)_\theta + A_{11}c = 0, \quad (91)$$

$$\left(\frac{\partial c}{\partial \theta_i}\right)_\theta + A_{11}[c + 2C] = 0. \quad (92)$$

Equations (90), (91), and (92) have solutions of the form

$$\tau_{11}^0(\theta, \theta_i) = [f(\theta_i) - f(\theta)]k(\theta) \times \{h(\theta) + \frac{1}{2}[f(\theta_i) - f(\theta)]\}, \quad (93)$$

$$c(\theta, \theta_i) = k(\theta)f(\theta_i)\{h(\theta) + [f(\theta_i) - f(\theta)]\}, \quad (94)$$

$$C(\theta, \theta_i) = k(\theta)f^2(\theta_i)/2 \quad (95)$$

(see Appendix B).  $k(\theta)$  and  $h(\theta)$  are arbitrary functions. Inserting the expression for  $\tau_{11}^0$  from (93) in (85) and integrating with respect to  $\theta_i$ , we get

$$\sigma_0'(\theta, \theta_i) = k(\theta)\{[h(\theta) - \frac{1}{2}f^2(\theta)] \ln f(\theta_i) + f(\theta_i)[f(\theta) - h(\theta)] + f^2(\theta_i)\} + g(\theta), \quad (96)$$

where  $g(\theta)$  is an arbitrary function of  $\theta$ . Equations (78) and (93)–(96) show how the  $\theta$  and  $\theta_i$  dependence of  $\gamma$ ,  $\tau_{11}^0$ ,  $c$ ,  $C$ , and  $\sigma_0'$  may be expressed in terms of four single variable functions  $f$ ,  $h$ ,  $k$ , and  $g$ . These are the only conclusions of this kind that we have been able to draw from Eqs. (80)–(86).

With the introduction of the free-energy density representation, (55),  $\tau_{11}^0$ ,  $c_{1111}$ ,  $c_{1122}$ ,  $c_{1212}$ ,  $\beta_{11}$ ,  $\hat{\tau}_{11}^0$ , and  $\hat{\beta}_{11}$  satisfy the following equations [see Eqs. (60)–(71)]:

$$\tau_{11}^0 = H_{11}^0, \quad \hat{\tau}_{11}^0 = (\partial H_{11}^0 / \partial \theta)_{\theta_i} / \rho_0, \quad (97)$$

$$\beta_{11} = H_{11}^4, \quad \hat{\beta}_{11} = (\partial H_{11}^4 / \partial \theta)_{\theta_i} / \rho_0, \quad (98)$$

$$c_{1111} = H_{1111}^2 + H_{11}^0, \quad (99)$$

$$\hat{c}_{1111} = [(\partial H_{1111}^2 / \partial \theta)_{\theta_i} + (\partial H_{11}^0 / \partial \theta)_{\theta_i}] / \rho_0,$$

$$c_{1122} = H_{1122}^2 - H_{11}^0, \quad \hat{c}_{1122} = (\partial H_{1122}^2 / \partial \theta)_{\theta_i} / \rho_0, \quad (100)$$

$$c_{1212} = H_{1212}^2 + H_{11}^0, \quad (101)$$

$$\hat{c}_{1212} = [(\partial H_{1212}^2 / \partial \theta)_{\theta_i} + (\partial H_{11}^0 / \partial \theta)_{\theta_i}] / \rho_0.$$

Using these identities, we now show that Eq. (86) can be derived from (80). This appears to be the only effect the introduction of  $F$  has on Eqs. (60)–(71). Inserting  $\hat{\tau}_{11}^0$ ,  $\hat{c}_{1111}$ , and  $\hat{c}_{1122}$  from (97), (98), and (99) into Eq. (86), we have

$$\frac{1}{\rho_0} \frac{\partial}{\partial \theta} \left[ \left( \frac{\partial H_{11}^0}{\partial \theta_i} \right)_\theta + A_{11}(\theta_i)[2H_{11}^0 + H_{1111}^2 + 2H_{1122}^2] - \frac{H_{11}^0}{\rho_0} \left( \frac{\partial \rho_0}{\partial \theta_i} \right) \right] = 0. \quad (102)$$

Now,

$$\left( \frac{\partial \rho_0}{\partial \theta_i} \right)_\theta = 3\rho_0 A_{11}, \quad (103)$$

(see Ref. 12) and, hence, Eq. (102) can be written in the form

$$\frac{1}{\rho_0} \frac{\partial}{\partial \theta} \left[ \left( \frac{\partial H_{11}^0}{\partial \theta_i} \right)_\theta + A_{11}(\theta_i) \right. \\ \left. \times [-H_{11}^0 + H_{1111}^2 + 2H_{1122}^2] \right] = 0. \quad (104)$$

On inserting  $\tau_{11}^0$ ,  $c_{1111}$ , and  $c_{1122}$  from Eqs. (97), (99), and (100) into the left side of Eq. (80), we obtain precisely the quantity in square brackets in Eq. (104); hence, Eq. (86) is equivalent to Eq. (80).

### VIII. DISCUSSION

In this section, we describe some of the implications of the  $\theta_i$  dependence of the equation of state. The discussion will be restricted to the case of the elastic stiffness  $c_{ijkl}$ .

We have seen in the previous sections that, in general, the elastic stiffness must be regarded as a function of two variables,  $\theta$ , the temperature of the state of interest and  $\theta_i$ , the temperature of the initial state. In Fig. 1, we have depicted a family of curves  $c_{ijkl}$ -versus- $\theta$ , with parameter  $\theta_i$ . Experimentally, we would expect to get one curve of this family from a set of static measurements in which stresses are applied isothermally and the resultant changes in lengths and/or angles (relative to some initial state) are recorded. In contrast, in a dynamic measurement of  $c_{ijkl}$ , the sample is induced to vibrate about the stress free state at the temperature of interest and this measurement, therefore, yields—after the transformation from adiabatic to isothermal constraint is carried out— $c_{ijkl}(\theta, \theta)$ . This function is clearly not a member of the family  $c_{ijkl}(\theta, \theta_i)$  sketched in Fig. 1. We must, therefore, conclude that static and dynamic measurements give different  $\theta$  functions for  $c_{ijkl}$ . In particular, the slopes of the curves  $\theta_i \equiv \text{const}$  and  $\theta_i \equiv \theta$  are  $(\partial c_{1111}/\partial \theta)_{\theta_i}$  and  $(dc_{1111}/d\theta) = [(\partial c_{1111}/\partial \theta)_{\theta_i} + (\partial c_{1111}/\partial \theta_i)_{\theta}]$ , respectively. It is shown in Sec. IX that, in the case of NaCl, the difference between these quantities is significant.

### IX. NUMERICS

From (83) and (84),

$$\frac{1}{c_{1111}} \left( \frac{\partial c_{1111}}{\partial \theta_i} \right)_\theta = -A_{11} \left( 1 + \frac{2(C_{111111} + 2C_{111122})}{c_{1111}} \right), \quad (105)$$

$$\frac{1}{\beta_{11}} \left( \frac{\partial \beta_{11}}{\partial \theta_i} \right)_\theta = -\frac{2A_{11}}{\beta_{11}} [\tilde{q}_{1111} + 2\tilde{q}_{1122}]. \quad (106)$$

<sup>12</sup> The value of the mass density cannot be a function of the choice of initial state and, hence, Eq. (25):

$$(\partial \rho / \partial u_{ki}) A_{ni}(\theta_i) (\delta_{kn} + u_{kn}) + (\partial \rho / \partial \theta_i) = 0.$$

Now,  $\rho = \rho_0[1 - u_{ii} + 0(u_{ij}u_{ji})]$ , where  $\rho_0$  is the mass density in the initial state described by  $\theta_i$  and, hence,

$$-\rho_0 A_{ii}(\theta_i) + (\partial \rho_0 / \partial \theta_i) = 0.$$

When  $A_{ii} = A_{11}\delta_{ij}$ , we obtain (103).

We expand  $f(\theta)$  in powers of  $(\theta - \theta_i)$  and use the approximation

$$f(\theta) \cong f(\theta_i)[1 - \alpha(\theta - \theta_i)]; \quad (107)$$

hence, from (87) and (88),

$$A_{11} = -\alpha, \quad (108)$$

$$\gamma(\theta, \theta_i) = \alpha(\theta - \theta_i). \quad (109)$$

Thus,  $\alpha$  is the coefficient of linear expansion. In the case of NaCl, the parameters appearing on the right of (105) and (106) have the following values:

$$A = -4 \times 10^{-5} \text{ } ^\circ\text{K}^{-1}, \text{ (RT, Ref. 13)}$$

$$\beta_{11} = 0.17/\epsilon_0, \text{ (RT, Ref. 14),}$$

$$\tilde{q}_{1111} = -2/\epsilon_0^*, \text{ (0}^\circ\text{K, Ref. 15),}$$

$$\tilde{q}_{1122} = 0.26/\epsilon_0^*, \text{ (0}^\circ\text{K, Ref. 15),}$$

$$c_{1111} = 4.9 \times 10^{11} \text{ dyn/cm}^2, \text{ (RT, Ref. 16)}$$

$$C_{111111} = -5.8 \times 10^{11} \text{ dyn/cm}^2, \text{ (RT, Ref. 17)}$$

$$C_{111122} = -5.8 \times 10^{10} \text{ dyn/cm}^2, \text{ (RT, Ref. 17).}$$

RT stands for room temperature. The asterisk indicates theoretical values. With these data and Eqs. (105) and (106), we can calculate  $(\partial c_{1111}/\partial \theta_i)/c_{1111}$  and estimate the value of  $(\partial \beta_{11}/\partial \theta_i)/\beta_{11}$  at room temperature; hence,

$$\frac{1}{c_{1111}} \left( \frac{\partial c_{1111}}{\partial \theta_i} \right)_\theta = -4.8 \times 10^{-4} \text{ } ^\circ\text{K}^{-1}, \quad (110)$$

$$\frac{1}{\beta_{11}} \left( \frac{\partial \beta_{11}}{\partial \theta_i} \right)_\theta = -7 \times 10^{-4} \text{ } ^\circ\text{K}^{-1}. \quad (111)$$

Overton and Swim (Ref. 18) and Robinson and Hallett (Ref. 14) report the following room-temperature values (Ref. 19):

$$\frac{1}{c_{1111}} \left( \frac{dc_{1111}}{d\theta} \right)^{\text{ad}} = 8 \times 10^{-4} \text{ } ^\circ\text{K}^{-1},$$

$$\frac{1}{\beta_{11}} \left( \frac{d\beta_{11}}{d\theta} \right) = -(5.9 \times 10^{-4}) \text{ } ^\circ\text{K}^{-1}. \quad (112)$$

<sup>13</sup>P. M. Meincke and G. M. Graham, Can. J. Phys. **43**, 1853 (1965).

<sup>14</sup>M. C. Robinson and A. C. Hollis-Hallett, Can. J. Phys. **44**, 2211 (1966).

<sup>15</sup>J. Grindlay and H. C. Wong, Can. J. Phys. **47**, 1563 (1969).

<sup>16</sup>J. K. Galt, Phys. Rev. **73**, 1460 (1948).

<sup>17</sup>P. B. Ghatge, Phys. Rev. **139**, A1666 (1965).

<sup>18</sup>W. C. Overton and R. T. Swim, Phys. Rev. **84**, 758 (1951).

<sup>19</sup>Robinson and Hallett measured the permeability at constant (zero) stress, i.e.,  $(\partial E_i/\partial D_i)_{\tau, \theta}$ . Standard arguments for  $m3m$  symmetry yield

$$(\partial E_i/\partial D_i)_{\tau, \theta} = \beta + (\tilde{q}_{1111} + 2\tilde{q}_{1122})\gamma.$$

See, for example, J. Grindlay, *An Introduction to the Phenomenological Theory of Ferroelectricity* (Pergamon Press, Ltd., Oxford, 1970). With the constraint  $\theta \equiv \theta_i$ ,  $\gamma \equiv 0$  and, hence,  $(\partial E_i/\partial D_i)_{\tau, \theta} = \beta$ .

Both measurements were carried out dynamically (i.e.,  $\theta \equiv \theta_i$ ); this fact is indicated by the use of the total derivative notation (see Sec. VIII). The superscript ad denotes the adiabatic value; it is superfluous in the case of the permeability but not in the case of the elastic stiffness  $c_{1111}$  of NaCl (see reference in footnote 19). Since the adiabatic correction for  $c_{1111}$  is small, we conclude from these results that, for NaCl at room temperature,

$$\left| \left( \frac{\partial c_{1111}}{\partial \theta_i} \right)_{\theta} \right| \sim \left| \left( \frac{\partial c_{1111}}{\partial \theta} \right)_{\theta_i} \right|,$$

and

$$\left| \left( \frac{\partial \beta_{11}}{\partial \theta_i} \right)_{\theta} \right| \sim \left| \left( \frac{\partial \beta_{11}}{\partial \theta} \right)_{\theta_i} \right|.$$

### APPENDIX A

The nonlinear elastic coefficients  $C_{ijvwxy}$ , Eq. (29), can be written in terms of the  $H_{ijk}$ 's, Eqs. (49) and (50); we find

$$\begin{aligned} C_{ijvwxy} = & \frac{1}{2} [H_{ij}^0 (J_{vwxy} + J_{xyvw}) \\ & + H_{wy}^0 \delta_{iv} \delta_{jx} + H_{wy}^0 \delta_{ix} \delta_{jv} - \delta_{vw} (H_{yj}^0 \delta_{ix} + H_{yi}^0 \delta_{jx}) \\ & - \delta_{xy} (H_{wj}^0 \delta_{iv} + H_{wi}^0 \delta_{jv}) + H_{ijwy}^2 \delta_{vx} - H_{ijxy}^2 \delta_{vw} \\ & - H_{ijvw}^2 \delta_{xy} + H_{ijvw}^2 \delta_{ix} + H_{wxy}^2 \delta_{iv} \\ & + H_{yivw}^2 \delta_{jx} + H_{wixy}^2 \delta_{jv}] + H_{ijvwxy}^5, \quad (\text{A1}) \end{aligned}$$

with

$$\begin{aligned} J_{1111} = J_{2222} = J_{3333} = 1, \\ J_{1122} = J_{2211} = J_{1133} = J_{3311} = J_{2233} = J_{3322} = J_{1221} = J_{2112} \\ = J_{1331} = J_{3113} = J_{2332} = J_{3223} = \frac{1}{2}; \end{aligned}$$

the remaining  $J_{vwxy}$ 's vanish.

The coefficients  $C_{ijvwxy}$  have the property that

$$C_{ijvwxy} = C_{ijxyvw} = C_{jivwxy}. \quad (\text{A2})$$

The first equality holds as a result of the definition of these coefficients, Eq. (29), and the second equality results from the introduction of an energy density together with the demands of rotational invariance [see discussion under (iii) in Sec. 1].

For material symmetry  $m3m$  the  $C_{ijvwxy}$  are invariant under the transformations  $x_1 \rightarrow x_2$ ,  $x_2 \rightarrow -x_1$ ,  $x_3 \rightarrow x_3$

and  $x_1 \rightarrow x_2$ ,  $x_2 \rightarrow x_3$ ,  $x_3 \rightarrow x_1$ ; hence,

$$\begin{aligned} C_{111111} &= H_{111111}^5 + \frac{3}{2} H_{1111}^2, \\ C_{111122} &= H_{111122}^5 + \frac{1}{2} (H_{1122}^2 - H_{1111}^2 - H_{11}^0), \\ C_{221111} &= H_{111122}^5 - \frac{1}{2} H_{1122}^2 + H_{11}^0, \\ C_{111212} &= H_{111212}^5 + 2H_{1212}^2 + \frac{1}{2} H_{1122}^0 + H_{11}^0, \\ C_{121112} &= H_{111212}^5 + \frac{1}{2} (H_{1212}^2 + H_{1122}^2 - H_{11}^0), \\ C_{112112} &= H_{111212}^5 + H_{1212}^2 + \frac{1}{2} H_{11}^0, \\ C_{122111} &= C_{212111} = H_{111212}^5 + \frac{1}{2} H_{1111}^2, \\ C_{212313} &= H_{121323}^5 + H_{1212}^2 + \frac{1}{2} H_{11}^0, \\ C_{123213} &= C_{123231} = H_{121323}^5 + \frac{1}{2} H_{1212}^2, \\ C_{211233} &= C_{121233} = H_{121233}^5 + \frac{1}{2} (H_{1122}^2 - H_{1212}^2 - H_{11}^0), \\ C_{331212} &= H_{121233}^5 + \frac{1}{2} H_{1122}^2, \\ C_{332112} &= H_{121233}^5 + \frac{1}{2} H_{11}^0, \\ C_{221212} &= H_{121222}^5 + \frac{1}{2} H_{1111}^2, \\ C_{332211} &= H_{112233}^5 - H_{1133}^2 + \frac{1}{2} H_{11}^0. \end{aligned}$$

The remaining coefficients, which cannot be obtained from these results using the subscript interchanges quoted above, vanish identically.

### APPENDIX B

To solve Eqs. (90)–(92), we first eliminate  $\tau_{11}^0$ ,  $\gamma$ , and  $C$  between Eqs. (88) and (90)–(92) to get

$$c'' + c'(3A_{11} - A_{11}'/A_{11}) + 2A_{11}^2 c = 0, \quad (\text{B1})$$

where  $c' = (\partial c / \partial \theta_i)_{\theta}$ , etc. We set

$$c(\theta, \theta_i) = k(\theta) \exp - \int H(\theta, \theta_i) d\theta_i,$$

where  $k(\theta)$  is some arbitrary function of  $\theta$ . Then,  $H(\theta, \theta_i)$  satisfies the Ricatti equation

$$H' = H^2 - (3A_{11} - A_{11}'/A_{11})H + 2A_{11}^2. \quad (\text{B2})$$

A particular solution to this equation is  $H = A_{11}$ ; hence,<sup>20</sup>

$$c(\theta, \theta_i) = k(\theta) f(\theta_i) \{ h(\theta) + [f(\theta_i) - f(\theta)] \}. \quad (\text{B3})$$

With this solution, we may then deduce expressions for  $\tau_{11}^0$ ,  $C$ ; hence,

$$\begin{aligned} \tau_{11}^0(\theta, \theta_i) = & [f(\theta_i) - f(\theta)] k(\theta) \\ & \times \{ h(\theta) + \frac{1}{2} [f(\theta_i) - f(\theta)] \}, \quad (\text{B4}) \end{aligned}$$

$$C(\theta, \theta_i) = k(\theta) f^2(\theta_i) / 2. \quad (\text{B5})$$

<sup>20</sup> H. T. H. Piaggio, *Differential Equations* (G. Bell and Sons, London, 1952), Chap. XV.